



Naval Warfare Research Center Final Report

March 1976

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MATERIEL WEIGHT AND CUBE CONTROL (1975-1980)

By: T. H. ALLEN, JR., and R. B. RINGO

Prepared for:

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U.S. MARINE CORPS
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a Marine Amphibious Force are compared with the capacities of available Navy

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Materiel criticality designation
Operational readiness evaluation
Shipping requirements

Time dependant phasing Usage rates Weight and cube control

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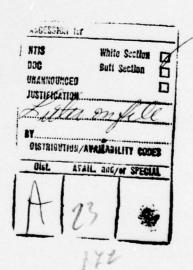
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#### ABSTRACT

Procedures are given for reducing USMC landing force materiel to be embarked in USN amphibious assault ships while minimizing loss of force readiness or sustainability. The feasibility of reducing this materiel by incremental phasing of units into the objective area by means other than amphibious assault ships is evaluated. Amphibious lift requirements for Marine air/ground task forces are computed by the SRI/NWRC-developed MAGTF computer system. Lift requirements of the assault echelon of a Marine Amphibious Force are compared with the capacities of available Navy amphibious assault ships to determine lift short falls. The effect on lift requirements of future changes to landing force materiel is analyzed. Described is a computer system designed as a decision aid for systematically reducing landing force materiel when required to load assault forces into a constrained amphibious lift capacity while optimizing the operational readiness of the force. A procedure for analyzing the effect on amphibious lift capability of introducing new materiel into the Fleet Marine Force is presented.

A



### PREFACE

The objective of logistics support for an amphibious landing has always been to provide the landing force with the materiel and equipment it needs for the duration of a campaign. In the past, those charged with the task of developing the logistic support operations used a simple, straightforward method. A scheme of maneuver would be projected for anticipated combat ashore, and logistic support requirements would be developed from this scheme and from the usage rates of previous similar combat operations. Shipping requirements would than be determined from the computed weight, cube, and square of personnel to be embarked.

Current and future anticipated economic constraints on the Military Services of this country may reduce the number of naval ships dedicated to amphibious warfare below levels previously available. This could result in shortages of lift capacity which will require modifications to earlier procedures for embarking MAGTF's. One aid to the logistics planner to offset this lift constraint will be a system that provides a rapid and accurate estimate of materiel and supplies required to sustain a landing force in accomplishing its combat mission.

Of critical importance to the planner will be the designation of those support functions expected to be required in the amphibious objective area (AOA) before arrival of the assault follow-on echelon shipping. Due to the shortage of naval amphibious ships comprising the assault echelon of the amphibious task force, the planning task includes determining those units whose functions are required to support the combat units of the MAF from D-Day to arrival of the AFOE in order to reduce the material required to be embarked in the assault echelon ships. During planning for the

arrival of the AFOE ships (when additional units and the preponderance of materiel became available for employment in the operation) consideration must also be given to the determination of functions, personnel and materiel actually required in the AOA during the assault phase, timephasing of materiel into the AOA as it is needed and air lift utilization when the situation permits.

Against this background, a series of logistic planning studies have been conducted by the Naval Warfare Research Center of Stanford Research Institute. When implemented, these studies will improve the logistic support planning process with respect to the Fleet Marine Force. The project, "Marine Air Ground Task Force Lift and Logistic Planning Factors Model (1975-1985) (MAGTF)," completed in January 1975, provides data expressing the amphibious lift requirement based on current allowances and replenishment rates. The MAGTF Model generated by that project provides the necessary tool for computing amphibious lift requirements for variable levels of materiel.

Based on data obtained from the MAGTF Lift Model, the landing force materiel of a notional MAF that is desired to be embarked in amphibious shipping has far greater volume than the total capacity of the available amphibious assault ships. Procedures are developed for reducing landing force materiel in a constrained amphibious lift capacity environment so that the operational readiness of the embarked force has been optimized.

The study was conducted for the Commandant of the Marine Corps under Contract N0014-75-C-0708. The originating agency was the Deputy Chief of Staff (Research Development and Studies). The sponsoring agency was the Concepts and Analysis Branch, Deputy Chief of Staff for Installations and Logistics (LPC). Project officer was Lieutenant Colonel J. E. Miller, USMC, Head, Concepts and Analysis Branch.

The analysis was conducted by members of the Tactical Logistics and Mobility Program of the Naval Warfare Research Center (NWRC), L. J. Low, Director. T. H. Allen, Jr., was the project leader. Other SRI principal contributors were C. J. Bording, R. S. Garnero, C. M. Ramos, and R. B. Ringo. A. R. Grant provided data from the GAMUT Simulation Model in support of the amphibious task force unloading problem. W. H. 7wisler assisted in the MAGTF improvement task. Dr. J. L. Brenner served as consultant to the project.

# CONTENTS

DD F	ORM 1	473	i
ABST	RACT		v
PREF	ACE .		vii
LIST	OF I	LLUSTRATIONS	xv
LIST	OF T	ABLES	xvii
I	INTR	ODUCTION	I-1
	A.	Scope	1-2
	в.	Method of Approach	1-3
	c.	Glossary of Terms Used in the Study Report	1-4
II	SUMM	ARY	11-1
	Α.	Feasibility of Reducing Amphibious Lift Requirements	11-1
	В.	Feasibility of the Incremental Phasing of Materiel Into the Amphibious Objective Area	11-3
	c.	Implementation Considerations for the Constrained Amphibious Lift Analysis System	11-4
			11-4
	D.	Actions to Establish a Materiel Weight and Cube Control Program	11-4
III	CONC	LUSIONS AND RECOMMENDATIONS	111-1
	Α.	Conclusions	111-1
		1. Objective I	111-1
		2. Objective II	III-3
			111-3
	В.	Recommendations	111-4
		1. Objectives I and II	111-4
			TTT-5

IV	STAT	TUS OF AMPHIBIOUS LIFT	IV-1
	Α.	General	IV-1
	В.	Scenario	IV-2
	c.	Amphibious Lift Capacity	IV-3
	D.	Amphibious Lift Requirements	IV-10
v	ANAL	LYSIS OF LANDING FORCE MATERIEL REQUIREMENTS	V-1
	Α.	General	V-1
	В.	The MAGTF System	V-1
		1. MAGTF Improvement	V-1
		2. MAGTF Lift Composition and Validity	V-2
		3. Data Base Update	V-7
	С.	Materiel Adjustments	V-16
		1. T/E Reductions	V-16
		2. New Materiel	V-19
		3. The New Combat Service Support	
		Organizational Structure	V-24
	D.	Analysis of Mountout/Prepositioned War	
		Reserves Materiel (PWRM)	V-30
	an i r	CONCERNATION AMONTOTORIC LITTE ANALYSIS CHARRY	
VI		AS)	VI-1
	Α.	General	VI-1
	В.	CALAS Description	VI-2
	C.	Amphibious Lift Requirements Subsystem	VI-5
	D.	Transportation Feasibility Estimator Model	
•		(TFE)	VI-7
VII	THE	CONSTRAINED AMPHIBIOUS LIFT PROBLEM	VII-1
	Α.	General	VII-1
	В.	Loading the CSS Notional MAF	VII-2
		1. Amphibious Lift Requirement Preparation 2. The TFE Subsystem	VII-2
		<ol> <li>The TFE Subsystem</li></ol>	VII-2
		Subsystem	VII-3

VII	THE	CONSTRAINED AMPHIBIOUS LIFT PROBLEM (Continued)	
	C.	Changing the Force Structure	VII-28
		<ol> <li>Third and Fourth Echelon         Maintenance Elimination</li></ol>	VII-29 VII-31 VII-34
	D.	The Timing Problem in Phasing Materiel into the Amphibious Objective Area	VII-40
VIII	A WE	GIGHT AND CUBE CONTROL PROGRAM	VIII-1
	Α.	Requirements	VIII-1
	В.	Background	VIII-1
	C.	Areas of Emphasis	VIII-2
	D.	Major Materiel Acquisition Phases	VIII-2
IX		IBIOUS STAFF PLANNING AND THE CONSTRAINED IBIOUS LIFT ANALYSIS SYSTEM (1985)	IX-1
	Α.	General	IX-1
	В.	CALAS Within an Automated Command and Control System	IX-2
		<ol> <li>CALAS and MIS</li></ol>	IX-3
		Requirements	IX-5
	С.	Implementation Considerations	1X-6
		<ol> <li>Program Conversion to IBM 360</li> <li>MAGTF Improvement Project</li> <li>MAGTF Data Base Maintenance</li> </ol>	IX-6 IX-6
	D.	Conclusions	IX-7
APPE	NDICE	S S	
	A	BIBLIOGRAPHY	A-1
	В	TROOP LISTS AND SAMPLE MAGTF OUTPUT	B-1
	С	SAMPLES OF COMPUTER OUTPUTS	C-1
	D	A MODEL TO COMPUTE AMPHIBIOUS LIFT FOR A VARIABLE DAY OF SUPPLY FROM THE F-2 JOPS CARD	D-1

# APPENDICES (Continued)

E	CONSTRAINED CARGO FACTORING MODEL	E-1
F	CONSTRAINED T/E EMBARKATION MODEL	F-1
	Part 1. Narrative Description	F-3
G	MAGTF IMPROVEMENT EFFORT	G-1
н	HO FMFPAC DATA ANALYSIS	H-1

# ILLUSTRATIONS

VI-1	Constrained Amphibious Lift Analysis System (CALAS)	VI-3
VII-1	Weighted Constrained Unit Loading Versus Percent Short Fall for the AE Using Assigned Parameters	VII-4
VII-2	Weighted Constrained Unit Loading Versus Percent Short Fall for Square Loaded Cargo Constraint Fixed at 88 Percent	VII-6
VII-3	Weighted Constrained Unit Loading Versus Percent Short Fall for AE Units Using 10 DOS Mountout	VII-27
VII-4	Weighted Constrained Unit Loading Versus Percent Short Fall for Reduced AE Force Structure	VII-38
VII-5	Weighted Constrained Unit Loading Versus Percent Short Fall Comparing the AE of the CSS Notional MAF with the Reduced AE Force Structure	VII-39
VII-6	Weighted Constrained Unit Loading Versus Percent Short Fall for Adjusted Mountout	VII-49
VII-7	Weighted Constrained Unit Loading Versus Percent Short Fall for the MAB Reduced Troop List with 34-Ship Force	VII-61
VII-8	Weighted Constrained Unit Loading Versus Percent Short Fall for Modified Troop List and Mountout Increase from Vietnam Data and Extra Tanks	VII-71
VIII-1	Proposed Family of Shelters and Transport	VIII-5
D-1	Program TFEIN	D-15
E-1	Program AMPSF	E-20
E-2	Subroutine CONST	E-25
F-1	Flow Diagram Illustrating the Assignment of Priorities to TAMs According to the Importance of	
	the Function the TAMs Support Within the Unit	F-47

F-2	Program CONTEAM	F-53
F-3	The Truncated Normal Distribution Truncated at $t = 0$ , $a = 0.78\bar{x}$ , $\sigma = 0.47\bar{x}$	F-70
F-4	Approximate Form of Relation Between LAM and Cube	F-80
H-1	Routine for Extracting TAM Records from Master	н-5

# TABLES

IV-1	Ships Involved in Swing Shift to Lift 1 MAF,	/
	FY-79	IV-4
IV-2	Amphibious Ship Force from MMROP	IV-5
IV-3	Amphibious Lift Capacity Used in the Computer Model	IV-6
IV-4	HQFMFPAC Source	IV-7
IV-5	HQFMFLANT Source	IV-8
IV-6	Notional MAF Source Comparisons	17-11
IV-7	Notional Marine Amphibious Force (MAF)	IV-12
IV-8	CSS Notional Marine Amphibious Force (MAF)	IV-13
V-1	Assault Echelon Lift Supply Class Organization	V-8
V-2(a)	Notional MAF Assault Echelon Lift Requirement	V-13
V-2(b)	Notional MAF Assault Follow-On Echelon Lift Requirement	V-14
V-3	MAGTF Program Input Parameters	V-15
V-4	Units Selected for T/E Reduction Analysis	V-17
V-5	Comparison of Planned TAM Items With Replacement TAMs for Bulk Loaded Items	V-21
V-6	Comparison of Planned TAM Items With Replacement TAMs for Square Loaded Items	V-22
V-7	Comparison of Cube and Square of Existing Shelter System with Replacement Shelter System	V-23
V-8(a)	CSS Notional MAF Assault Echelon Lift Requirement	V-25
V-8(b)	CSS Notional MAF Assault Follow-On Lift Requirement	V-26

V-9	Notional and CSS MAF Comparison	V-2
V-10	AFOE Unit Function Comparisons	V-29
V-11	Percentage of TAM Items (Type 1) Having CARFs	V-30
V-12	Demand Rates for Class VII Square Loaded Items	V-36
V-13	Mountout Adjusting Factor Calculation: Vietnam Data (Classes IIW, VIIW Nonsquare)	V-38
V-14	Mountout Adjusting Factor Calculation: Vietnam Data (Class VIIW Mountout)	V-39
V-15	Values Used to Compute a CARF Adjusting Factor from the 1968 TAM	V-41
VII-1	Constraint Values and DOS for CCF Model Processing	VII-3
VII-2	Weighted Constrained Unit Loading vs. Percent Short Fall	VII-5
VII-3(a)	Constrained T/E for M1038 When Constrained to 90% of Authorized T/E Lift Requirement	VII-8
VII-3(b)	Constrained T/E for M1038 When Constrained to 85% of Authorized T/E Lift Requirement	VII-12
VII-3(c)	Constrained T/E for M1038 When Constrained to 75% of Authorized T/E Lift Requirement	VII-16
VII-3(d)	T/E Item Deficiencies of M1038 When Constrained to 90%, 85% and 75% of Authorized T/E Lift	
	Requirement	VII-20
VII-4(a)	Constrained Cube for Classes IIW and VIIW Nonsquare and VIIW Square (T/E Categories	
	Only)	VII-24
VII-4(b)	Constrained Factored Cargo Categories	VII-25
VII-5	Weighted Constrained Unit Loading vs. Percent Short Fall	VII-28
VII-6	Eliminated AE Units	VII-30
VII-7	Amphibious Lift Tradeoff from Substituting Maintenance Contact Teams for Maintenance	
	Units in the AE	VII-32

VII-8	Equipment Necessary to Support Beach Cargo Handling Function	VII-33
VII-9	Logistic Support Vehicles, AE	VII-34
VII-10	Amphibious Lift Tradeoff from Phasing Force Engineer Units into the AOA from AFOE Support Ships	VII-35
VII-11	Combat Support Units Selected for Phased Deployment	VII-35
VII-12	Aviation CSS Units Selected for Phased Deployment	VII-37
VII-13(a)	Program GAMUT Input Parameters: Runs No. 1 and No. 2	VII-42
VII-13(b)	Program GAMUT Input Parameters: Run No. 3	VII-43
VII-14	Ship Unloading Rates and Times: Conventional Landing Craft	VII-44
VII <b>-1</b> 5	Ship Unloading Rates and Times: Advanced Landing Craft	VII-45
VII-16	Unloading Rates for Conventional Landing Craft at a 25-NMI Standoff Distance	V11-46
VII-17	Marine Amphibious Unit (MAU) Troop List	VII-53
VII-18	Marine Amphibious Brigade (MAB) Troop List	VII-54
VII-19	MAB Unit Cargo Categories	VII-57
VII-20	Weighted Constrained Unit Loading vs. Percent Short Fall for a Notional MAB to be Loaded in	
	a 34-Ship Force	VII-58
VII-21	Units Selected for Reduced MAB Troop List	VII-59
VII-22	Lift Requirements for the Residual MAF	VII-62
VII-23	Follow-On Residual Assault Echelon of MAF	VII-63
VII-24	CSS AFOE Lift Requirements	VII-65
VII-25	Commercial Ships Availability and Capacity	VII-66
VII-26	AFOE Lift Requirements	VII-68
7111-1	Sample of Existing Hard Shelter/New Shelter Replacement Allowances	VIII-6

VIII-2	Unit-by-Unit Replacement Allowances for Existing Hard Shelters and Transport with	WIII 0
	New Shelters and Transport	VIII-8
VIII-3	MAGTF Input Data Cards for Existing Replacement Shelter Analysis	VIII-10
VIII-4	Initial Issue of Major Equipment for Shelter - AE	VIII-12
VIII-5	General Cargo for Shelter - AE	VIII-15
VIII-6	Mountout (Class III) for Shelter - AE Organizational Load	VIII-16
VIII-7	Mountout (Class III) for Shelter - AE Landing Force Supplies	VIII-17
F-1	Equipment Functions	F-24
F-2	M1038 Infantry Battalion Functions, By Relative Importance	F-40
F-3	M1758 Service Battalion Functions, By Relative Importance	F-41
F-4	List of Unit Functions, By Relative Importance	F-43
F-5	Sequence of TAMs Sorted According to the Benefit Provided by Each UnitConstraint = 45	F-75
F-6	Values of the Normal Probability Integral, $P(u)$ , for Values of u Between 0.0 and 3.49	F-76
G-1	Comparison Between Original Version of MAGTF and Improved Version of MAGTF Execution Times	
	for Processing Marine Corps T/O Units	G-11

### I INTRODUCTION

The objectives of the study, and thus of this report, are to:

- (1) Within the constraints of operational readiness and sustainability, determine the feasibility of reducing amphibious lift requirements by reducing the weight and cube of landing force material that is presently in the inventory or programmed; and, if feasible, recommend specific implementation actions.
- (2) Determine the feasibility of reducing overall amphibious lift requirements by the redesign of the incremental phasing and scheduling of material into the amphibious objective area; and if feasible, recommend specific implementation actions.
- (3) Determine actions necessary to establish a viable weight and cube control program for landing force materiel, which will insure that lift requirement considerations are given major attention during the materiel acquisition process.

The foregoing objectives have been achieved without exception.

Section II, immediately following, presents in executive summary form, the general findings of the study within the framework of the above-cited objectives. Every attempt has been made to match objectives with results without unnecessary elaboration or detail. Thus, the reader desiring to quickly grasp the essence of this report is obliged to read no further than the summary and Section III, the Conclusions and Recommendations.

Those readers wishing to explore the details of the completed research are invited to pursue the remaining sections of the report. These sections essentially reflect the research steps taken during the course of the study. A brief description of these steps is given here for guidance.

- (1) Section IV presents a development of the problem as defined by the first two study objectives.
- (2) Section V provides an explanation of the data used to conduct the analysis of the study.
- (3) Section VI describes the computerized mathematical models used to obtain the problem solution procedure.
- (4) Section VII contains the data analysis and numerical results supporting the problem solution procedure.
- (5) Section VIII explains the Materiel Weight and Cube Control Program developed during the study, as required by the third objective.
- (6) Section IX presents a description of an automated data systems (ADS) environment for implementing the computer system developed within the study.
- (7) The appendices contain technical information, i.e., extensive data supporting the analysis, mathematical model descriptions, and general flow charts describing computer programs.

# A. Scope

The primary source of guidance for the research reported on in this document was the Marine Corps Mid-Range Objectives Plan (MMROP). The stated capability requiring the lift of the assault echelon of a MAF by amphibious assault ships provided the basic framework for the scenario within which the principal areas for research were conducted. Subsidiary research into the use of common user airlift and sealift to support the total MAF lift requirement was also included.

The study examined in detail the nature and extent of landing force materiel as defined and computed by the MAGTF Computer System. It should be noted that results obtained from this study are based upon the assumption that the MAGTF Computer System expresses a true representation of amphibious lift requirement for the units depicted as derived from official allowances, with the exception of MAGTF data base deficiencies defined in Section V of this report.

The numbers and characteristics of amphibious assault ships defining amphibious lift capacity to support the assault echelon (AE) of the MAF were also included in the research effort.

The effect of unloading times for amphibious assault ships on the possibilities of phasing units within the AE troop list ashore from assault follow-on echelon support ships was part of the study.

A research task was conducted to develop a materiel weight and cube control program which would monitor the effect on the lift status of units in the FMF from introducing new items of materiel into tables of equipment (T/Es).

A MAGTF Program improvement task was included in the study with the purpose of reducing the excessive processing time required to compute MAF lift requirements using the original version of the program.

# B. Method of Approach

The study was conducted in three phases. Phase I included the MAGTF improvement task, which was required to support the study effort. The gathering of pertinent data and specification of the scenario were also part of Phase I.

Phase II was devoted to analyzing landing force material in its many categories for accuracy and completeness and developing mathematical models to conduct the necessary data analysis. The extent of the amphibious lift short fall, i.e., landing force material of the AE that cannot be loaded into the available amphibious assault shipping was determined.

The data analysis conducted during Phase III provided the insight necessary for generating a computer assisted decision aid that provided the solution procedure for satisfying the objectives of the study.

# C. Glossary of Terms Used in the Study Report

In order to assist the reader in understanding the special meanings of the various terms used in this report, the following glossary is provided.

MAGTF -- Marine Air Ground Task Force of MAF, MAB, or MAU.

MAU--Marine Amphibious Unit, with the battalion landing team as the combat element.

MAB--Marine Amphibious Brigade, with the regimental landing team as the combat element.

MAF--Marine Amphibious Force, with the reinforced Marine Division providing three regimental landing teams as the combat element.

AE -- assault echelon of the MAF.

AFOE--assault follow-on echelon of the MAF.

Amphibious lift requirement—the totals of bulk cargo in units of the measurement ton (40 cubic feet) and square loaded cargo in square feet for a unit or groups of units.

Amphibious lift capacity -- the bulk cargo (in measurement tons) and square loaded cargo (in square feet) that can be loaded into an amphibious assault ship or groups of ships.

Amphibious lift short fall--the amount of cargo that could not be put into a group of amphibious assault ships for a specified group of troop units.

Constrained amphibious lift short fall--the amount of cargo that could not be put into a group of amphibious assault ships after having been reduced by an applied constraint for a specified group of troop units.

AOA -- amphibious objective area.

SMLS -- Seaborne Mobile Logistics System.

<u>Unit load</u>—the amount of cargo carried by a unit when embarked in assault shipping, consists of organic materiel and a specified number of days of supply for mountout.

Landing force supply--the amount of cargo embarked in assault shipping and required to support the AE of the MAF, consists of the specified number of days of supply of mountout.

TFE Model--Transportation Feasibility Estimator Model, converted to a practical computer simulation program from a CINCPAC version called GFE by HQ FMFPAC.

<u>CSS</u>--combat service support, used in this study to designate a group of units recently reorganized.

MAGTF System -- refers to a series of computer programs and data base developed by NWRC/SRI in a previous project.

MAGTF Program -- the computing program of the MAGTF System providing the lift requirement listings used in this study.

<u>DODIC</u>--Department of Defense identification code for ammunition items.

OMA--a designation for unit cargo to support organizational level maintenance in USMC aircraft squadrons.

<u>IMA</u>--a designation for unit cargo to support intermediate level maintenance in USMC headquarters and maintenance squadrons.

TMR--Tables of Manpower Requirements, an automated file of tables of organization used by the MAGTF System to update the MAGTF data base.

<u>VALU card</u>--the term used to describe the card input used to manually update the MAGTF data base.

CREATE--the computer program within the MAGTF System that converts the tape files of the MAGTF data base to direct access disk files.

FLOAT quantities—an amount of equipment in supply classes IIW and VIIW carried by units of the Force Service Support Group to replace major end items deadlined from FMF units.

<u>LVTs</u>--landing vehicles tracked (amphibious tractors) used by the AE of the MAF to carry initial assault waves to the beach.

<u>JOPS</u>--Joint Operational Planning System (defined in JCS Pub 6, Part 6).

CARF--combat active replacement factor (derived from the TAM).

TAM -- Table of Authorized Materiel.

### II SUMMARY

# A. Feasibility of Reducing Amphibious Lift Requirements

It is possible to examine the impact of reducing the amount of cargo desired to be embarked in amphibious ships of the assault echelon on force effectiveness and/or sustainability through the use of constraints applied by a computer system designed to augment the decision making process.

Research into the feasibility of reducing amphibious lift requirements directed the study efforts to analyzing the purpose, composition, and amount of materiel to be loaded into amphibious assault ships for units comprising the assault echelon (AE) of the MAF. The basic scenario for the study defines the amphibious lift problem within the framework of lifting the AE of the MAF by sea for an assault on a hostile shore. This scenario constitutes the greatest demand for lift as outlined by the MMROP, which was used as the basic guidance for the study.

The first research task performed to determine the feasibility of reducing amphibious lift was to analyze the table of equipment (T/E) for a sample of organizations included in the AE for nonessential equipment. Findings from this task established that units are continuously conducting T/E reviews to eliminate nonessential items. Many items included in T/Es are essential for some function at some specific time but may not be essential for carrying ashore in an amphibious assault and could be landed from AFOE support ships at a later time in the operation. While this task failed to provide a significant reduction in lift requirements, it did suggest an approach for the solution procedure that was later developed.

Comparison of the amphibious lift requirement obtained from the MAGTF System (using the force structure contained in the MMROP) and the total capacity of the available force of 59 amphibious ships showed that only 60 percent of the designated material of the AE of the MAF could be loaded. This result varies drastically when compared to the MMROP notional MAF assault echelon requirement which supposedly can be lifted by a force of 49 amphibious ships.

The determination of the magnitude of the amphibious lift short fall directed research efforts to the development of a systematic procedure to reduce unit amphibious lift requirements by the application of constraints until the reduced force could be loaded into the available lift capacity. The system developed permits the evaluation of operational readiness for every constraint level applied and further determines the effect on the lift short fall from varying the mountout days of supply for loading in assault shipping.

The systematic procedure generated to reduce amphibious lift requirements consists of three computerized mathematical models organized into a computer assisted decision aid to be used by the commander and his staff on an on-line-real-time basis or in a batch-mode processing environment. The system named, the Constrained Amphibious Lift Analysis System (CALAS), combines the computational power and speed of the computer with the operational experience and subjective judgment of the Commander to determine the force level which optimizes operational readiness within the constrained amphibious lift environment. The study provides extensive constrained loading analysis using the AE of a notional MAF within the framework of the scenario to demonstrate the practicality and feasibility of the developed approach to the constrained amphibious lift problem.

# B. <u>Feasibility of the Incremental Phasing of Materiel</u> Into the Amphibious Objective Area

The incremental phasing of materiel to reduce amphibious lift requirements appears entirely feasible. "Appears" is the appropriate descriptor since, while the second objective of the study directs the study of the feasibility of reducing landing force materiel carried by the AE by incrementally phasing and scheduling materiel into the objective area, the scenario for the study contained only notional forces without a specified enemy or terrain, and the requirement to include units performing specialized functions in the AE could not be specified. The analysis therefore was limited to determining the effects on the constrained lift problem of removing these units from the AE troop list.

The solution procedure, CALAS, was also used to determine the effect on the amphibious lift short fall from varying the units within the AE force structure to obtain a problem solution. In point of fact, no solution is possible without the combination of varying the units to be included in the troop list with the systematic reduction of material from included units and the possible reduction of mountout to be carried by the AE. Both eliminated units and material from embarked units are assumed to be phased ashore from the AFOE support ships.

The effect of the timing problem on phasing AE units ashore from the AFOE support ships was determined by calculating unloading times from a computer simulation model called GAMUT. This task showed that all ships of the 59-ship force lifting the AE could be unloaded in 37 hours. The days required would depend on the hours per day unloading could take place. A beach cargo handling simulation was also used to determine that adequate material handling assets were available to prevent beach congestion.

# C. <u>Implementation Considerations for the Constrained</u> Amphibious Lift Analysis System

The study presents a concept which adapts the computer programs of CALAS into the management information systems (MIS) of the future. The exact configuration of Marine Corps Automated Data Systems (ADS) of the 1980s is presently under study at SRI. The Marine Tactical Command and Control System is also presently under development. CALAS would become an operational system to be employed in a predeployment environment and could reside in either an administrative, tactical or combination MIS.

Although the development of computer software for installation on a USMC computer system was not envisioned at the beginning of the study, the obvious advantages of using a system such as CALAS to be a computer assisted decision aid for field use will require careful consideration. The primary application for this system would be at the MAF staff level. The proposed system would be accessed by the MAF G-4 from a terminal in his office on line with the MAF computer. Within a period of about 5 hours or less, depending on the number of units in the MAGTF troop list prepared in response to a warning order, the MAF G-4 would be able to analyze and solve a constrained amphibious lift problem presented by an insufficient number of amphibious assault ships achieving an optimized operationally ready force.

## D. Actions to Establish a Materiel Weight and Cube Control Program

The third objective of the study required the development of Materiel Weight and Cube Control Program. In effect, this objective defined a research task which would develop a procedure to be included within the Marine Corps materiel acquisition process to determine the effect on amphibious lift of introducing new items of equipment into the T/Es of FMF units. The MAGTF System was found to be ideally suited for this purpose.

During the acquisition process a time is reached when the physical characteristics of an item are established on a conceptual basis. Since most items are replacing some existing piece of equipment, the procedure advanced in this study consists of performing an update of the MAGTF data base to include the newly considered item of equipment. Once this is done, MAGTF runs would be processed for units planned to receive the new equipment. Lift totals of these units would be compared before and after the introduction of the new equipment to determine the overall effect on lift.

The principal advantages of this procedure are that the MAGTF program includes not only the weight, cube and square of the item, but also computes the secondary effect of fuel requirements, repair parts, and ammunition requirements if appropriate. The update of the MAGTF data base requires the inclusion of these secondary lift requirements when appropriate.

The study offered an example of how this procedure should be accomplished and computational results. The new family of shelters was used as a prime example. With the increase of 13,900 square feet of shelter space, an increase of 62.5 measurement tons of bulk cargo requirement and 2500 square feet of square loaded cargo space on the AE of the CSS MAF would occur upon the introduction of the shelter items.

### III CONCLUSIONS AND RECOMMENDATIONS

## A. Conclusions

The conclusions derived from the analysis reported herein have been organized to support each objective of the study in order of their importance. Conclusions are also presented at the end of each section. Following each conclusion is a page number reference which includes the section and the page.

# 1. Objective I

- (a) The cargo lift requirement for the assault echelon of a representative MAF, as presented in the MMROP, is significantly less than that computed by the MAGTF System. (Page
- (b) Based on the MAGTF System Data, an amphibious lift short fall of approximately 40 percent would occur when loading the assault echelon of a notional MAF into the available amphibious assault ships used in this study. (Page IV-14.)
- (c) Based on the MAGTF System Data, significant amphibious lift short falls will exist when attempting to load a MAB whose troop list is the size of the notional MAB used in this study into a 34-ship force, and, to a greater extent, a 21-ship force. (Page VII-56.)
- (d) The use of CALAS installed within an automated command and control system provides the computational support necessary to systematically determine the optimal operationally ready force in a constrained amphibious lift environment in a short period of time during the planning phase of an amphibious operation. (Page VII-2.)
- (e) The Constrained T/E Embarkation Analysis Model using the criticality factors denoting all item's importance to a unit's function provides a practical systematic methodology for reducing a unit's T/E when its lift requirements

must be constrained by limited assault shipping assets. This analytical procedure may also be used to compute lift requirements for airlift when a percentage reduction of unit T/E materiel is desired. (Page VII- 7.)

- (f) It is feasible to implement CALAS on USMC computer systems to function as a computer assisted decision aid in amphibious staff planning. (Page IX-6.)
- (g) Current USMC computer installation work loads will dictate the timing of installing CALAS on USMC computer systems. (Page IX-6.)
- (h) The overall capability of the MAGTF System and the continuous requirement for lift data from all categories of cargo available from this system justifies the expenditure of effort to conduct the further improvement of the MAGTF Program and continued updating of the MAGTF data base. (Page V-15.)
- (i) The MAGTF System generated lift expression for the MAF is the most current and accurate source of this specialized data in existence. (Page V-2.)
- (j) The known errors in the MAGTF System data cause an understatement of the total lift requirement. (Page V-9.)
- (k) The T/E reviews conducted by units in the FMF prevent the accumulation of significant quantities of nonessential equipment. (Page V-16.)
- (1) The combat active replacement factor (CARF) used to compute PWRM for mountout and mountout augmentation is not currently based on realistic expected consumption rates for supply classes IIW and VIIW. (Page V-30.)
- (m) The statement of mountout for supply classes IIW and VIIW computed from current combat active replacement factors (CARF) may be inadequate to support future expected combat losses. (Page V-30.)
- (n) The practice of using the same value for CARF for mountout calculations regardless of the different missions of units in the force results in an inadequate statement of mountout or prepositioned war reserve materiel. (Page VII-51.)

# 2. Objective II

- (a) The lift requirements for the notional MAF AE are larger than can be satisfactorily reduced by applying constraints to complete units in order to fit into amphibious assault shipping capacity. The solution procedure advanced in this study requires the incremental phasing of certain AE units into the objective area from AFOE support ships. (Page VII-28.)
- (b) An assessment of the time phased deployment ashore possibilities for combat and combat service support units within the MAGTF mission provides the greatest potential for optimizing the utilization of limited amphibious assault ship assets. (Page VII-29.)
- (c) Based on GAMUT simulation results, the potential for landing the AE from the amphibious assault force used in this study within 3 days is a real possibility. (Page VII-46.)
- (d) In some amphibious operations, units may begin unloading from AFOE support ships from D+2 on. (Page VII-46.)
- (e) The unloading rates simulated by GAMUT can be supported by the units handling cargo transfer operations at the beach. (Page VII-47.)
- (f) Sufficient ships are available to lift the AFOE of the MAF from common user sealift assets. (Page VII-69.)

## 3. Objective III

- (a) The comparative analysis between the existing/replacement shelter systems performed with the assistance of Program MAGTF to determine the effects upon amphibious shipping requirements has demonstrated the usefulness of the program in a cube, square, and weight control program. (Page VIII-9.)
- (b) The "conceptual stage" of system and materiel acquisition by the Marine Corps could utilize Program MAGTF to determine the total effects of the new acquisition on the lift requirements of the MAF. (Page VIII-2.)

(c) The utility of Program MAGTF may also be used in the "conceptual phase" of system and material acquisition to investigate the secondary effects of the acquisition, such as fuel consumption, repair parts requirements, ammunition consumption, and personnel requirements. (Page VIII-3.)

# B. Recommendations

- 1. The following recommendations are provided to satisfy objectives 1 and  $2^1$ .
  - (a) The amphibious lift expression computed from the MAGTF System should be by cognizant Marine Corps considered for adoption staff agencies for official planning data.
  - (b) The MAGTF lift expression should be considered for use by Fleet Marine Force Commands to determine materiel deficiencies relative to authorized allowances.
  - (c) The Constrained Amphibious Lift Analysis System should be considered for adoption as a planning aid in Fleet Marine Force Commands. If recommendation (c) is approved, NWRC/SRI would be available to prepare an IBM 360 computer system version of CALAS and to install on a MAF computer of the 360-65 configuration.
  - (d) The proposal submitted to Headquarters U.S. Marine Corps to conduct the improvement task for the MAGTF program should be considered for use at an appropriate time and be considered part of the implementation of CALAS on MAF computer systems.
  - (e) The proposal mentioned in the previous recommendation includes a task for correcting MAGTF data base deficiencies and to support a continuous data base update effort. It is also recommended that this task be given favorable consideration.
  - (f) A study to conduct a detailed analysis of the combat active replacement factors used to compute mountout for supply classes IIW and VIIW and usage rates for supply class IX be considered for the studies program in the near future. This study should also analyze the requirement to assign CARFs to units reflecting the mission in the assigned values.

<sup>1</sup> See Page I-1 for the study objectives.

- 2. The following recommendations are provided to satisfy objective 31.
  - (a) That the Materiel Weight and Cube Control Program defined in this study be considered for adoption within the Marine Corps Materiel Acquisition Process.
  - (b) The utility of Program MAGTF should also be considered for use in the "conceptual phase" of system and material acquisition to investigate the secondary effects of the acquisition process to include fuel consumption, repair parts requirements, ammunition consumption, and personnel requirements.

See Page I-1 for the study objectives.

### IV STATUS OF AMPHIBIOUS LIFT

## A. General

In the amphibious planning cycle, the stated mission, scheme of maneuver, and geographic characteristics dictate the troop list and days of supply from which amphibious lift requirements are derived. At this point in the cycle, the number of amphibious assault ships required can be determined, permitting the comparison of lift capacity with lift requirement. The predominant consideration in the current amphibious planning environment is the shortage of amphibious assault ships needed to conduct training exercises, support the forward deployment of the MAU and MAB, and lift the assault echelon of the MAF when supporting contingency plans.

When considering the problem of the amphibious ship short fall, one can move in the direction of obtaining more ships, if feasible, or one can examine the nature of landing force materiel planned for embarkation to discover, if possible, where reasonable reductions may be effected. In other words, is the materiel to be embarked in excess of that required to accomplish the assigned mission? To answer this question, there are four principal areas to pursue. The first area is the requirement to justify each unit included in the croop list with respect to the landing force mission. The second area is the combat environment, which includes the enemy situation and terrain. In this regard, certain units may not be required in the objective area until some period after D-Day, thus affecting the selection of units embarked in assault shipping. The third area is the requirement to include all Table of Equipment (T/E) materiel belonging to each unit in its loading plan. The fourth area is the

specification of the days of supply (DOS) embarked with the landing force. When amphibious lift capacity is fixed at some level below the desired lift requirement, reductions must be exacted from the four areas stated above. Since a specific mission and combat environment was not given for the study, an analysis of troop list adequacy to support a mission is not included. However, tradeoffs in lift requirements from removing certain units from the troop list are offered; these may be used for planning until an actual mission is assigned to a landing force commander. These four areas affecting landing force material constituted the major research areas of the study. Research into these areas provided the support for satisfying the first two objectives of the project.

This section contains the factors defining the scenario that provides the structure for analyzing landing force material within a constrained amphibious lift environment. The amphibious lift short fall will be presented, along with the lift capacity derived from the list of amphibious ships and their characteristics affecting loading that were used in the study. The lift requirement for the MAF troop list obtained from the MMROP, as modified by the MAGTF Project and the MAF troop list containing the new combat service support (CSS) organizations, are used to determine the amphibious lift short fall.

### B. Scenario

The structure for conducting this study was directed to be employment of a notional MAF as described in the MMROP. The case taken for the primary research was the deployment of a MAF to an overseas destination totally by sealift, excluding self-deployable fixed wing aircraft and those associated support equipments normally considered as a fly-in echelon. The AE was specified to be lifted by amphibious assault ships, with the AFOE lifted by common user sealift. The AFOE was scheduled to arrive by D+5, with an increment scheduled to arrive on D-Day. This case constitutes the "worst case" condition in terms of the amphibious lift short fall.

The following conditions define the scenario of the study:

- (1) A notional MAF was deployed with no specific mission
- (2) Transit time to the AOA was 8 days
- (3) The amphibious assault consisted of two RLTs landed by helicopter at inland landing zones
- (4) One RLT landed over the beach
- (5) All support forces landed over the beach
- (6) The beach was organized into one colored and two numbered beaches
- (7) No time factors in ship loading were considered in the scenario
- (8) The unloading problem in the objective area and beach clearing operations were considered part of the scenario
- (9) The availability of common user sealift was assumed
- (10) The troop list used for the analysis conducted in the study was the notional MAF containing the new CSS organization.

The following variation to the scenario was included:

(1) Deploy the MAF by escalating from an initial MAB deployment.

## C. Amphibious Lift Capacity

The ships available to lift the AE of the MAF were provided to the project team by CNO (OP 323). Table IV-1 presents the ship types used throughout the study. This list contains all amphibious assault ships in one fleet and a force of ships from the other fleet, called the swing force. The total of the force is 59 ships, and 100 percent availability of the ships is assumed in the engaged fleet. This assumption may not be realistic, and an 80 percent availability of the ships in the

Table IV-1
SHIPS INVOLVED TO LIFT 1 MAF
FY-79

1 MAF Lift	From LANT To PAC	PACFLT Assets	TYPE	LANTFLT Assets	From PAC To LANT	1 MAF Lift
2	1	1	LCC	1	1	2
6	2	4	LKA	2	4	6
11	4	7	LPD	7	4	11
2	1	1	LPA	1	1	2
7	4	3	LPH	4	3	7
4	1	3	LHA	2	2	4
11	4	7	LSD	6	5	11
16	6	10	LST	10	6	16
59	23*	36		33	26*	59

<sup>\*</sup> Size of Force Assumes 100 Percent Availability of Ships in the Engaged Fleet

engaged fleet may be more realistic. It should be noted that the force defined in the MMROP consists of 49 ships. The ship types for this total are found in Table IV-2.

Table IV-2

AMPHIBIOUS SHIP FORCE FROM MMROP

Ship Class	Number
LCC	2
LKA	4
LPD	9
LPH	5
LHA	5
LSD	8
LST	16
Total	49

This force, being less than the total for the swing force, may be closer to reality since it allows for some ship nonavailability.

The lift capacity of the ships used in the computer models of the study are listed in Table IV-3. The basic data source used to determine the ship lift characteristics were HQFMFPAC and HQFMFLANT pamphlets. These pamphlets differed in their definition of terms (Tables IV-4 and IV-5 contain this data). The data obtained from these pamphlets was further modified by ship plans available at SRI as they were applied to a ship loading/unloading model called GAMUT that was used in the analysis of amphibious assault landing craft. The application of GAMUT in this study will be presented later in the report. Table IV-3 lists the lift

 $\label{tw-3} \mbox{ Table IV-3}$  (U) AMPHIBIOUS LIFT CAPACITY USED IN THE COMPUTER MODEL (U)

Order	Туре	ID	Passengers	Sq Ft	MT	Barrels
1	LKA	30	226	43,025	3,158	0
2	LKA	31	226	43,872	3,153	0
3	LKA	32	226	44,062	3,153	0
4	LKA	34	322	23,871	1,343	0
5	LKA	48	226	38,100	1,825	1,276
6	LKA	49	226	38,100	2,093	1,276
7	LPA	33	1,374	10,322	613	0
8	LPA	47	1,331	9,137	2,764	4,114
9	LHA	2	1,903	28,000	3,802	563
10	LHA	2	1,903	28,000	3,802	563
11	LHA	2	1,903	28,000	3,802	563
12	LHA	2.	1,903	28,000	3,802	563
13	LPD	7	947	12,500	1,564	0
14	LPD	8	927	13,300	1,576	0
15	LPD	9	858	13,700	1,188	0
16	LPD	10	861	12,400	1,413	0
17	LPD	11	875	11,000	1,243	0
18	LPD	12	859	13,200	1,440	0
19	LPD	41	925	13,100	873	2,849
20	LPD	42	863	14,000	1,326	8,871
21	LPD	43	1,863	13,600	1,111	8,380
22	LPD	44	861	18,400	549	8,381
23	LPD	46	922	14,100	404	8,871
24	LSD	13	333	4,455	0	0
26	LSD	15	323 316	4,455	0	0 99
27	LSD	16	314	4,455	0	0
28	LSD	17	337	4,455	0	0
29	LSD	18	337	4,455	0	0
30	LSD	19	337	4,455	0	0
31	LSD	50	316	4,455	0	1,153
32	LSD	51	308	4,455	0	761
33	LSD	54	337	4,455	0	. 780
34	LSD	55	337	4,455	0	822
35	LST	20	386	20,960	134	8,738
36	LST	21	386	20,960	134	8,738
37	LST	22	386	20,960	134	8,738
38	LST	23	386	20,960	134	8,738
39	LST	24	386	20,960	134	8,738
40	LST	25	386	20,960	134	8,738
41	LST	26	386	20,960	134	8,738
42	LST	27	386	20,960	134	8,738
43	LST	28	386	20,960	134	8,738
44	LST	29	386	20,960	134	8,738
45	LST	56	317	24,000	600	3,372
46	LST	57	393	21,000	525	8,784
47	LST	58	387	21,000	525	8,784
48	LST	59	396	24,000	600	5,628
49	LST	60	387	24,000	0	5,628
50 51	LST	61	387	23,780	0	5,628
52	LPH	3 4	1,771	4,766 4,338	1,434	6,333
53	LPH	5	1,764	5,886	1,272	6,333
54	LPH	36	1,970	5,567	1,472	6,489
55	LPH	37	1,948	7,370	1,444	7,060
56	LPH	38	1,933	6,781	1,342	6,909
57	LPH	39	1,801	6,349	1,143	8,863
				-,		-,
	TOTAL			711,923*	47,192*	223,409

<sup>\*</sup>Totals reduced by broken stowage factor.

Table IV-4

(U) HQFMFPAC SOURCE (U)

ID	Ship	Passengers	Cu Ft	Sq. Ft	Sq Ft Add'1 (X	1000)
1	Blue Ridge LCC-19	281	0	2,800	Helo plat	5
					Flt deck	60
2	Tarawa LHA-1 (F)	1903	152,112	29,400	Hgr deck	21
					Well deck	19
					Hgr deck	13
3	Okinawa LPH-3 (F)	1771	57,366	4,766	Flt deck	45
4	Tripoli LPH-10 (F)	1764	51,820	4,338	-Do-	
5	New Orleans LPH-11 (F)	1815	50,882	5,586	-Do-	
					Well deck	8
6	Vancouver LPD-2	926	28,056	11,928	Helo plat	14
					Well deck	8
7	Ogden LPD-5	947	61,831	14,083	Helo plat	15
					Well deck	8
8	Duluth LPD-6	927	63,054	15,185	Helo plat	15
					Well deck	7
9	Cleveland LPD-7 (F)	858	47,525	15,618	Helo plat	15
					Well deck	7
10	Dubuçus LPD-8 (F)	861	56,509	13,978	Helo plat	15
					Well deck	7
11	Denver LPD-9 (F)	875	49,699	12,104	Helo plat	15
					Well deck	7
12	Juneau LPD-10 (F)	859	57,614	15,025	Helo plat	15
					Well deck	18
13	Thomaston LSD-28	333	6,010	9,432	Helo plat	5
					Well deck	18
14	Pt Defiance LSD-31	323	5,523	9,012	Helo plat	5
					Well deck	18
15	Alamo LSD-33	316	3,957	8,268	Helo plat	5
					Well deck	18
16	Monticello LSD-35	314	4,473	8,960	Helo plat	5
					Well deck	20
17	Anchorage LSD-36	337	1,580	11,201	Helo plat	5
					Well deck	20
18	Mt Vernon LSD-39	337	1,580	11,201	Helo plat	5
		-			Well deck	20
19	Ft Fisher LSD-40	337	1,580	11,201	Helo plat	5
20	Fresno LST-1182	386	5,370	20,960	Helo plat	2.6
21	Peoria LST-1183	386	5,370	20,960	Helo plat	2.6
22 ,		386	5,370	20,960	Helo plat	2.6
23	Schenectady LST-1185	386	5,370	20,960	Helo plat	2.6
24	Cayuga LST-1186	386	5,370	20,960	Helo plat	2.6
25	Tuscaloosa LST-1187	386	5,370	20,960	Helo plat	2.6
26.	San Bernardino LST-1189	386	5,370	20,960	Helo plat	2.6
27	Racine LST-1191	386	5,370	20,960	Helo plat	2.6
28	Barbour Cty LST-1195	386	5,370	20,960	Helo plat	2.6
29	Bristol Cty LST-1198	386	5,370	20,960	Helo plat	2.6
30	Durham LKA-114	226	126,329	43,025	Helo plat	5
31	Mobile LKA-115	226	126,114	43,872	Helo plat	5
32	St Louis LKA-116	226	126,107	44,062	Helo plat	5
33	Paul Revere LPA-248	1374	24,524	10,322	Helo plat	4
34	Tulare LKA-112	322	53,706	23,871	. Helo plat	4

Table IV-5
HQFMFLANT SOURCE

ID	Ship	Passengers	Cu Ft	Sq Ft
35	Mount Whitney LCC-20	627	24,408	3,426
36	Iwo Jima LPH-2	1970	58,883	5,567
37	Guadalcanal LPH-7	1948	57,746	7,370
38	Guam LPH-9	1933	53,687	6,781
39	Inchow LPH-12	1801	45,707	6,349
40	Raliegh LPD-1	931	84,094	11,000
41	Austin LPD-4	925	34,934	14,848
42	Coronado LPD-11	863	53,055	16,093
43	Shreveport LPD-12	1863	44,456	15,564
44	Nashville LPD-13	861	42,319	21,975
45	Trenton LPD-14	924	48,951	13,754
46	Ponce LPD-15	922	53,263	16,184
47	Francis Marion LPA-249	1331	110,570	9,137
48	Charleston LKA-113	226	79,983	38,100
49	El Paso LKA-117	226	83,714	38,100
50	Plymouth Rock LSD-29	316	N/A	26,371
51	Port Snelling LSD-30	308	N/A	27,525
52	Spiegel Grove LSD-32	273	N/A	28,746
53	Heritage LSD-34	265	N/A	30,412
54	Portland LSD-37	337	N/A	32,269
55	Pensacola LSD-38	337	N/A	32,269
56	Newport LST-1179	317	N/A	24,000
57	Manitowac LST-1180	393	N/A	21,000
58	Sumter LST-1181	387	N/A	21,000
59	Saginaw LST-1188	396	N/A	24,000
60	Boulder LST-1190	387	N/A	24,000
61	Spartanburg County LST-1192	386	N/A	23,780
62	Fairfax County LST-1193	386	N/A	24,094
63	La Moure County LST-1194	345	N/A	24,094
64	Harlan County LST-1196	294	N/A	24,094
65	Barnstable County LST-1197	294	N/A	22,000

data used in the Transportation Feasibility Estimator (TFE) Model and the Constrained Cargo Factoring Model, which are also explained in a later section of this report.

The following considerations were used in determining the data in Table IV-3:

Well deck space was used for boats of the Assault Craft Unit and LVTs. The square loading capacity assigned to well deck spaces was based on preloading the boats. A broken stowage factor of .6 was used in loading vehicles into boats. The square feet of the boats and LVTs was not included in the unit's cargo totals holding this material.

Helicopter platforms, flight deck, and hangar deck spaces were not included in ship loading capacity. Aircraft were not included in lift requirements for squadrons.

Due to the nature of the cargo found in the AE of the MAF, the models of this study were designed to convert excess square loading space into bulk cargo, if available. No square loaded cargo was permitted to be loaded into bulk stowage spaces. Broken stowage factors were assigned as follows:

- (1) Bulk BSF = .8
- (2) Square BSF = .75.

The passenger and bulk fuel cargo categories were not included in the analysis of this study.

No special considerations were made for loading ammunition or handling supply class V separately. Investigation of ammunition stowage spaces revealed that sufficient space existed with the ships of the force supporting the AE of the MAF. An assumption is therefore made that ammunition will be stowed separately in assigned spaces. Any unused space resulting from an

insufficient amount required on separate ships was not allowed in the model. Therefore, class V was included in the total bulk for loading, and all ammunition spaces were included in ship capacity.

The helicopter loading problem on the LHA and LPA type ship was not included in this study. Only personnel and all other material for units having aircraft was considered in the loading analysis.

## D. Amphibious Lift Requirements

Before the comparison of lift capacity with lift requirement can be made, cargo totals for the MAF must be established. Table IV-6 presents two notional MAF lift requirement cargo totals. In the table the cargo totals for the notional MAF are derived from a troop list provided to the MAGTF Project by the Study Advisory Committee. With some alterations, the troop list used for this MAF is the same as in the MAGTF Project. At the beginnings of this study, this MAF was adopted as the base case for all analysis. Table IV-7 provides an outline of the organizational structure of this MAF. At the end of Phase I of the study, the project team was advised that a new organizational structure for combat service support (CSS) was adopted for integration into the FMF. Research was begun at that time to develop cargo data for a notional MAF that included the new CSS structure. The organizational structure in outline form for the CSS MAF is listed in Table IV-8. The detailed troop lists for these MAFs are found in Appendix B. As shown in Table IV-6, cargo lift requirements for the two notional MAFs are considerably higher than the data presented in the MMROP for the same MAF troop list. The significant differences between the MMROP data and the other raises the question of data validity. This subject will be discussed in detail in Section V. The troop list for a notional MAF provided in the MMROP differs from those used in MAGTF by including two TOW Co, a Tank Bn, and two 155mm How Btry, FAG. The

Table IV-6
NOTIONAL MAF SOURCE COMPARISONS

	Notional	CSS Notional
		<u>AE</u>
Bulk, MT*	82,906	77,624
Square, sq ft	870,856	786,926
		AFOE
Bulk, MT*	105,749	189,009
Square, sq ft	658,076	648,209

<sup>\*</sup> Measurement Tons

## Table IV-7

## NOTIONAL MARINE AMPHIBIOUS FORCE (MAF)

## Assault Echelon

Command Element
Radio Bn
Communications Bn

Ground Combat Element
Marine Division
Tank Bn
AMTRAC Bn
Field Arty Grp

Aviation Combat Element MACG 2nd MAG (VH)

Combat Service Support Element
Medical Bn
Service Bn
Shore Party Bn
Military Police Bn /-/
Engineer Bn /-/
Det FSR

## Assault Follow-On Echelon

Command Element

Aviation Combat Element LAAM Bn MWSG

Combat Service Support Element
Det Serv Bn
MT Bn
Det Engr Bn
FSR

## Fly-In Echelon

Aviation Combat Element Det 3rd MAG

#### Table IV-8

# CSS NOTIONAL MARINE AMPHIBIOUS FORCE (MAF)

## Assault Echelon

Command Element
Radio Bn
Communications Bn

Ground Combat Element
Marine Division
Tank Bn
AMTRAC Bn
Field Arty Grp

Aviation Combat Element
MACG
2nd MAG (VH)

Combat Service Support Element
Medical Bn
Div Serv Spt Grp
Military Police Bn
Engineer Bn /-/
Det FSSG

## Assault Follow-On Echelon

Command Element

Aviation Combat Element LAAM Bn MWSG /-/

Combat Service Support Element
MT Bn /-/
Det Engr Spt Bn
FSSG /-/

## Fly-In Echelon

Aviation Combat Element Det 3rd MAG source for the cargo data of the notional MAF and the version containing the new CSS structure was the MAGTF System.

#### E. Amphibious Lift Short Fall

The MAF lift data presented herein was compared with the amphibious lift capacity to obtain an understanding of the extent of the lift short fall. The data provided by the MAGTF System for the assault echelon of the MAF, when compared to the lift capacity of the 59-ship force used in the study, indicates a lift short fall of 40 percent for bulk cargo and 10 percent for square loaded cargo. Based on data from the present study, only 60 percent of the AE of the notional MAF will fit in the available ships. The lift data contained in the MMROP indicates that all AE cargo for the same MAF can be lifted by the 59-ship force.

These results reveal the extent of the problem facing the amphibious planner. The completion of the MAGTF System project in January 1975 made possible the undertaking of the study now being reported. The foundation of all study results to be presented herein is based on the data generated by the MAGTF System. Therefore, Section V presents an analysis of landing force material in order to substantiate the results obtained from the entire study.

#### F. Conclusions

The following conclusions are presented based on the MAGTF System data:

- (a) The cargo lift requirement for the assault echelon of a representative MAF, as presented in the MMROP, is significantly less than that computed by the MAGTF System. (Page IV-10.)
- (b) Based on the MAGTF System Data, an amphibious lift short fall of approximately 40 percent would occur when loading the assault echelon of a notional MAF into the available amphibious assault ships used in this study. (Page IV-14.)

In summary, this section has provided the framework for conducting the study from the scenario description. The data used to represent amphibious lift capacity for the study was provided along with a statement of MAF lift requirements. The extent of the amphibious lift short fall was then presented, highlighting the magnitude of the problem to be solved within this study.

## REFERENCES (U)

- A. R. Grant; "Systems Analysis of Amphibious Assault Landing Craft"; NWRC/MSO-RM-67, Stanford Research Institute, Menlo Park, California; 1973.
- W. L. Edwards, H. B. Wilder, T. H. Allen, W. Schubert, and J. L. Brenner; "Organization and Operation of Combat Service Support Elements of the Fleet Marine Forces (1975-1980)"; Naval Warfare Research Center, Stanford Research Institute, Menlo Park, California; March 1974.

#### V ANALYSIS OF LANDING FORCE MATERIEL REQUIREMENTS

#### A. General

An accurate statement of the cargo lift requirement for the assault echelon of a MAF configured for an amphibious assault is essential before the adequacy of the amount of assault shipping can be determined. The previous section illustrated the variety of assessments of amphibious lift capacity that can result from vastly dissimilar statements of lift requirement. Cargo lift requirements were presented for two notional MAFs generated from the MAGTF System. It is therefore necessary to substantiate the data used in this study that was obtained from the MAGTF System.

A major part of project work was devoted to an improvement effort of the MAGTF Program and to data base update to enhance system processing time and data accuracy. Results of these efforts are reported in this section. An explanation of the nature and composition of MAGTF data output is presented to provide an understanding of MAGTF data, which is expected to establish its validity.

Various adjustments to materiel of the MAF may have impact on lift requirements during the 1976-1980 time period. Research into these areas was among the tasks of the study. Results from this work are presented in this section.

## B. The MAGTF System

#### 1. MAGTF Improvement

The MAGTF System<sup>1</sup>, when installed on the HQMC computer, processed the first MAF using as input the troop list of the notional MAF found in

Appendix B. The processing time was about 63 hours. The restart procedure designed in the MAGTF Program permitted processing the MAF in 2- to 8-hour increments. The output from this run indicated minor errors in the data base and the program code. At the beginning of this project, the MAGTF System was also operational on the SRI CDC 6400 computer. Since MAGTF was required to provide the data for this project and the processing time was excessive, a task was included and approved in the study outline plan to conduct a limited program modification to the MAGTF Program for the purpose of reducing processing time. This task also included the correction of any processing errors found in the program as the result of extensive use of the output. When completed, this effort reduced the running time of the same troop list to 15 hours. (The actual time will vary according to the number of programs processing simultaneously in the computer.)

The new version of the MAGTF Program was installed on the HQMC computer when completed. Use was made of the Naval Postgraduate School, Monterey, California, Computer Center for debugging and processing most production runs needed for the study. Appendix G provides a complete explanation of the MAGTF improvement task. Although a dramatic reduction in processing time was achieved during this effort, further modifications, identified as the result of this work, are expected to reduce processing time by at least 50 percent. When processing a MAF in 5 to 7 hours becomes possible, extensive use of the capabilities of the system will be feasible on the larger MAF computer available in the FMF.

#### 2. MAGTF Lift Composition and Validity

The MAGTF System provides the lift expression, i.e., total cargo requirements, for all units in the FMF for which T/Os and T/Es exist in Marine Corps automated files. There are two types of units in the MAGTF

data base; these are major units and basic units, which are defined in the MAGTF System to be:

- Basic unit--companies, batteries
- Major unit--any organizational level having "basic units" as subordinate units, i.e., battalions and higher level organizations.

The following explanation of unit lift data applies to the basic unit. Lift data for major units is obtained from processing subordinate basic units. Appendix B contains two simple basic unit listings which can be used for reference during the following discussion.

Cargo data for a basic unit consists of initial issues and mountout. Included in initial issues are garrison operating stocks which are a function of theater peacetime training allowances obtained from the Item Data File (IDF). The MAGTF System defines garrison operating stocks for supply class IX only. Initial issues consist of T/E items obtained from the HQMC Equipment Allowance File (EAF), which is the source of the printed USMC T/E listing. The T/E is composed of supply classes IIW and VIIW and limited IV. The MAGTF data base receives the same allowance as the printed T/E for any basic unit. In addition to ground equipment, supply classes IIA and VIIA are included in initial issues for aviation units. Data for classes IIA and VIIA, ground support equipment (GSE), were obtained from the ADMRL File provided to SRI by the Aviation Materiel Office, Norfolk, Virginia. Supply classes VIIW and VIIA are further separated into square loaded and non-square loaded items for embarkation purposes. The beds of all trucks and trailers contained within basic units are used as mobile loading capacity. The MAGTF Program uses this space to mobile load designated cargo of all eligible supply classes of the unit, thereby providing an accounting for utilized and nonutilized mobile loading space. The weight and dimensions for all class IIW, VIIW, and some VIIA items contained in the MAGTF data base were obtained

from a 2-year data gathering and validation task within the MAGTF Project. The MCDEC Project Officer conducted this extensive effort, which is the foundation of the MAGTF data. Continuous updating and correcting efforts since 1974 have achieved an accuracy of over 90 percent for this data. This effort, of course, never ends so long as the system is in continuous use. Sample listings for initial issues by supply class are found in Appendix B, 'MAGTF Sample Output.'

The second cargo category for the basic unit is mountout. This category consists of all nine classes of supply. For explanatory purposes, mountout is composed of five separate categories. The first category includes supply classes I, VI, and VIII. Data for this group of supply classes included in the MAGTF System was derived from the Table of Authorized Materiel (TAM) and from the MAGTF Project Officer at the Marine Corps Development and Education Command (MCDEC), Quantico, Virginia. The values for weight and cube inserted in the MAGTF data base were therefore based on Marine Corps and Navy authorized planning factors for 1 day of supply (DOS). All data computed by the MAGTF System in this category was validated by the project team and by a validation committee at MCDEC before completion of the MAGTF Project.

The second category within mountout consists of supply class III. The MCDEC Project Officer provided a deck of all Marine Corps TAM items for classes IIW and VIIW that consume fuel or have a mobile loaded item that consumes fuel. The data provided included gallons per hour and average hours per day for the type of fuel consumed for each TAM item. From this source the total gallons per day for each type of fuel consumed per TAM item was computed and entered into the MACTF data base. Included was all packaged grease, gear lube, and engine lube, which were computed as functions of the total gallons of gasoline and diesel as specified by the TAM. Class III consumables of all types were entered for all aircraft

types from data provided from the MCDEC Project Officer (see Appendix B for sample MAGTF listings).

The third mountout category is supply class V. Data for this class was entered directly into the MAGTF data base from Marine Corps Order 8010.1B. This data provides the basic allowance for each DODIC fired by each weapon or individual. The mountout assault rates and sustaining rates for these DODICs were obtained from the IDF. A unit's ammunition load consists of the basic allowance and the specified number of DOS of mountout. Values computed by MAGTF have been validated by the MCDEC committee (see Appendix B for sample listings for class V). Class VA was obtained in a classified version for each aircraft. To avoid complicating the handling, the detailed classified data was not entered into the data base. An unclassified version of total weight and cube for each aircraft was computed and included in the data base.

The fourth category in mountout is supply class IX. Data for this class was obtained from the Marine Corps Supply Activity, Philadelphia, which provided methods of calculating the weight and cube of all repair parts needed to support an end item for all echelons of maintenance for one day. The automated files provided, unfortunately contained repair parts for only about one-third of the end items. Included in the class IX category are the secondary reparables with subclass designation of R-Code and D-Code. Data for these items was provided on magnetic tape. The information on this tape was extracted by program totals calculated for the MAF and loaded into the data base. This cargo requirement is included in the supply company detachment of both MAF lift expressions.

The last categories are classes IIW and VIIW. The mountout computed for these classes was based on the combat active replacement factors contained in the TAM and the T/E allowances. Sources for these

items were the EAF and IDF automated files. Materiel obtained for classes IIA and VIIA as initial issues includes 90 days mountout by definition. Therefore no additional materiel for aviation was included in mountout.

Now that MAGTF data has been explained, the organization of cargo for loading may be presented. For each basic unit, cargo is composed of the unit load and landing force supply. The unit load consists of the initial issues and a prescribed number of DOS for mountout. The MAGTF Program calculates the unit mountout cargo to the desired number of DOS as directed by the landing force commander. In this study five DOS have been specified for mountout accompanying the unit. This value was included, along with other parameters, for cargo computation. Although the DOS for mountout contained in the unit load may be greater than can be transported by organic means, as defined by the "prescribed load2," the excess cargo will still require handling as landing force supply. The specification of the DOS for unit load does not change total lift requirement for the AE. The effect is mostly felt in the total cargo required for initial helicopter lift in the short run, but does not affect total cargo helicopter lift requirements over the period of the assault phase.

Aviation units having aircraft contain GSE equipment for OMA and IMA support as computed by the MAGTF Program. The IMA materiel is always held by the H&MS in reality. This category of classes IIA and VIIA is stored in the MAGTF data base by aircraft rather than by unit due to the organization of the source data file.

Landing force supply contains all classes of supply found in mountout by the specified numbers of DOS. For the AE of this study, 10 DOS were assigned. Landing force supply is computed for each unit based on its requirement, even though this material is consolidated for

handling in loading and unloading. The materiel is, of course, loaded throughout the ships of the amphibious task force.

The final category of materiel is the operational readiness float of major end items. The EAF has provided a source for float computations to support a MAF. The data for this float was obtained but consisted of class VIIW items only. A figure of one-third the total number of items was assigned to the AE, with the remainder assigned to the AFOE. The supply company detachment was assigned the extra square loading items for accounting purposes.

Table V-1 provides a graphic representation of MAGTF cargo data organization as previously explained. This representation does not reflect relative size of the cargo, but only the supply class breakdown in each category of the AE lift expression.

When an amphibious operation is planned for the climatic conditions of desert, cold weather, or Arctic, an additional amount of materiel can be provided to the lift expression by setting an input parameter to the MAGTF Program. The additional cargo will be mainly supply class IIW, type 3, and class III, containing an additional amount of fuel for stoves and other fuel consumers found in T/Es for these climatic conditions. This capability was not used in this study. The effect of an extreme climatic condition is a dramatic increase in lift requirements.

## 3. Data Base Update

The Study Outline Plan included a task for a limited update of parts of the MAGTF data base. It was desired to have as accurate a representation of lift as possible within the time constraints of the study. An update from three primary source tapes was accomplished.

Table V-1
ASSAULT ECHELON LIFT SUPPLY CLASS ORGANIZATION

Unit Load	Landing Force Supply
i, IIW, III, IV, V, VI, VIIW, VIII, IX	I, IIW, III, IV, V, VI VIIW, VIII, IX
- 5 DOS Mountout -	
VIIW Square Loaded	
- 5 DOS Mountout -	- 10 DOS Mountout -
Operational Readiness Float IIW, IIA, IV, VIIW, VIIA	VIIW Square Loaded
- T/E -	
VIIW, VIIA Square Loaded	
- T/E -	- 10 DOS Mountout

Personnel adjustments are constantly occurring in the T/Os of various units. The Table of Manpower Requirements (TMR) Automated Master Line File is the source for T/Os in the MAGTF data base. Distribution of these files includes NWRC/SRI. Three separate updates from the TMR were accomplished during the study. The last update included all new CSS and aviation units recently placed in the file.

The next major update was from the EAF, which made current the T/Es of units in the MAGTF data base. Three complete updates from this file were accomplished, including the new CSS and aviation units.

Three updates by manual preparation methods were also completed.

These updates included a group of TAMs, for which weight and dimensions were not previously available, and corrected all data base errors discovered from the continuous use of the output listings.

The following sources for update were not obtained, or were not accomplished due to reprogramming requirements which could not be performed in the time frame of the study:

- (1) Aviation repair parts
- (2) ADMRL File GSE Data
- (3) Table of Basic Allowance (TBA) File
- (4) Ground repair parts.

In effect, no update of aviation materiel was possible. Data was obtained for ground repair parts, but the extensive programming effort necessary could not be accommodated within the time constraints of the study.

## 4. Data Base Deficiencies

Certain deficiencies in MAGTF data remained at the conclusion of the MAGTF Project. These deficiencies cause an understatement of the lift requirement. The error in MAGTF output, therefore, causes the lift expression to be less than total requirements. These deficiencies were not corrected during the MAGTF Project due to extreme difficulties encountered at the time. Each deficient area is explained below, along with the corrective measures taken.

The designation of certain items in supply class VIIA as square loaded equipment, obtained from the TBA File, was not accomplished. This problem also occurred to a limited degree for GSE items as well. An estimate of 1000 square feet was added to each unit having aviation equipment to partially correct this deficiency.

Supply class IIIA failed to include fuel requirements for GSE fuel consumers. Estimates of the fuel requirement for each aircraft having this type of equipment was added to the MAGTF data base.

As previously mentioned, class IXW, repair parts were initially obtained for about one-third of the end items in unit T/Es. This means that class IXW is understated by about two-thirds. At the time the repair part data was obtained from MCSA, that was all the coding accomplished for this huge data source. A new tape and format were received upon request from MCSA. After examining the programming work required to extract this data, it was decided time was not available to conduct this task within the current study. The MAGTF Program computes up to fourth echelon maintenance requirements for repair parts for each unit. Of course, the unit has maintenance responsibilities of various levels. The MAGTF listing provides the data for class IXW, indicating the amount actually attributed to the unit's requirement and the amount actually carried by supporting maintenance organizations.

Supply class IXA GSE repair parts were never included in MAGTF data sources for entry into the data base during the MAGTF project. Estimates for these items were also obtained during the present study and included in the data base. All estimates of GSE fuel and repair parts were obtained from 3RD MAW units.

Airframe and engine repair parts were originally obtained from 16 tapes received from ASO, Philadelphia, during the MAGTF Project. Of these tapes many records were lost due to parity errors occurring in computer system processing. This category therefore is understated by an unknown degree.

All MAGTF listings for units and totals contain some obsolete supply class VIIW items in unit T/Es. These items were not removed during updates from the EAF files due to interface problems with the source file

and the MAGTF data base. A modification to the EAF LOAD peripheral program will be necessary to eliminate the obsolete TAM items when conducting a routine EAF or T/E update. These obsolete TAM items were identified during this study and were removed from unit lift requirements by computer programs processing the data for the current study.

## 5. Comparison of MAGTF Lift Data With MEDS

During the project, MAGTF data was compared with that obtained from an external source within those supply classes having any commonality. A comparison was made with the Marine Embarkation Data System (MEDS) obtained from units in I MAF.

Four units were used to conduct the "spot check" comparison of MEDS data with MAGTF for supply classes II and VII. The MAGTF lift for classes IIW and VIIW nonsquare were compared between units of the same T/O and T/E as obtained from the MEDS listings, as well as class VIIW square loaded. For T/E M3243, the engineer maintenance company, a 16 percent reduction from MAGTF data was observed for class VIIW square loaded items and a 39 percent reduction in classes IIW and VIIW nonsquare. The numbers in this comparison are not important in themselves. The significant factor is that for whatever reason, MEDS is usually below T/E requirements due to either an incomplete MEDS deck or the existence of T/E deficiencies. Spot checks of other units revealed the same relative differences from MAGTF. Other supply classes and mountout are not included in MEDS, thus preventing a total comparison. When comparing a MEDS listing of aviation units, nothing conclusive could be determined due to very different definitions of cargo categories in the MEDS data.

## 6. Notional MAF Amphibious Lift Expression

The preceding paragraphs have presented the explanatory information outlining the source, composition, adjustments, and validity of the MAGTF System data. In Section IV the total lift requirements and the troop list for the notional MAF were presented. The MAGTF lift expression for the notional MAF is a multivolume document. Copies of these computer output listings are available at NWRC/SRI and at HQMC (Code LPS). The computer system developed for data analysis in this project prepares the lift expression computed from JOPS cards, the automated output of the MAGTF Program. This lift expression is the statement of cargo requirements used in the analysis presented in the next two sections of this report. The units in the notional MAF troop list and their cargo lift requirements are listed in Table V-2. The values for measurement tons of bulk cargo and square feet of square loaded items in Table V-2 were calculated from JOPS cards and adjusted as previously explained. These figures have been reduced from values in the MAGTF listings to compensate for total utilization of unit mobile loaded capacity. This compensation simulates the allocation of vehicles to other units requiring additional mobile loading support.

The amphibious lift cargo totals generated by the MAGTF System are dependent on parameters defined for the program upon execution. Knowledge of these parameters is essential for fully understanding the lift totals. Table V-3 lists the parameters used in all notional MAF runs used in this study. The parameters shown in the table cause the following actions in the lift requirement:

- (1) Loads 2 DOS of diesel and MOGAS into drums as part of the unit load.
- (2) Loads all JP fuel into the bulk category for the AE and AFOE. (Tankers of units generating JP fuel would of course be fully loaded. All other fuel type tankers and cans would also be filled.)

Table V-2(a)

NOTIONAL MAF ASSAULT ECHELON LIFT REQUIREMENT

Unit	Quantity*	MT <sup>†</sup>	Square <sup>†</sup>	Barrels <sup>†</sup>	PAS
CMD-GP	1	3737	86488	4755	2155
M1988	1	936	23004	1340	1368
M1038	9	1014	4427	453	1230
M1096	3	186	4663	491	184
M1128	3	1678	23016	1170	707
M1196	1	969	17364	1208	278
M1378	1	8843	43671	4000	773
M1423	4	437	69	19	85
M1427	1	115	6470	283	130
M1653	3	34	8409	358	79
M1657	1	42	1918	94	58
M4233	4	906	6531	453	110
M4237	1	847	16382	774	313
M4652	4	110	15292	1491	229
M4654	1	226	11536	943	253
****					
M4226	1	677	8661	528	177
M4112	1	664	14469	736	225
M4193	2	417	10497	528	177
M4201	1	67	2019	170	120
M0601F	1	35	0	0	212
M0604F	1	668	11024	906	257
M8821	2	87	2181	208	73
M8612	1	288	21433	1358	419
M8615	i	774	7403	849	217
M8625	1	126	4297	208	284
M8631	1	637	14889	1585	271
M8640	1	283	10912	1208	234
M8914	2	275	5522	283	405
M8921	2	3238	17237	1283	390
M8621	1	309	6578	264	120
M8937	5	1222	4584	1849	248
M8944	3	1264	5480	3604	345
M8964	2	1134	4536	1302	278
M8968	1	1248	4817	1509	231
M8970M	1	1214	4938	1642	391
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M8859	1	2056	7386	8755	372
M0300F	1	136	5432	283	256
M1523	4	93	2869	170	98
M1557	1	174	3015	189	146
M0301F	1	632	9096	358	333
M1743	1	542	16307	1113	404
M1753	1	75	16410	698	132
M0303F	1	952	5137	302	176
M1863	3	57	575	38	66
M1867	1	1404	18715	830	314
M4903	3	35	605	38	120
M4907	1	96	6296	358	182
M4353	2	182	8927	358	165
M0305F	1	212	11914	736	120
M0307F	1	24	571	38	82
M3223	1	409	19264	566	249
M0312F	1	169	6495	170	195
M3243	i	218	5046	151	159
M0314F	i	14	520	19	36
M3253	i	2846	7662	170	128
M0322F	1	2882	22867	19	118
M0324F	1	534	836	170	48
M3333	1	2401	7716	755	370
M0326F	1	105	743	38	129
M0332F	1	18	585	38	98
M0701F	1	6482	2701	66	914

 $<sup>\</sup>star$ Amounts listed are for one (1) unit; multiply by Quantity for total lift requirement.

MT = 82906 Sq = 870856 B1 = 87057
Computed totals have been adjusted by removal of obsolete TAMs.

Table v-2(b)

NOTIONAL MAF ASSAULT FOLLOW-ON ECEHLON LIFT REQUIREMENT

Unit	Quantity*	MT <sup>†</sup>	Square <sup>†</sup>	Barrels <sup>†</sup>	PAS
M4722	1	17	919	200	16
M4392	1	114	2550	800	53
M0602F	1	30	0	0	66
M0605F	1	153	3086	500	77
M8820	3	4712	19439	14200	479
M8620	1	3204	23664	6800	360
M8621	2	581	7013	1400	120
M8710M	1	2998	18589	10300	612
M8715	1	15065	32696	23900	265
M3333P	1	2422	7875	4200	388
M4343	1	7056	32597	2100	185
M4903	1	102	610	300	120
M4512	1	204	2677	1700	122
M4552	4	133	1814	1000	71
M4592	1	266	3897	2100	250
M0304F	1	8	168	0	13
M0302F	1	16	107	0	31
M4643	3	276	10332	2100	82
M4644	1	437	20885	2300	97
M4647	1	184	3925	1500	70
M4353	2	366	8545	2000	165
M0306F	1	441	12763	4200	116
M0308F	1	1470	11707	3300	136
M3213	1	102	1695	300	80
M0313F	1	272	5985	1100	198
M0315F	1	271	16381	3200	121
M0323F	1	314	46219	900	272
M0325F	1	1767	2569	3100	187
M0327F	1	389	2817	900	237
M3346	1	217	9386	1900	155
M3403	1	193	2755	900	243
M3413	1	991	66372	9900	276
M0333F	1	2466	10136	2100	255
M3443	1	251	4531	1300	257
M3447	1	4695	21624	12400	384
M0702	1	4893	53658	0	763
M0603F	1	13	σ	0	4
M8712	1	62	831	200	49
M8652	1	674	11244	62500	122
M8780M	1	1650	7642	64300	429
M8813	3	824	8699	11400	484
M8855	2	6185	7680	26500	227
M8857	2	5269	9417	38700	355
M8849	4	2393	6885	51100	320

<sup>\*\*</sup> Amounts listed are for one (1) unit; multiply by Quantity for total lift requirement.

MT = 105749 Sq = 658076 B1 = 657900

Computed totals have been adjusted by removal of observe TAMs.

Table V-3

MAGTF PROGRAM INPUT PARAMETERS

Parameter	Value
DOS for MAF	60
DOS for AE	15
DOS for AE Unit Load	5
DOS for AE Landing Force Supply	10
DOS for AFOE Landing Force Supply	55
AE DOS for Drummed Fuel	2
AFOE DOS for Drummed Fuel	0
DOS JP Fuel AE Unit Load	0
DOS JP Fuel AE Landing Force Supply	15
DOS JP Fuel AFOE Unit Load	0
DOS JP Fuel AFOE Landing Force Supply	60

All values used in these input fields are options for the user. The values selected were provided by the Study Advisory Committee, HQMC.

## 7. Summary

The purpose of this discussion on the MAGTF-System-generated cargo data was to emphasize the fact that MAGTF data was designed to include every cargo category required to support the MAF in the amphibious assault. The AE totals obtained from MAGTF data are larger than previously thought, since earlier estimates were based on older lift expressions. The lack of information necessary to state the complete lift expression in former years led to the planning and execution of the MAGTF Project. Proposals have been submitted to HQMC (Code RDS) for

improving MAGTF processing time and to correct all known MAGTF data base deficiencies. After using the MAGTF System extensively during the current project, it is possible to state that the system was adequately designed for content, and with proper maintenance on a day-to-day basis, the data base will easily reach an accuracy of over 95 percent.

Having discussed the data to be used throughout the computational portion of this report, the next subject to consider is the material adjustments recently completed and proposed for future changes to unit material that have and will have an impact on MAF lift requirements.

#### C. Materiel Adjustments

This section will present findings relative to the possible effect on the MAF lift cargo requirements of certain material adjustment that may be made in unit material. Research into six areas was conducted to determine these effects, if any. The data from the research will be presented in this section, with the effects on overall MAF lift included in Section VII.

## 1. T/E Reductions

One of the first research tasks conducted in the study was the examination of a sample of T/Es selected from FMF units to determine the existence, if any, of nonessential equipment. Results from this effort were planned to be used for making inferences relative to other units of the MAF. The term "nonessential equipment" was interpreted to mean equipment no longer required to support any current or anticipated mission or function, either by the quantity of the item on the T/E or the lack of usefulness for any reason. The purpose of this task was to determine if any significant reductions of materiel were possible in support of the first objective of the study, namely, to find areas where feasible reductions of materiel were possible without reducing operational readiness or sustainability of units in the MAF.

The units listed in Table V-4 were those selected for analysis.

Table V-4
UNITS SELECTED FOR T/E REDUCTION ANALYSIS

Unit T/E	Description
м1038	Inf Bn
M1128	Arty Bn
M1758	Serv Bn
м1658	Mt Bn
м3233	Mt Maint Co, FSR
м3243	Engr Maint Co, FSR
м3253	Comm/Elect Maint Co, FSR
м8813	H&MS
M8847	VMFA

This task was conducted by making visits to units in I MAF at MCB, Camp Pendleton, and MCAS, El Toro, California, and interviewing knowledgeable personnel in each of the type units listed above. A discussion was held with those personnel on each item of the latest T/E (just received during April 1975) for the first four units visited. Results achieved during the visits to the first four units indicated that general discussions of T/E essentiality would be adequate when visiting the other units. Personnel interviewed were commanding officers, operations officers, logistics officers, maintenance officers, and division, wing, and MAF staff personnel. Enthusiastic support of the research task was evidenced by all personnel contacted.

Initially, results expected from this task were lists of items to be deleted from unit T/Es. With one exception, the unit T/Es analyzed

contained only insignificant numbers of items that could be considered nonessential. In every unit visited, the existence of T/E review efforts was evident from the precisely stated usefulness of all items contained in T/Es. Actions had been or were in the process of being taken to update T/Es to reflect exact requirements. The unit whose T/E review produced significant material reduction recommendations was a maintenance company originally configured to separate into more deploying detachments than experience ever required, thus additional sets of test and repair equipment were included beyond any current support requirements. No reduction actions were forthcoming from that unit for two reasons. First, the unit never deploys as a complete company and is therefore a tailored detachment when part of a MAGTF. Second, the implementation of the new CSS organizational structure eliminates this unit as a source of detachments for future troop lists.

The information obtained in conducting this task failed to provide grounds for obtaining permanent T/E reductions from which lift requirements could also be reduced. The important fact gleaned from this task was that many items in the T/E were useful in some types of operations and not needed in others. If any item had a use in at least one possible circumstance, then it was not considered for elimination. Since the controlling factor in this analysis was the preservation of operational readiness and sustainability of the unit, these factors would be unaffected if items not needed for an operation were excluded from the unit load. The eliminated items could be left in garrison or be included in the landing force supply of the AFOE, to be redistributed after D+5 at some convenient time. A detailed analysis3 of combat essentiality conducted at NWRC/SRI found unit T/Es to be comprised of three mission essentiality categories. These are primary, secondary, and tertiary missions. A manageable latitude of what equipment to include in the unit load of an AE unit faced with constrained loading problems was

found to exist. A collateral consideration is that any equipment eliminated from the unit load embarked in assault shipping would be unavailable to the unit only from D-Day to D+5, plus unloading time if it were included in the AFOE cargo. These findings led to the development of a systematic procedure to eliminate T/E items from a unit in a constrained assault shipping environment based on a criticality assessment of the T/E. The criticality factors used in such a procedure would be based on the mission essentiality categories previously discussed. These findings, along with the fact that units usually deficient to some degree in T/E items for a variety of reasons are still capable of accomplishing their missions, substantiate the approach to solving the problem of deciding how to configure the AE of the MAF or MAB or even a MAU when less assault shipping is available than lift requirements for a selected troop list. A solution procedure consisting of mathematical models designed as a computer assisted decision aid is presented in the study, i.e., the development of a materiel weight and cube control process. It was considered necessary to determine the effect on the lift requirement of the notional MAF used in the study from the introduction of new materiel into the T/Es of units contained in the MAF troop list. The results of this research are presented in the next section.

## 2. New Materiel

The time frame of this study includes the period to 1980. Materiel changes are constantly in progress within the Marine Corps. This incorporates upgrading equipment to stay abreast of the latest technological developments, which is in line with the third objective of the study. Results from the task were only partially successful due to a lack of available data. A task was planned to determine the difference in lift that could be expected from introducing the planned TAM<sup>4</sup> items into the T/Es of units. Precise results were not obtained from this

effort because of the small number of planned items for which embarkation data was available and the high cost of obtaining these limited results from large computer tape files. However, an analysis of the trend in lift requirements for planned items was conducted without consideration of the quantities to be included in T/Es. This analysis consisted of comparing planned (P) TAM items with those TAM items being replaced in T/Es. The comparison included only the cube for bulk loaded items and square feet for square loaded items. Table V-5 lists the TAM numbers and the cube for the replacement TAMs and the P TAMs. Information extracted from the IDF indicated that one P TAM was often replacing more than one replacement TAM. Results from this analysis show an increasing trend in cube. An increase of 2272.36 cubic feet was obtained from the data. Table V-6 shows a decrease of 582.19 square feet for square loaded items. The actual effect of planned items would be determined only after entering into the MAGTF data base the exchange of TAMs for each affected T/E. This procedure, however, is included in the weight and cube control program presented in Section VIII.

However, considerable data was found to be available supporting an analysis of introducing a new family of shelters into T/Es of many units in the notional MAF. A task was conducted that caused the data for the new shelters to be entered into the MAGTF data base, along with the elimination of replaced TAM items. With completion of these efforts, a separate run of the MAGTF Program was obtained, which provided the necessary information to determine the difference in lift requirements of the MAF with and without the new shelters. Table V-7 presents these results. Examining this data reveals that an insignificant percentage increase in measurement tons of bulk cargo, and an approximately 1 percent increase of square feet of square loaded items resulted from the new family of shelters, which added 13,900 square feet of shelter space to the affected units.

Table V-5

COMPARISON OF PLANNED TAM ITEMS WITH REPLACEMENT TAMS
FOR BULK LOADED ITEMS

Replaceme	nt TAMs	P TAMs		
TAM No. C	ubic Feet	TAM No.	Cubic Feet	
A0120	3	A0122	1.60	
A0490	2	A0493	0.20	
A0893	1	A0645	0.17	
A1180	1 )	A1195	1.55	
A1190	4 ∫			
A1420	11	A1415	5.65	
A1435	552	A1436	545.8	
A1460	2165			
A1505	89	A1500	627.7	
A1507	89			
A1480	82	A1503	4131.0	
A1800	1	A1815	12.25	
A2020	8	A2065	2.81	
A2380	3 )	A2505	1.66	
A2490	6 ∫			
A3000	1	A1225	1.53	
A3060	10	A3062	1.14	
в0270	33	в0325	0.30	
Total	3061		5333.36	
Difference	2272.36			

Table V-6

COMPARISON OF PLANNED TAM ITEMS WITH REPLACEMENT TAMS
FOR SQUARE LOADED ITEMS

Replacement TAMs		P TAMs	
TAM No.	Square Feet	TAM No.	Square Feet
A1350	44	A1360	176.19
A1900	70	A1935	59.0
A1940	59 ∫		
A2080	10	A1795	4.15
A2440	208	A2441	88.8
в0400	141	в0399	495.0
в0410	126		
В1020	34	B1021	21.75
В1900	402	В1925	348.0
В2460	184		
D0900	118	D0915	122.22
D1000	132		
E0605	383	E0692	383.02
E0690	258		
E1360	398	E1377	304.68
Tota1	2576		1993.81
Differenc	e 582.19		

Table V-7

COMPARISON OF CUBE AND SQUARE OF EXISTING SHELTER SYSTEM

WITH REPLACEMENT SHELTER SYSTEM

	Existing Shelters (sq ft)	Replacement Shelters (sq ft)	Increase (sq ft)	Percent of Increase	Replacement* Shelters (cu ft)
AE AFOE	32,100 18,700	40,600 24,100	8,500 5,400	26.5% 28.9	1,900 600
MAF	50,800	64,700	13,900	27.4	2,500

<sup>\*</sup> Shelters in existing system are square loaded and do not affect cube. The added cube shown is for the knockdown shelter, which is the only replacement shelter not square loaded.

Section VIII of this report presents a detailed discussion of the use of the MAGTF System to support the data for a materiel weight and cube control program. The shelter MAF MAGTF run is explained in more detail in that section. The methodology presented in Section VIII provides procedures to constantly monitor the direction amphibious lift requirements are taking from the proposed introduction of new materiel into T/Es of FMF units.

# 3. The New Combat Service Support Organizational Structure

The most important development occurring during the conduct of this study was the implementation of the new CSS organizational structure within the FMF. The data necessary to modify the notional MAF troop list with the new organization became available in automated form during November 1975. The TMR had the T/Os available earlier, but the availability of T/Es did not occur until the end of November 1975. The project was extended one month to provide the additional time to update the MAGTF data base in order to process the new CSS units through the analysis system of this study. The CSS notional MAF totals were presented in Section IV. Table IV-6 showed a reduction in lift requirements for the AE of the CSS MAF. This section presents a comparative analysis of the notional MAF with the CSS modified MAF. Table V-8(a) contains the AE of the CSS MAF, with the AFOE in Table V-8(b).

The effect of the newly structured MAF is illustrated in Table V-9, where totals for the AE and AFOE are compared for the notional and CSS notional MAFs. For the AE, a 6.4 percent reduction in bulk cargo, and a 9.6 percent reduction in square feet was achieved by restructuring the CSS units concerned. In the AFOE, a 79 percent increase in bulk cargo and a 1.5 percent decrease in square feet was observed. For the total MAF, a 41.3 percent increase in bulk cargo, and a 6.1 percent decrease in square loaded cargo was obtained. It should be

Table V-8(a) CSS NOTIONAL MAF ASSAULT ECHELON LIFT REQUIREMENT

Unit	Quantity*	MT <sup>†</sup>	Square <sup>†</sup>	Barrels <sup>†</sup>	PAS
M4623M	1	1758	328	824	161
M1096	3	186	4663	491	184
M1038	9	1014	4427	453	1230
M1128	3	1678	23016	1170	707
M4233	4				
M4233	4	906	6531	453	110
M1423	4	437	69	19	85
M1373X	4	71	1096	75	121
M4652	4	110	15292	1491	229
M1863X	1	99	1961	113	182
M1864X	1	345	12631	755	244
M1862X	1	136	23312	1038	223
M0701F	1	6482	2701	66	914
M4643F	1	667	5788	264	57
M1196	1	969	17364	1208	278
M1363X	1	2313	31214	1830	202
		0/7	14000		
M4237	1	847	16832	774	313
M4233	4	906	6531	453	110
M4903	3	35	605	38	120
M4907	1	96	6296	358	182
M3857X	1	398	10957	1245	287
M3853X	4	59	1001	112	102
	1		1901	113	103
M1427		115	6470	283	130
M8625X	1	172	3640	208	278
м1988	1	847	10486	925	1225
M1377X	1	118	788	94	131
M1867X	1	159	6562	340	173
M4654	1	226	11536	943	253
CMD-GP	1	1932	85992	3931	1984
M8612X	1	386	16526	1283	388
M8631X	ĺ	1005	13757	2302	244
M8640X	1	322	7935	943	197
M8621X	i	115	4831	491	115
M8615X	1	196	2870	301	158
M8937X	5	1217	3164	1811	241
M8943X	3	1291	3896	3057	298
M8970X	1	1150	2670	1189	292
M8964X	2	1109	2767	1245	269
M8968X	1	1305	3848	1472	217
M8859X	i	2001	5421	8642	363
M4112	1	664			
M4112		004	14469	736	225
M0601F	1	35	0	0	212
M0604F	1 .	668	11024	906	257
M4193	2	417	10497	528	177
M4201	1	67	2019	170	120
M4226	1	677	8661	528	177
M3223X	1	571	11275	491	280
M3233F	1 .	43	1455	57	125
M3447F	1	113	5832	358	337
M3343F	1	10	427	19	136
M3247F	1	127	1975	38	55
м3313F	1	2954	22677	0	140
M3323F	1	8	458	19	47
M3442F	1	1111	11201	472	202
M3243X	1	814	7131	189	191
M3253X	1	210	2741	75	190
M3851X	1	631	10957	1245	287
M0305F	1	212	11914	736	120
M0307F	1	24	571	38	82
M3751X	1	2220	7847	755	315
M3753X	2	108	8884	434	144
W001/#		100			
M8914X	2	180	4801	189	359
M8921	2	3238	17237	1283	390
M1985X	1	62	12516	415	143
M8821	2	87		208	

 $<sup>^{\</sup>star}$ Amounts listed are for one (1) unit; multiply by Quantity for total lift requirement.

 $<sup>^{\</sup>dagger}$ MT = 77624 Sq = 786926 Bl = 82848 Computed totals have been adjusted by removal of obsolete TAMs.

Table V-8(b)
CSS NOTIONAL MAF ASSAULT FOLLOW ON LIFT REQUIREMENT

Unit	Quantity*	MT <sup>†</sup>	Square <sup>†</sup>	Barrels <sup>†</sup>	PAS
M4722	1	17	919	200	16
M4392	1	114	2550	800	53
M0602F	1	30	0	0	66
M0605F	1	153	3086	500	77
M8820X	3	2828	9188	6800	333
M8620X	1	766	21116	7900	325
M8621X	2	189	4902	2700	115
M8710X	1	1892	12123	9500	515
M8715X	1	31075	85424	13900	503
M8714X	1	34099	44688	11600	377
N3751X1	1	2275	7919	4100	315
M3752X	1	1919	25159	1200	139
M3851X	3	301	1564	900	71
M4903	1	107	610	300	120
M4644X	1	17847	60770	5700	238
M4647X	1	1398	10083	2600	156
M3853X	1	110	1916	600	103
M3854X	1	191	2067	700	239
M3753X	1	3798	8955	2400	144
M3233N	1	978	10233	1100	158
M3757N	1	403	841	314700	82
M3755N	1	12723	32739	1035100	115
M4643N	1	16439	37103	8700	264
M3247N	1	2857	15185	6400	152
M3313N	1	427	46763	900	405
M3323N	1	1285	1285	400	142
M3343N	1	948	3827	900	268
M3447N	1	1037	12246	6600	255
M3442N	1	1733	9196	3800	388
M3444N	1	237	1571	600	179
M3445N	1	158	756	400	268
M3347X	1	584	7914	3300	379
M3443X	1	510	4932	1700	375
M0702	1	4893	53658	0	763
M0603F	1	13	0	0	4
M8712	1	62	831	200	49
M8652	1	674	11244	62500	122
M8780X	1	1368	3975	63400	419
M8813X	3	444	3923	1300	449
M8855	2	6185	7680	26500	227
M8857X	2	5443	7436	38200	347
M8848X	4	2884	5116	65000	377

 $<sup>^{\</sup>star}$  Amounts listed are for one (1) unit; multiply by Quantity for total lift requirement.

 $<sup>^{\</sup>dagger}_{\rm MT}$  = 189009 Sq = 648209 B1 = 2022400 Computed totals have been adjusted by removal of obsolete TAMs.

Table V-9
NOTIONAL AND CSS MAF COMPARISON

Assault Echelon							
	MT	Square					
Notional	82,906	870,856					
CSS Notional	77,624	786,926					
Difference	5,282	83,930					
Percent of difference	6.37%	9.64%					
Assault Follo	w-on Echelon						
	105 7/0	(50.076					
Notional	105,749	658,076					
CSS Notional	189,009	648,209					
Difference	84,000	9,867					
Percent of difference	79.43%	1.50%					
Total	MAF						
Notional	188,655	1,528,932					
	266,633						
CSS Notional	200,033	1,435,135					
Difference	77,978	93,797					
Percent of difference	41.33%	6.13%					

remembered that these figures represent ship loading requirements and do not include aircraft, boats, or bulk fuel. The significant reduction, of course, is in the AE, where the constrained assault shipping capacity exists. Section VII will include common user sealift assets required to lift the AFOE. There were no constraints identified for lifting the AFOE of the MAF, and no further work was done on the loading of the AFOE.

Because of the increase in bulk cargo of the CSS AFOE, a comparison of the AFOE by functional area was conducted to illustrate from which units the increase was derived. Units were compared by following functional areas:

- (1) Aviation
- (2) Motor transport
- (3) Medical/dental
- (4) Engineer, bulk fuel, bridge support
- (5) FSSG/FSR units
- (6) Aviation fly-in units.

Table V-10 contains the unit comparisons within the functional areas listed above. The information in the table clearly indicates where the cargo increases were obtained. Since each MAF is only notional, and a great many variations in troop lists are possible when preparing a force structure for a specific mission, the comparison presented here is not of too much importance. The complete reorganization of the CSS functions within units does not lend itself to a unit-by-unit comparison with the structure from which it was derived. Observing the troop list provided, one sees many detachments which could and would be organized differently than shown here when preparing for specific missions.

At the direction of the Study Advisory Committee, the CSS structure presented here was the basis of all analysis to be presented. No further mention of the notional MAF will be made in this report.

Table V-10

AFOE UNIT FUNCTION COMPARISONS

		Notional M	AF			CSS Notiona	1 MAF	
	Unit	Quantity	MT	Square	Unit	Quantity	МТ	Square
Aviation Function	M8820	3	14,136	58,317	M8820X	3	8,484	27,564
	M8620	1	3,204	23,664	M8620X	1	766	21,116
	M8710	1	2,998	18,589	M8710X	1	1,892	14,123
	M8621	2	1,162	14,026	M8621X	2	378	9,804
	M8715	1	15,065	32,696	M8715X	1	31,075	85,424
	MO/13	•	15,005	32,030	M8714X	1	34,099	44,688
	Total		36,565	147,292	107141			
	Difference		MT =	40,129	Sq =	55,427	76,694	202,719
Notor Transport Function	M4643	3	828	30,996	M4643N	1	16,439	37,103
	M4644	1	437	20 885	M4644X	1	17,847	60,770
	M4647	1	184	3,925	M4647X	1	1,398	10,083
	Total		1,449	55,806			35,684	107,956
	Difference		MT =	34,235	Sq =	52,150		
Medical/Dental Function	M4552	4	532	7,256	M3851X	3	903	4,692
	M4512	1	204	2,677	M3853X	1	110	1,916
	M4592	1	266	3,897	M3854X	1	191	2,067
	Total		1,002	13,830			1,204	8,675
	Difference		MT =	202	Sq =	5,155	1,204	0,075
			0.100	7 075			0.075	2 010
Engineer/Bulk Fuel/	M3333P	1	2,422	7,875	M3751X	1	2,275	7,919
Bridge Functions	M4343	1	7,056	32,597	M3752X	1	1,919	25,159
	M0306F	1	441	12,763	M3755N	1	12,723	32,739
	M0308F	1	1,470	11,707	M3757N	1	403	841
	M4353	2	732	17,090	M3753X	1	3,798	8,955
	Total Difference		12,121 MT =	82,032 8,997	Sq =	6,419	21,118	75,613
	Difference		M1 -	0,997	54 -	0,419		
FSSG/FSR/CSS Functions	M3213		102	1,695	M3233N	1	978	10,233
	M0313F	1	272	5,985	M3247N	1	2,857	15,185
	M0315F	1	271	16,381	M3313N	1	427	46,763
	M0323F	1	314	46,219	M3323N	1	1,285	1,285
	M0325F	1	1,767	2,569	M3343N	1	948	3,827
	M0327F	1	389	2,817	M3347X	1	584	7,914
	M3346	i	217	9,386	M3443X	i	510	4,932
	M3403	i	193	2,755	M3447N	1	1,037	12,246
	M3413	1	991	66,372	M3442N	1	1,733	9,196
	M0333F	i	2,466	10,136	M3444N	i	237	1,571
	M3443	i	251	4,531	M3445N	i	158	756
	M3447	i	4,695	21,624	MOHADIN		150	750
	M0304F	1	4,693	168				
	M0304F M0302F	1	16	107				
	Total		11,952	190,745			10,754	113,908
	Difference		MT =	1,198	Sq =	76,837		
Fly-In Function	M8780	1	1,650	7,642	M8780X	1	1,368	3,975
	M8813	3	2,472	26,097	M8813X	3	1,332	11,769
	M8857	2	10,538	18,834	M8857X	2	10,886	14,872
	M8849	4	9,572	27,540	M8848X	4	11,536	20,464
	Total Difference		24,232 MT ≈	80,113 890	Sq =	29,033	25,122	51,080
All Punchions	Avne		26 565	147 202	AVAI		76 604	202 710
All Functions	AVN		36,565	147,292	AVN		76,694	202,719
	MT M-1/D		1,449	55,806	MT Mad/Day		35,684	107,956
	Med/Dent		1,002	13,830	Med/Der		1,204	8,675
	Engr/Bulk/Br		12,121	82.032	Engr/Bu		21,118	75,613
	FSSG/FSR/CSS		11,952	190,745	FSSG/FS	r/CSS	10,754	113,908
	Fly-In		24,232	80,113	Fly-In		25,122	51,080
	Total Difference		87,321 MT ≈	569,818 83,255	Sq =	10,597	170,576	559,951
							10 100	90.050
	Unchanged Units		18,433	88,258	Unchang		18,433	88,258
	Comparison		87,321	569,818	Compari	son	170,576	\$59,951
			105 75	650 076			100 00-	
	Total		105,754	658,076			189,009	648,209
	Difference		MT =	83,255	Sq =	9,867		

# D. Analysis of Mountout/Prepositioned War Reserve Materiel (PWRM)

The final area of materiel adjustment having impact on the MAF lift cargo requirement is the mountout specified by the MAGTF data base automated service files. The IDF maintained by HQMC contains the CARF, which is the basis for computing supply classes IIW and VIIW. During 1972 a review of CARFs was conducted at HQMC (Code AO4) to determine those items whose CARFs could best be eliminated from the IDF in order to reduce the cost of replenishing mountout at the end of the Vietnam conflict. The elimination and reduction of the CARF for many TAMs was not made as a result of any user demand history. Because of the changes in the CARFs to the values currently in the TAM, a strong suggestion is self-evident that the mountout now held by the FMF may be inadequate for any future conflict. A comparison of the items having CARFs in the TAM published before 1972 with the current TAM is made in Table V-11.

Table V-11
PERCENTAGE OF TAM ITEMS (TYPE 1) HAVING CARFS

TAM Date	TAMs* with CARFs	Total*	Percent with CARFs
1968	891	1315	68
1974	218	1088	20

Does not include obsolete or reassigned TAMs.

Only 20 percent of the items have CARFs in the current TAM as compared with 68 percent in the 1968 TAM.

Because of the possibility of the current mountout failing to adequately support a deployed MAF, a research task was undertaken within the study to obtain a more realistic approach to computing mountout. If an increase in mountout occurs, a definite impact on the lift of the AE will result. Obtaining an estimate of the increased lift was the result desired from this material adjustment problem.

To properly plan, store, warehouse, and load supplies and equipment in mounting an amphibious mission, it is necessary to know expected consumption rates of end items. It is also necessary to know average unavailabilities (NORS rates).

Actual consumption rates will vary from nominal figures, even if the nominal figures are reasonably accurate averages over several scenarios, geographical locations, and weather conditions. Variation will occur because of chance events, unpredictable losses, repair service problems, possibility of substitution, etc.

Although replacement factors are shown in the literature, these factors may not be adequate for use in planning an amphibious operation. Close analysis of the application of these and similar replacement figures was therefore undertaken. There are several possible sources of information. These are reviewed below.

# 1. Previous Studies of Consumption Rates of End Items

In 1966 a U.S. Army study<sup>5</sup> of consumption rates of end items was directed towards computing the budget required to support an Army operation under any one of 15-20 scenarios at various parts of the globe. The scenarios included conventional warfare in several intensities. This particular Army study is important in computing variation in planning factors from one theater of operations to another. It does not

seem to be directly useful in addressing the problem at hand: expected consumption of class VII end items.

A second report<sup>8</sup>, as well as the data used in compiling it, was made available to the study team. Analysis of the data is included later in the present document. Although this report was intended to pinpoint fiscal requirements, the subject matter seemed at first to cover recoverable consumption data. Unfortunately, this data turned out not to be as useful as hoped.

A third previous study<sup>7</sup> tabulates and totals the shipments that passed through various Vietnam ports in the period 1966-1968. Combat strengths and combat active days in several logistic islands are also tabulated.

The important figure from this study is that consumption of class VII items by Marine Corps personnel averaged 5.18 pounds per manday of active combat. The corresponding figure for class II items is 7.83. This number varied over the logistic islands, being much higher in the Saigon zone, and somewhat lower in the Cam Ranh Bay and other logistic zones. Further discussion and application of this figure is given later in the present report.

#### 2. Application of Consumption Rates to Planning

## a. General Remarks

Even if a consumption rate were known with unassailable accuracy, it is not immediately clear how the rate should be used in planning an amphibious operation.

"Consumption rate" by itself usually denotes an average or expected rate; this rate can vary from day to day, and is, in the nature of things, a parameter that describes a stochastic (variable)

process. Random wear, unpredictable combat losses, incomplete maintenance, and unavailability of repair parts will all affect the complement or T/E that is operational during a combat exercise.

Because actual consumption is, in the nature of things, a variable rather than a fixed quantity, the strategy that will most efficiently guarantee combat readiness of a deployed unit is known to be a complicated one.

## b. Conventional Restocking Procedure

Conventional restocking and redeployment of end items dictates that replacement units be supplied at constant rates, these rates being equal to the wear rates of the end items. This strategy is an inefficient one for several reasons. In the first place, it assumes that all end items have equal criticality; this assumption is open to question. In the second place, it assumes that all end items will require replacement at precisely predictable times, which is not the case. And in the third place, there is no provision, under this stocking policy, for replacement of those items for which the safety stock in the objective zone is exhausted. At least, there is no provision other than emergency resupply. But emergency resupply is known to be rather expensive in terms of personnel effort and of shipping space.

#### c. Improved Stocking Procedure

As soon as it is realized that actual consumption will vary above or below the "expected consumption" of each end item, a more efficient stocking, shipping, and supply policy can be devised.

The first step, however, must be a reasonably useful knowledge of consumption (demand) rates. The CARF (combat active

replacement factor) listed in the present TAM is zero for a large number of end items, and no criticality is listed.

The absence of a criticality factor is not surprising, since the criticality of any piece of equipment does depend on the function assigned to the military unit that is consuming the equipment. The statement that the CARF is zero is more questionable. The CARF may vary from military unit to military unit, but it is seldom zero.

# 3. Analysis of Data From HQ FMFPAC

### a. Description of Data

The data in the HQ FMFPAC report<sup>6</sup> consists of computer tapes, together with supporting documents. The computer tapes contain records of 900,000 requisitions that were processed at FSR and FLC during the period 1968-1970.

Each record shows FSN, requesting military unit, quantity requested, date (month) and unit price. The supporting documents show the nature of the requesting military unit (defined in the computer tape by a numerical code); these documents also show the combat status of the military unit.

The TAM number is not shown, nor is the square, cube, weight, NML indicator, square load indicator, or quantity in T/E.

MAGTF data base. On the other hand, this data base does not show unit price. Since the unit price is now available, and can be used for certain other routine statistical analysis and correlations, it is suggested that the unit price be incorporated into the MAGTF data base as a permanent field in the EQUIP record.

### b. Attempt to Extract Consumption Rates

The first step in the analysis was to extract those requisition records that pertain to the TAMs of interest. This extraction was carried out by the use of an FSN-TAM conversion code prepared for a previous project. It turned out that several FSNs correspond to the same TAM; even more surprising, more than one TAM corresponded to the same FSN in some cases.

The next step was to organize the data according to the T/E of each of several military units. The military unit code in the HQ FMFPAC tapes differed from the military unit code used in authorized Marine Corps documents. The conversion key was furnished by SRI, based on knowledge of Vietnam troop organization.

The last step was to take out demand and divide the demand by the quantity in the T/E. All this information had to be merged with another file that contained square, weight, cube, etc., (EQUIP File). The ratio of crude demand to quantity in the T/E, TAM by TAM, was called normalized demand, or specific demand.

It had been hoped that there would be some correlation between this demand rate and unit price. No such meaningful correlation was found, in spite of heroic attempts. (Such a correlation is known to exist under other field conditions.) The absence of correlation in the present data can be explained in several ways: demand was a function of what was available rather than what was actually needed; demand data records were grossly incomplete.

Both these explanations are reasonable, and, to a certain extent, both of them are true. On the last point, the supporting documents specifically mention the fact that many requisitions have been lost and are unrecoverable. On the first point, although demand rates were by no means flat over all items, they did not vary much.

In any case, the best information that can be gleaned from the HQ FMFPAC data is that the expected demand rate for an A TAM is to be estimated by taking an average figure; the table following shows the final conclusion of the data manipulation that was performed.

(Caution: since the data is incomplete, the tabulated numbers are low. The magnitude of the error is discussed later in this report.)

Table V-12

DEMAND RATES FOR CLASS VII SQUARE LOADED ITEMS (Average Figures 24-Month Replacement Factors)

No. of TAMs Averaged	TAM Category	Demand (24-month)	Average Unit Cube	Average Unit Price
107	A	.07066	43.82	3226.07
37	В	.07357	87.20	1790.45
402	C	.06123	5.26	144.30
102	D	.06130	171.23	1429.35
93	E	.05173	16.41	1184.90
741 (total)				
Mean		.0620	39.17	959.54

Note: Items included are only those (1) for which information could be obtained, and (2) that are included in the T/E of the three military units M1988, M1038, M4112. (Other TAMs are not included in these average figures.) Additional details concerning the analysis are given in Appendix H.

## 4. Computation of Mountout Adjusting Factors

## a. Analysis of the PRC Study

- 1. The Raw Consumption Rate. As stated above, the PRC study indicates a consumption rate of 5.18 pounds of class VII items, i.e., 4.17 for square loaded and 0.10 for nonsquare, and 7.83 pounds of class II items per man-day of combat in the Vietnam conflict, 1966-1968. This figure was obtained from on-the-spot analysis teams; these teams had access to shipping information and were thus able to include all supplies that passed through the ports. Internal checks of the data, comparisons with performance of truck companies that off-hauled equipment, and variation from one logistic island to another show that the information is self-consistent.
- 2. Reduction of the Raw Consumption Rate. To reduce the data to the form needed for planning purposes, it is necessary to know the T/E being supported. This is the weak point in the present analysis; the actual T/E deployed in the field at that time cannot be determined. It was probably somewhat larger than current T/Es.

Another judgmental adjustment has to do with the relation between quantities shipped and quantities consumed. The amount shipped, or even the amount received, is not necessarily equal to the quantity consumed. In fact, it is known that large surpluses remained at the end of the Vietnam conflict. However, if these surpluses were only a fraction of the total shipped per year, the adjustment that is required to take account of the remaining surplus may not be overwhelming.

The figures 4.17, 7.93 pounds/man/day were reduced to pounds/man-day demand figures for TAM items in the following fashion. First the total weight of all class VIIW square loaded items and class IIW and VIIW

nonsquare contained in mountout computed by the MAGTF System for the CSS notional MAF were computed. Next, the total personnel strength was used to compute the number of combat man-days in a 15-day period as specified for the AE. Dividing the total weight of demand as computed for 15 DOS, and the 4.17, 7.93 values by the weight of mountout currently computed, resulted in an adjustment factor, as shown in Table V-13, of 39. This means that the mountout computed from the current values of the CARF and the float is 39 times too low when compared with the Vietnam usage data contained in the relevant study. The total weight used to obtain this factor includes the operational readiness float for the same supply classes.

Table V-13

MOUNTOUT ADJUSTING FACTOR CALCULATION: VIETNAM DATA
(Classes IIW, VIIW Nonsquare)

Data Source	Mountout Weight
MAGTF	46,099*
Float	106,943
Total	153,042
Vietnam	4,201,790†
Adjusting Factor	39

<sup>\*</sup>Data obtained from notional MAF:
MAGTF summary.

Value obtained from:

Wt = 7.93 x 35,324 x 15
7.93 = 1b/man/day
35,324 = personnel strength AE
15 = DOS for AE.

The figure used for the float was one-third the total for the entire MAF. For supply class VII square, again including the float, the factor is 1.09, as shown in Table V-14. The sizeable float embarked, when included in these calculations, reduces the factor from 1.4. The float was included since both mountout and the float are available to supply the total demand and should be included in the comparison with total Vietnam demand.

Table V-14

MOUNTOUT ADJUSTING FACTOR CALCULATION: VIETNAM DATA (Class VIIW Mountout)

Data Source	Mountout Weight
MAGTF	1,564,384*
Float	465,387
Total	2,029,771
Vietnam	2,209,516 <sup>†</sup>
Adjusting Factor	1.09

<sup>\*</sup>Data obtained from notional MAF: MAGTF summary.

The adjusting factors computed here were used to determine their effect on the AE lift problem when loading in a constrained assault shipping environment. Results from this analysis are presented in Section VII.

<sup>†</sup>Value obtained from:

Wt = 4.17 x 35,324\* x 15

4.17 = 1b/man/day

35,324\* = personnel strength AE

15 = DOS for AE

# b. Middle East War Adjustments

The consumption data used here to evaluate the adequacy of the current mountout computations, of course, was based on the Vietnam conflict. Usage rates observed from the Middle East war might have added additional insight to the shipping requirement needed to lift the square loaded mountout cargo category—if such data had been available. General information concerning that conflict suggests that high loss rates may be expected in the class VIIW square category when a combat force engages predominant mechanized forces. An arbitrary adjusting factor will be used in Section VII to indicate the additional mountout lift requirement needed to support much higher loss rates.

## c. Adjustments From the 1968 TAM

After examining the difference in the number of TAM items having CARFs between the TAMs of 1968 and 1974 previously presented, it was also necessary to compute an estimate of the effect of using the 1968 TAM CARFs to compute mountout on AE lift requirements. It was originally planned to enter the 1968 CARF values into a special MAGTF data base version, and rerun the MAF. This method was not possible due to excessive costs and the lack of opportunity to process this run on the NPGS computer. It was decided that the accuracy obtainable from using an approximation method was sufficient to demonstrate the effect on amphibious lift. The procedure used was to select a small sample of units found in the AE and compute an adjusting factor derived from the difference in the weight of mountout between the 1968 and 1974 TAM CARF values. A value of 2.38 for an adjusting factor was obtained. Table V-15 contains the units and values from which the adjusting factor was derived.

In summarizing the PWRM analysis conduced during this study, the original intent was to compute recommended values for the CARF from combat usage data. Although this task was accomplished, the observed problems with the data prevent the recommendation to use the computed CARFs for mountout calculations. This task establishes a requirement for further study of the mountout computational problem.

Table V-15

VALUES USED TO COMPUTE A CARF ADJUSTING FACTOR FROM THE 1968 TAM

Unit	1968 TAM	1974 TAM	Ratio
м8615	24,599	8,203	3.0
м1038	19,015	3,521	5.4
M4112	36,688	21,980	1.67
Total	80,302	33,704	2.38

The adjusting factors obtained from the Vietnam data contained in the PRC study, the adjusting factor computed from the 1968 TAM, and an arbitrarily selected adjusting factor for high combat loss rates reflecting Middle East war effects are used to emphasize the lift requirement generated from more realistically computed mountout.

## E. Summary

This section has provided a description of the data and its sources to be used for conducting the analysis of the constrained amphibious lift problem. The MAGTF System data was presented, along with material adjustments that will have an effect on the complete lift requirement for a notional MAF. The next section will present a description of a computer assisted model that generates and uses the data presented herein.

#### F. Conclusions

As a result of the analysis presented in this section, the following conclusions were developed.

(1) The overall capability of the MAGTF System and the continuous requirement for lift data from all

categories of cargo available from this system justifies the expenditure of effort to conduct the further improvement of the MAGTF Program and continued updating of the MAGTF data base. (Page V-15.)

- (2) The MAGTF System generated lift expression for the MAF is the most current and accurate source of this specialized data in existence. (Page V-2.)
- (3) The known errors in the MAGTF System data cause an understatement of total lift requirement. (Page V-9.)
- (4) The T/E reviews conducted by units in the FMF during this study did not identify an accumulation of significant quantities of nonessential equipment. (Page V-16.)
- (5) The combat active replacement factor (CARF) used to compute PWRM for mountout and mountout augmentation is not currently based on realistic expected consumption rates for supply classes IIW and VIIW. (Page V-30.)

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- 7. L. Christensen, L. Genney, N. Ketlner, F. Licord, M. Pollack, and R. Tate, "Developement of Logistics Planning Factors in South Vietnam (LOG PLAN V)," PRC-1240, Planning Research Corporation, Los Angeles, California (March 1969).

VI THE CONSTRAINED AMPHIBIOUS LIFT ANALYSIS SYSTEM (CALAS)

## A. General

In the previous two sections of this report, the nature and extent of the amphibious lift problem were presented. Briefly, the extent of the problem was defined by comparing the capacity of amphibious assault ships expected to be available during the period to 1980 with a realistic statement of lift requirement computed from a notional troop list for an assault echelon component of a MAF. The nature of the problem was derived from the four principal areas controlling cargo totals and the flexibility obtained from incrementally phasing the arrival of units ashore in the objective area. The data presented in the statement of amphibious lift short fall showed that only 61 percent of the bulk cargo and 9 percent of the square cargo could be loaded into the 59 ship force for the troop list comprising the AE of the notional MAF. The first two objectives for the study indicate the nature and extent of the lift problem by stating the requirement of determining the feasibility of reducing landing force materiel for embarked units, and by reducing lift requirements from phasing units ashore, when possible, from the AFOE embarked in nonassault shipping.

The approach pursued to solving the amphibious lift short fall problem within the descriptors contained in the study objectives was to analyze the problem from the four principal areas controlling cargo totals. As previously stated in Section IV, those areas are:

- (1) Troop list of AE
- (2) Selection of AE units for phasing ashore
- (3) Days of supply for mountout
- (4) T/E lift requirement.

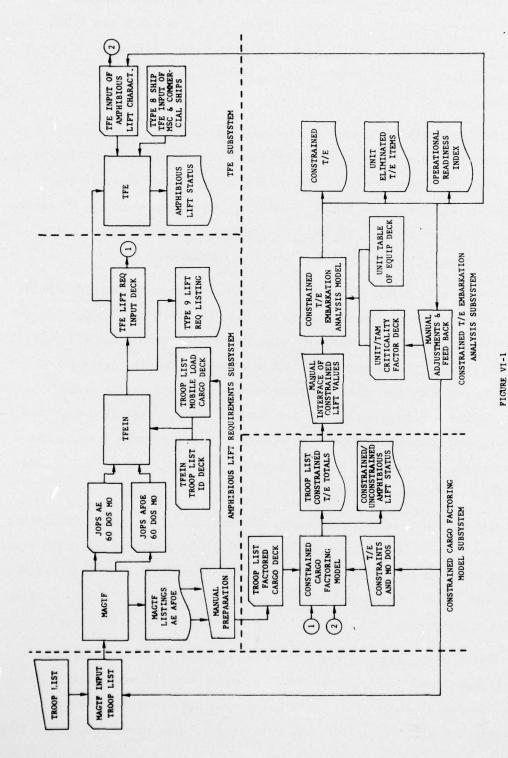
A change in the number of amphibious ships will affect the problem (if feasible).

To find a solution to this difficult problem, a series of models was developed from very practical approaches. These models provide the means for analyzing each principal aspect of the problem as field commanders would be required to do, utilizing subjective judgment along with a systematic analytic technique designed within a series of computer programs. In effect, a solution procedure has been developed that functions as a computer assisted decision aid to the commander for solving the constrained amphibious lift problem within the context of an assigned mission. This section provides a description of the solution procedure, which has been called the Constrained Amphibious Lift Analysis System (CALAS). Each subsystem will be explained, along with the overall system functioning process. References will be made to appendices that contain technical descriptions of the mathematical models designed within the supporting computer programs comprising the system.

#### B. CALAS Description

Figure VI-1 contains a flow chart of CALAS, which will be repeatedly referred to in this section. Application of CALAS begins when the commander has been given a specific mission for which a troop list has been developed. The first step is to determine the lift requirement for the selected force. The number of days of supply for the AE and AFOE, and the configuration for loading fuel requirements must also be specified, along with any special material for the geographic location of the objective area. When these decisions are made, CALAS may then be employed.

CALAS consists of the four subsystems shown in Figure VI-1. A brief description of each subsystem is presented here.



CONSTRAINED AMPHIBIOUS LIFT ANALYSIS SYSTEM (CALAS)

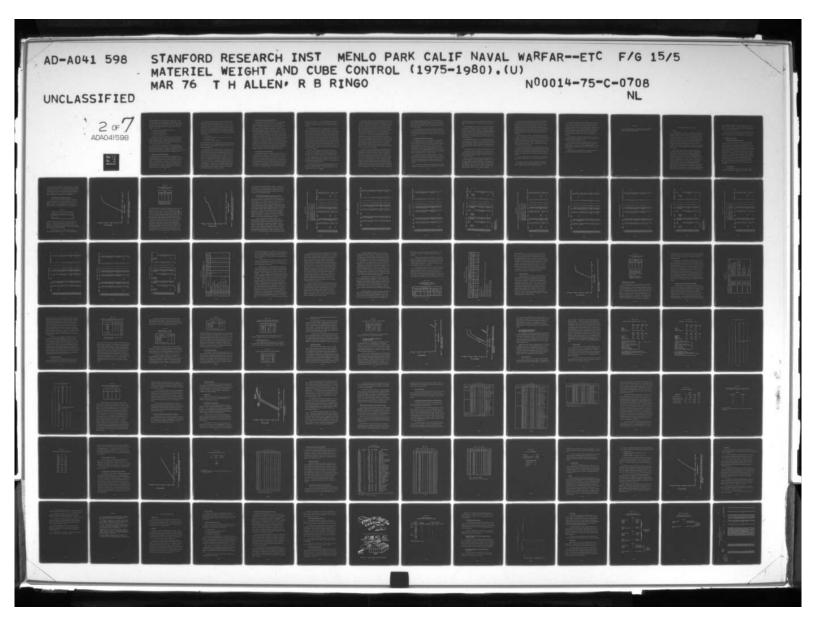
The amphibious lift requirements subsystem provides the amphibious lift requirements for the specified troop list from MAGTF and TFEIN programs. Automated data providing the precise cargo categories of personnel, bulk cargo, square loaded cargo, and bulk fuel are obtained from this subsystem.

The TFE subsystem receives the cargo data, called the movement requirement, for each unit of the AE, and, with the added input of the amphibious lift characteristic card deck of amphibious assault ships available, simulates the loading/unloading and movement to the objective area. In so doing, the lift short fall, i.e., cargo not loaded, is obtained along with the time required for the movement.

When a lift short fall does exist, the Constrained Cargo Factoring Model subsystem uses the same input as the TFE subsystem, along with the factored cargo deck for each unit, the constraint values for T/E reduction, and the DOS for the AE mountout, and systematically reduces cargo by specific category for the constraint values provided to the program. The output of this subsystem is the listings of constrained T/E totals and the constrained/unconstrained AE lift status. This subsystem applies the constraints and loads the ships, computing the lift status, i.e., lift short fall for each constraint.

The Constrained T/E Embarkation Analysis Model subsystem determines the T/E items to be included and excluded from the lift requirement based on the criticality factors assigned to each item of the T/E. An operational readiness index is computed for all constraints applied. This subsystem prints a constrained T/E and operational readiness index as output.

Based on the input troop list, days of supply, shipping available, and assigned constraint values, a shipping short fall may still exist in spite of the T/E reductions. For each constraint, the list of items selected for elimination from the unit load is also presented. With this



information available to the commander and his staff, analysis of the various options may now be made using CALAS. Referring again to Figure VI-1, the feedback lines in the flow chart represent the courses of action possible. Because there is a constraint value below which computed T/E reductions are unacceptable, alternative courses of action must be considered. These are to:

- (1) Increase the number of amphibious assault ships
- (2) Reduce the DOS for mountout
- (3) Increase the constraint value
- (4) Reduce the units in the troop list.

In addition to these major options, the criticality factors assigned to the T/E items of the unit may be varied according to the judgment of the unit commander concerned. By varying the options that are input to CALAS, the most operationally ready force possible may be determined within the overall constraints facing the commander.

The brief discussion of CALAS presented above should present the general concept of how the system functions. In the following paragraphs, a more detailed explanation of the subsystems is provided, with the technical presentations included in the appendices. An application of a constrained loading problem using the CSS notional MAF data constitutes Section VII.

#### C. Amphibious Lift Requirements Subsystem

Referring to Figure VI-1, an input deck for the MAGTF Program is prepared describing the AE and AFOE, as previously mentioned. Instructions for preparing the MAGTF input deck are found in the MAGTF System "Users' Manual." The MAGTF Program is then processed, which provides as output a complete listing of the units in the AE and AFOE. Appendix B contains two sample MAGTF AE unit listings. A summary for the AE and AFOE is available from the run. The MAGTF Program also punches a JOPS card file as an automated output for both the AE and AFOE.

The JOPS card deck then becomes the input to a computer program called TFEIN. An additional input deck consists of a troop list identification (ID) deck and a mobile loading cargo deck. There is one card in each deck for each unit. The purpose of Program TFEIN is to read the JOPS deck for each unit, combine the data from the ID and mobile loading decks, and punch a movement requirement card for each unit. The movement requirement card is formatted for input to the Transportation Feasibility Estimator Model<sup>1</sup> (TFE), to be explained later. The data elements contained on this card are:

- (1) Total personnel
- (2) Bulk cargo in measurement tons (40 cubic feet = 1 m. ton)
- (3) Bulk fuel in barrels
- (4) Square feet of square loaded items.

Additional data elements are included on this card for specific requirements of Program TFE. The data elements listed above also serve as input to the Constrained Cargo Factoring Model, facilitating a dual use of the movement requirement card.

The JOPS cards, having been designed for JCS specifications, are not directly representative of AE unit lift quantities. JOPS cards contain total cargo without regard to mobile loading, and mountout is fixed to the days of supply (DOS) specified for the MAF. The parameters used for computing lift of the notional MAF are listed in Section V. From that list, one observes that the DOS for mountout of the MAF are 60, and for the AE 15. It became necessary to include an algorithm to reduce the 60 DOS to 15 for AE units. The problems of converting the cargo totals to 15 DOS are more complicated than may be expected at first inspection. The development of the necessary conversion mathematical model is presented in Appendix D. Program TFEIN also produces a printed listing of the movement requirements for each unit in the force. An explanation of the TFEIN Program is also included in Appendix D.

## D. Transportation Feasibility Estimator Model (TFE)

The TFE Program was obtained from HQ FMFPAC to provide an automated means of determining the lift status, given the principal inputs of movement requirements and the amphibious assault shipping capacity. TFE, however, is a simulation computer model that determines the gross movement feasibility of a projected plan of deployment. Specifically, given the movement requirement, the assault shipping, the capacity of the ports handling the loading and unloading, and the geographic locations of the ports of embarkation and debarkation, TFE will determine the time required to complete the movement of the materiel. Of the many listings provided by Program TFE, the significant output for this study was the cargo quantities not lifted by the ships provided as input. The ship input data was presented in Section IV. The format of the shipping data presented there conforms to the TFE Program. Because of the need to move the AE and AFOE from the port of embarkation to the amphibious objective area, with no turnaround shipping permitted, the extensive simulation capabilities provided by Program TFE were not needed. A loading simulation was then included in the Constrained Cargo Factoring Model. Sample outputs from the TFE Program are found in Appendix C. Amphibious lift status is contained in the TFE output.

#### E. Constrained Cargo Factoring Model (CCF)

After inspecting TFE output, the shipping short fall for the cargo of the notional MAF's AE is defined. The CCF model provides the next stage for CALAS, where the solution procedure begins to function. As evidenced in Figure VI-1, there are four inputs to the CCF Model. These are the same movement requirement deck and amphibious ship lift capacity deck used in the TFE Program, the troop list factored cargo deck, the values of DOS for mountout, and the constraints to be used for reducing the unit's T/E. The CCF model is a computer program that loads the movement requirements for each unit into the ships provided in an unconstrained mode, while

printing the lift short fall. It then constrains the amount of cargo to be loaded for each unit for a variety of constraint values, printing the troop list of constrained T/E totals and the constrained/unconstrained lift status.

The CCF model functions within the following scheme. The data provided to the model for each unit is in measurement tons (MT) for bulk cargo and square feet for square loaded cargo. Using the cargo factoring deck, these totals are factored into T/E totals, which include only supply classes IIW, VIIW (nonsquare) and IV; mountout of all nine supply classes, and class VIIW square loaded totals. For aviation units a further factoring is done for bulk cargo with respect to classes IIA and VIIA nonsquare, VIIA square loaded, and the IMA square loaded items. Now that the unit's cargo is factored into categories providing the logical areas for reduction, further constraints are then applied by multiplying the specific constraint by the T/E total for bulk cargo and by the T/E square loaded total. Since for classes IIA and VIIA, totals for units are defined to be initial issues, plus 90 days mountout, constraints are not applicable to these categories and they are not reduced.

Because of a decision made by the Study Advisory Committee, IMA equipment is eliminated by the model for loading into assault shipping, i.e., LPHs, LHAs. The assumption is made that this equipment will be furnished by the LPHs and LHAs, allowing it to be loaded into AFOE ships.

Mountout adjustments may be made by changing the DOS for the AE. Since the mountout cargo is factored and was computed for a specified number of DOS, reduction of the cargo quantity to 1 DOS is done. This amount is then converted to the desired number of DOS.

When all adjustments are made to the factored cargo quantities, new totals are then obtained by adding the factored parts together for both bulk cargo and square loaded cargo. The ship loading operation is then conducted and the next unit is processed.

The constraint values used for T/E reductions are given in decimals. A constraint value would be .90, indicating a 10 percent reduction in the T/E totals. Constraints were not applied to the same degree for all units of the AE. By the use of codes, constraints were not applied to detachments that were formed for performing a specific function. Constraint values used to reduce T/E cargo for combat units are assigned to be onehalf the overall constraint for the AE. Combat support units generally were constrained by the same value as the overall constrained value. Certain combat service support units were constrained twice the overall This variation in constrained values provides a reduction value. weighted constraint for units in the AE according to their mission or function. The values assigned to the units in the notional MAF were arbitrary and could be changed by the user to satisfy his judgment in accepting the ultimate list of items eliminated from the T/E as determined by the constrained T/E embarkation model. The decision as to whether a detachment should be constrained can also be made at the discretion of the user of CALAS. A change in the code for the detachment will include the unit in the constraint calculations.

An additional feature of the CFF Model is the reallocation of square stowage space to bulk cargo when excess square space occurs through constraining the total square to be loaded. The nature of the cargo data indicated that such a feature was desirable because of a tradeoff that exists between eliminating some big item and loading more smaller items. Since there are many large square loaded items, such as trucks, included in AE cargo, and since the decision as to what to include or eliminate applies only to the period between D-Day and the arrival and specific unloading of the AFOE, options do exist as to which vehicles or engineer equipment to include in the AE units. Results obtained from analyzing the CSS notional AE cargo within CALAS, presented in Section VII, will demonstrate the usefulness of this feature. When excess square loaded space is

obtained during a constrained loading run, the space is reallocated to bulk cargo by assuming two-pallet high stacks. New totals for bulk and square loading are computed for the shipping capacity, and the units are reloaded for the same constraint value. A new value for shipping short fall is then obtained.

The output listings of the CFF Model are then used to provide the exact space reductions for the T/Es of each unit, which are then used by the Constrained T/E Embarkation Analysis Model to determine the most operationally ready mix of equipment for the reduced space allotted to the T/E of the unit.

# F. Constrained T/E Embarkation Analysis Model

Each standard military unit in the Marine Corps has a prescribed Table of Equipment (T/E) detailing the equipment it is authorized to maintain. The ability of a unit to perform its function(s) is predicated on the availability of the major items of equipment listed in its T/E. The standard T/E of a unit assumes that there will be no shortage of shipping space in which to load the authorized equipment; but if there is such a shortage, two questions immediately arise: (1) Can the operation be successfully mounted? and (2) What part of the full strength T/Es should be carried by each unit in the assault echelon.

The problem addressed in the following paragraphs is: Given that shipping capability is limited by a fixed constraint (cube or square), what is the optimum T/E that should be loaded? It follows that when there is a volume or square constraint on shipping, the objective is to minimize the loss in efficiency caused by the decrease in equipment and supplies.

For the purposes of the Constrained T/E Embarkation Analysis Model (CONTEAM), it is assumed that for each unit a known amount of constrained

cube and square storage is given from the Constrained Cargo Factoring Model. The problem remaining is the optimal allocation of this scarce space.

For the CONTEAM model only the class IIW and class VIIW TAM items are constrained. However, a constraint can theoretically be applied to any other class(es) of supply, if desired. This procedure produces a concrete, pared down T/E that is smaller than the standard published T/E for a unit. The output from the CONTEAM model shows for each unit's T/E the class IIW and class VIIW TAM items to be omitted from the assault echelon; these will be carried by the assault follow-on echelon or later replenishment phase.

The CONTEAM model first fills the available space with a "skeleton T/E" consisting of those items that will be absolutely essential during the interval between the landing of the assault echelon and the arrival of the assault follow-on echelon. The balance of the shipping space is then filled with T/E items (TAMs) according to their importance to the unit.

The CONTEAM model operates within the following systematic design.

The importance of an item of equipment to a unit's mission can be derived by relating its usage to specific functions of the unit, and, in turn, determining the relative importance of the specific functions to the unit's combat mission.

Before a criticality can be assigned an item of equipment for a unit, it is necessary to relate each principal item (TAM) to one or more of 22 distinct functions performed by FMF units. For the purposes of the CONTEAM model, each T/E item is assigned a criticality that relates to its importance in the unit's mission. Within this framework, the model makes use of probability tables to compute the quantity of each TAM to be loaded to fill, but not to overflow the constraint.

For TAM items that occur in a unit's T/E with authorized quantities of 1 to 20, the program will include TAMs with the highest criticality and exclude TAMs with the next-to-highest criticality when the constraint amounts to 60-75 percent of the space required to load the unit's full authorized T/E. Of the TAMs with low criticality, the bulky ones will be selectively excluded, but usually in part. That is, the quantity admitted to the constrained T/E will be some fraction of the authorized quantity. Nonpriority TAM items will probably be completely excluded from the constrained T/E.

For items that appear in the unit's T/E with authorized quantities of 40-1200, the program will exclude some portion of the full T/E quantity in almost every case--even for the highest priority items. This is purely a function of the algorithm as it begins to favor the first units of low priority items over, say, the 100th unit of a higher priority item. Experience shows these results to be useful, although they can be modified if the planner feels this is necessary.

The output from the CONTEAM model is a constrained T/E, plus a list of quantities of each T/E item that must be left behind under the constraint (limited cube or square shipping space) assumed during the execution of the model. It must be emphasized that the CONTEAM model produces nothing but a tentative T/E that may need to be adjusted by the operational planning officer.

After the planner has made all of the adjustments he deems necessary, he can rerun the CONTEAM model to obtain a more desirable constrained T/E.

By assigning a weight (or importance) to each item of equipment of a unit, a measure or index of operational readiness can be calculated that is oriented toward the unit's operational function(s). For a given T/E and unit, multiplying the quantity (density) of each item of equipment by its weight (criticality) and summing the products will give a value that indicates full or maximum readiness for that unit. If for some reason the T/E must be constrained by lack of shipping, availability of T/E items, etc, the items that can be shipped or that are available can be multiplied by their weighting factor, and, after summing the products, the value of readiness obtained can be compared against that value of readiness obtained from a 100% filled T/E and expressed as a percentage.

The OR index gives the capability of examining important tradeoffs. For example, the reallocation of square storage to bulk storage may actually increase the operational readiness of a unit.

It must be kept in mind that the CONTEAM model is but one subsystem of a much larger system and by itself does not necessarily provide the complete solution to the problem of limited shipping availability. Rather the CONTEAM model is designed to be utilized as an equal partner within the CALAS system.

Appendix F offers the interested reader the complete rationale and a detailed mathematical explanation behind the CONTEAM model.

# REFERENCES

1. V. E. Alessi; "Users Manual for the FMF Pac Transportation Feasibility Estimator FMF-TFE"; Operations Analysis Branch, Headquarters Fleet Marine Force, Pacific, February 1973

### A. General

The preceding sections of this report have provided the necessary background information to permit a detailed discussion of the solution procedure available from CALAS when applied to the amphibious lift problem created by comparing the CSS notional MAF lift expression and available amphibious assault ship capacities. This section will provide an analysis of the amphibious lift problem obtained by processing the input data previously described through the computer models of CALAS. The presentation will follow a logical procedure available to the staff planner in order to arrive at an optimal lift expression in a constrained amphibious assault shipping environment when utilizing the options available in CALAS.

The process of analyzing the CSS notional MAF data for the AE within CALAS demonstrates a systematic procedure for reducing landing force material within the constraints of operational readiness and sustainability. Additionally, the effects of incremental phasing of units and functions into the objective area from AFOE loaded ships are determined, which satisfies the first two objectives of the study. While the use of a notional MAF combat capability does not satisfy any real world combat mission, its troop list and resultant lift requirement provides a realistically sized problem for demonstrating the use of CALAS in aiding the staff planners of the MAF to include the most combat capable force for the assigned mission when embarked in the available assault shipping. Many iterations of processing the AE lift data through CALAS are possible while analyzing the effect of the different options

before selecting the commander's optimally combat ready force to be embarked in assault shipping. The greatest advantage from applying this method to the constrained loading problem is the rapid response available from a computer assisted decision aid.

Section IX will present a description of CALAS installed within an automated command and control system, demonstrating the concept of how the MAF commander and his staff may use the system in a routine manner.

#### B. Loading the CSS Notional MAF

# 1. Amphibious Lift Requirement Preparation

The AE troop list and cargo data used for the analysis were presented in Table IV-7 of Section IV. It may be recalled that this data prepared for ship loading was obtained by processing the troop list through the amphibious lift requirements subsystem of CALAS. For the staff planner, the troop list prepared for conducting the loading analysis was determined by analyzing the tactical problems to be solved from all available information. In the case of the notional MAF, it is assumed that the troop list contains all units desired for loading in assault shipping. By processing MAGTF and the JOPS cards, the lift requirement is computed for the AE. At the same time, the troop list factored cargo deck is punched. This deck is currently prepared by hand from data contained in the MAGTF listings, but when operating as an automated decision aid, CALAS would have this deck automatically written by the MAGTF program and available as input to the CCF model with no manual intervention.

### 2. The TFE Subsystem

The TFE program may be run at this point with the movement requirement and amphibious lift characteristic input decks. Sample

output listings from this program are found in Appendix C. This program primarily provides arrival times in the objective area, which are not a problem area in this study. This program does provide listings of unit cargo not loaded, as well as lists of ships sailing partially loaded, when that condition occurs. This program is most useful for cases where shipping capacity is greater than lift requirements.

## 3. Constrained Cargo Factoring Model Subsystem

With the same two input decks used by the TFE Program, the CCF computer model may be run for as many different values of the T/E constraint as desired up to some preestablished limit built into the program. Currently, the program executes for seven constraints, as shown in Table VII-1 for one program execution. After execution, the

Table VII-1

CONSTRAINT VALUES AND DOS FOR CCF MODEL PROCESSING

Constraints 1.0, .90, .85, .80, .75, .70, .65

DOS for AE = 15

CCF Model output provides the staff planner the information shown in Table VII-2. The first constraint used by the model is 100, or no constraint. The amphibious lift short fall presented in Section IV was obtained from this unconstrained loading run. Results for each constraint value used are also included in this table.

A graph of percent short fall versus the constraints used within the model is shown in Figure VII-1. The curve shows the effect

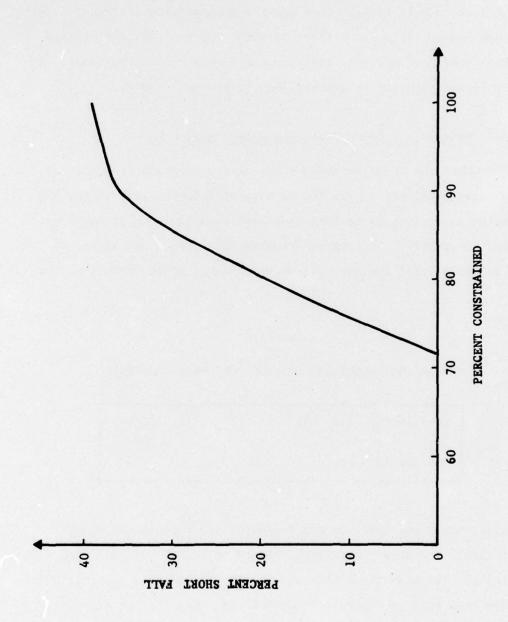


FIGURE VII-1. WEIGHTED CONSTRAINED UNIT LOADING VERSUS PERCENT SHORT FALL FOR THE AE USING ASSIGNED PARAMETERS

Table VII-2
WEIGHTED CONSTRAINED UNIT LOADING
VS PERCENT SHORT FALL

Per	cent
Short Fall	Constraint'
39%	100%
36	90
29	85
19	80
9	75
0	70.8

Constraints are weighted according to units' missions, as explained in Section VI.

of increasing the amount of materiel eliminated from T/Es of units on the percent short fall, i.e., percent of the constrained cargo not being loaded into the assault ships. The curve illustrates well the interactive effect when constraints reduce the square loading requirements below the square capacity, permitting the reallocation of square space to bulk storage. If constraints were limited to being applied to square loading requirements until no square loading short fall occurred, the reduction in bulk loading necessary to reduce the short fall for bulk items would be prohibitive. Square loaded cargo space is fully loaded when constraining units by 88 percent. Therefore, when constraining square loaded items by values lower than 88 percent and in the same amount as bulk cargo, excess square loading space will exist and increase so that reallocating square space to bulk accounts for the steep slope of the curve in Figure VII-1. Total loading of the constrained AE at a more reasonable value of 70.8 percent is then possible. Figure VII-2 shows

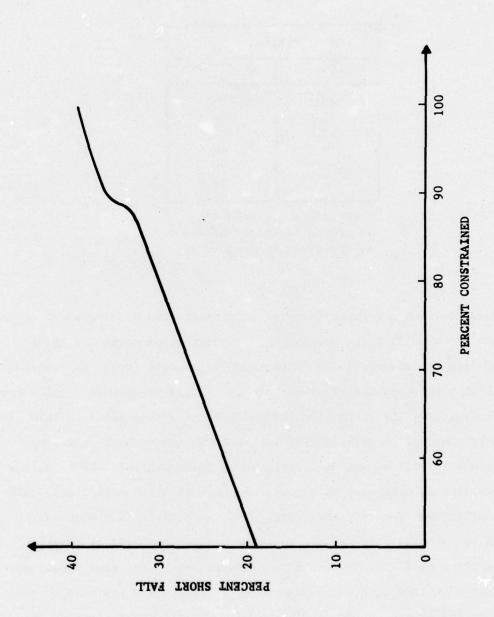


FIGURE VII-2. WEIGHTED CONSTRAINED UNIT LOADING VERSUS PERCENT SHORT FALL FOR SQUARE LOADED CARGO CONSTRAINT FIXED AT 88 PERCENT

the effect of limiting the square loading constraint to 88 percent, the amount necessary to load all square space. In Figure VII-2, the lack of any further reduction of square loaded items below 88 percent is illustrated. Constraints as low as 50 percent still permit a short fall of 19 percent of the constrained bulk cargo.

## 4. The Constrained T/E Embarkation Analysis Model Subsystem

At this point the staff planner becomes interested in the T/E reductions calculated for units when applying the lower constraint values. He observes that, with no constraint, there is a 39 percent short fall in shipping capacity for the original troop list, and the short fall is further reduced for each constraint. Since the constraint value providing complete loading is lower than may be acceptable, other CALAS options will be considered in finding the optimal operationally ready force for loading into the assault shipping. Before considering other options, a study of the effect on unit T/Es for the lower constraint values is necessary to determine what T/E reduction level can be accepted while maintaining a viable unit's equipment list. Table VII-3 contains the T/E listings for a sample of unit, M1038, in the troop list. At this point the subjective judgment of officers doing the planning becomes all important.

Although the constrained T/E Embarkation Analysis Model (CONTEAM) operates systemically on the criticality factors assigned as input, returning the greatest operational readiness index value for the T/E mix included for loading, the experience and judgment of officers reviewing T/E reductions for all combat, combat support, or combat service support functions is required for determining the acceptable constraint level. The need for exercising such judgment is ever present in current peacetime amphibious training exercises. Making such judgments is therefore routine. The advantage gained from using a computer assisted decision

Table VII-3(a)

CONSTRAINED T/E FOR M1038 WHEN CONSTRAINED TO 90% OF AUTHORIZED T/E LIFT REQUIREMENT

INFANTRY BATTALION. MARINE DIVISION

CURTATE T/E FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED 1/E IS 16656.65 CU FT CONSTRAINED TO 95.0 PCT DR 15824.00 CU FT

SQUARE OF PUBLISHED TZE IS 4431.00 SQ FT CONSTRAINED TO 95.0 PCT UR 4209.00 SO FT

	ITEM	1 TEM	ITEM	1/6	1/5	176	1/E	CRIT	****	*****REDUCED I/E***	1/E***	DEFIC-
TAM	SQUARE	CUBE	WEIGHT	SQUARE	CUBE	WE I GHT	017		9TY	SOUARE	CURE	IFNCY
AOOOS		5.0	159.0		5.0	159.0	-	60	:		5.0	
40090		3.0	47.0		39.0	611.0	13	60	13.		39.0	
A0265		0.0	0.0		0.0	0.0	-	80			0.0	
A0320		1.0	20.0		12.0	240.0	12	80	12.		12.0	
A0328		1.0	0.6		0.4	35.0	4	89	*		0.4	
40490		1.0	12.0		25.0	300.0	25	80	25.		25.0	
A0710		1.0	45.0		1.0	42.0	-	4	.1		1.0	
A0800		2.0	0.40		5.0	0.46	-	4	1.		5.0	
A0922		1.0	3.0		15.0	45.0	15	80	15.		15.0	
A1180		1.0	26.0		1.0	26.0	-	4	:		1.0	
A1240		8.0	252.0		8.0	252.0	-	*	:		8.0	
A1250		1.0	10.0		2.0	20.0	2	4	2.		2.0	
A1420		11.0	93.0		22.0	185.0	2	4	2.		22.0	
A1570		1.0	45.0		1.0	45.0	-	4	:		1.0	
A1730		1.0	22.0		15.0	330.0	15	, <b>œ</b>	15.		15.0	
A1800		1.0	26.0		7.0	392.0	1	8	7.		7.0	
A1900	10.0		4190.0	140.0		8380.0	2	8	2.	140.0		
A1920	61.0		2535.0	122.0		5070.0	2	80	2.	122.0		
04614		350.0	2575.0		700.0	5150.0	2	8	8		700.0	
A1950		0.0	0.0		0.0	0.0	-	8	:		0.0	
A2010		8.0	101.0		24.0	303.0	2	8	÷		24.0	
42020		8.0	139.0		40.0	695.0	r.	80	5.		40.0	
A2040		1.0	23.0		3.0	0.69	3	0	3.		3.0	
A2050		1.0	20.0		58.0	1160.0	58	8	58.		48.0	
A2182	0.09		3370.0	120.0		6740.0	~	8	2.	120.0		
A2184		2.0	55.0		0.4	110.0	8	8	2.		4.0	
A2390		1.0	5.0		10.0	20.0	10	8	10.		10.0	
A2480		1.0	28.0		2.0	140.0	S	8	5.		5.0	

Table VII-3(a) (Continued)

500ARE         CUBE         WEIGHT         GTA         OTA         SOUARE         CUBE         WEIGHT         OTA         SOUARE         CUBE         WEIGHT         OTA         SOUARE         CUBE         WEIGHT         OTA         SOUARE         CUBE         SOUARE         CUBE         OTA		MALL	MUL	TEM	1/6	1/6	1/6	1/5	CRIT		REDUCED	T/F***	DEF 1C-
53.0         145.0         53.0         145.0         53.0         145.0         53.0         53.0         145.0         33.0         53.0	TAN	SOUARE	CUBE	WEIGHT	SQUARE	CUBE	WEIGHT	017		017	SOUARE	CUBE	FENCY
54.0  5.0  97.0  9	A2510		53.0	145.0		53.0	145.0	-	4	:		53.0	
1.0   20.0   20.0   2.	A2580		1.0	97.0		3.0	291.0	m	œ	3.		3.0	
1.0   20.0   20.0   4.0   40	A2660		2.0	0.00		5.0	6.06	-	8	:		8.0	
1.0   20.0   1.0   20.0   1.0   20.0   1   4   1.   1.   1.   1.   1.   1.	A2685		1.0	10.0		0.4	40.0	4	Œ	;		4.0	
1.0   25.0   2.0   3.0   4   2.0   2.0     2.0   3.0   2.4   3.0   3.0   4   3.0     3.0   2641.0   2640   2940   212.0   1   2   1   54.0     3.1   3.5   3.5   3.0   2.5   1   2   1   5.0     3.2   3.5   3.5   3.5   3.0   3.0   3.0   3.0     3.2   3.5   3.5   3.5   3.5   3.0   3.0   3.0     3.3   4.0   3.5   3.0   3.0   3.0   3.0     3.3   4.0   3.5   3.0   3.0   3.0   3.0     3.3   4.0   3.5   3.0   3.0   3.0     3.4   3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5   3.5   3.5     3.5   3.5   3.5     3.5   3.5   3	00.		1.0	20.0		1.0	20.0	-	*	:		1.0	
2.0         10.0         2.0         30.0         1         4         1.0         2.0         3.0         2.0         1.0         2.0         2.0         3.0	01.		1.0	25.0		2.0	20.0	~	4	2.		2.0	
1.0   15.0   3.0   45.0   3.4   3.4   3.5   3.0     2641.0   225.0   212.0   1   2   1   54.0     1.0   116.0   225.0   212.0   1   2   1   54.0     1.0   116.0   225.0   212.0   1   2   1   54.0     1.0   116.0   225.0   213.0   2   2   2   2     1.0   116.0   225.0   213.0   2   2   2   2     1.0   12.0   225.0   213.0   2   2   2   2     1.0   12.0   225.0   225.0   2   2   2   2     1.0   12.0   225.0   225.0   2   2   2   2     1.0   12.0   225.0   2   2   2   2   2     1.0   12.0   225.0   2   2   2   2     1.0   12.0   225.0   2   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   12.0   225.0   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     1.0   225.0   2   2   2     2.0   2.0   2.0   2     2.0   2.0   2.0   2     2.0   2.0   2.0   2     2.0   2.0   2.0	00		2.0	30.0		2.0	30.0	-	•	:		2.0	
54.0         2641.0         54.0         2641.0         1         2         1         4         11         54.0         20.0         20.1         25.0         1         4         11         54.0         20.0	90		1.0	15.0		3.0	45.0	•	•	3.		3.0	
29.0         312.0         22.0         312.0         1 4         1.         22.0         20.0         112.0         1.         4         1.         22.0         2	65	54.0		2641.0	54.0		2641.0	-	2	:	54.0		
1.0   1.0   2.25.0   2.5.0   1   2   1.0   2.5.0   1.0   2.5	06		29.0	312.0		29.0	312.0	-	4	:		29.0	
1.0   116.0   2.0   233.0   2.0	00		8.1	225.0		8.1	225.0	-	~	:		8.1	
13.0   355.0   25.0   710.0   2   2   2   36.0     4.2   4.0   1970.0   2   2   2   36.0     4.2   4.0   12.0   150.0   25   1   25   1   25     3   4.0   13.5   150.0   25   1   25   1   12.0     4.2   4.0   13.5   150.0   25   1   25   1   12.0     4.2   4.0   13.5   150.0   25   1   25   1   12.0     4.2   3.0   13.5   150.0   25   1   25   1   13.0     4.2   2.0   13.5   150.0   25   1   25   1   10.0     4.2   2.0   17.0   2.0   2   1   12.0     4.2   2.0   17.0   20.0   2   1   12.0     4.2   2.0   10.0   2.0   1   1   1     4.2   2.0   2.0   2.0   2.0   1   1     4.3   3.0   10.0   2.0   1   1   1     4.4   4.5   2.0   2.0   2.0     4.5   10.0   2.0   2.0   2.0     4.5   10.0   2.0   2.0   2.0     4.5   10.0   2.0   2.0   2.0     4.5   2.0   2.0   2.0   2.0     4.5   2.0   2.0   2.0   2.0     4.5   2.0   2.0   2.0     4.5   2.0   2.0   2.0     4.5   2.0   2.0   2.0     4.5   2.0   2.0   2.0     4.5   2.0   2.0     4.5   2.0   2.0     5.0   2.0   2.0   2.0     5.0	40		1.0	116.0		2.0	232.0	~	~	2.		2.0	
173.0         966.0         346.0         1970.0         2         2         2         2         346.0           4.2         140.0         4.2         140.0         1         2         1.         4.2         4.2           4.2         140.0         7.8         160.0         25         1         25.         7.8           5.3         5.0         150.0         25         1         25.         18.7         18.7           1.9         60.0         18.7         150.0         25         1         25.         18.7           1.9         60.0         18.7         150.0         25         1         25.         18.5           1.9         60.0         18.5         60.0         6         1         60.0         18.5           2         2.0         18.5         60.0         50.0         50.0         50.0         18.5           1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0           2.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0           2.0         2.0         2.0         2.0	20		13.0	355.0		26.0	710.0	2	~	2.		26.0	
4.2         140.0         4.2         140.0         1         2         1         25.         7.8           4.3         5.0         12.0         150.0         25         1         25.         17.8           4.5         6.0         13.5         150.0         25         1         25.         13.5           1.9         60.0         13.6         150.0         25         1         25.         18.5           1.9         60.0         1         5.0         25         1         25.         18.5           1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         18.5         1.0         18.5         1.0	06		173.0	0.096		346.0	1920.0	2	N	2.		346.0	
*3         4.0         7.8         100.0         25         1         25.         7.8           *3         3.0         13.5         150.0         25         1         25.         12.0           *3         3.0         13.5         150.0         25         1         25.         12.0           *3         7.0         18.7         175.0         25         1         25.         18.7           *2         3.0         18.7         175.0         25         1         25.         18.7           *2         3.0         18.7         17.0         18.0         50.0         50.0         10.0         10.0           *2         3.0         18.5         60.0         25         1         25.         18.7           *2         2.0         17.0         25.0         25.0         25.0         25.0         17.0           *3         80.0         75.0         25.0         25.0         25.0         17.0         17.0           *4.2         50.0         25.0         25.0         1         1         1         1         1           *4.2         53.0         4.2         50.0         25.0	50		4.2	140.0		4.2	140.0	-	e	:		4.2	
.5         6.0         12.0         150.0         25         1         25.         12.0           .3         7.0         13.5         150.0         50         1         50.         13.5           .0         1.0         1.0         1.1         5.0         5         1         25.         18.5           .0         1.0         1.0         1.0         1.0         1.0         1.0         1.0           .1         1.0         3.5         60.0         5         1         55.         1.1           .2         2.0         1.0         1.0         1.0         1.0         1.0           .2         2.0         3.0         5.0         5         1         50.           .2         2.0         1.0         5.0         25.0         1         50.           .2         2.0         1.0         2.0         2.0         1         25.         1.2           .2         2.0         1.0         2.0         2.0         1         2.0         3.0           .2         2.0         2.0         2.0         2.0         1         1.0         1.0           .2         2.0	10		£.	•••		7.8	100.0	25	-	25.		7.8	
3       3.0       13.5       155.0       56       13.5         .9       7.0       18.7       175.0       25       18.7         .0       1.0       18.7       175.0       25       18.7         .2       2.0       11.0       18.5       600.0       10       10.0       18.5         .2       2.0       1.0       1.0       18.6       50.0       25       1       25.0       18.5         .2       2.0       1.0       2.0       2.0       25       1       25.0       3.8         1.0       16.0       17.0       25.0       25       1       25.0       17.0         6.3       80.0       17.0       25.0       25       1       25.0       17.0         2.0       50.0       12.0       25       1       25.0       17.0         2.0       50.0       12.0       25       1       25.0       17.0         3.3       40.0       10.0       25       1       10.0       25.0       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1 <td< td=""><td>30</td><td></td><td>• 5</td><td>0.9</td><td></td><td>12.0</td><td>150.0</td><td>52</td><td>-</td><td>25.</td><td></td><td>15.0</td><td></td></td<>	30		• 5	0.9		12.0	150.0	52	-	25.		15.0	
***         7**         18*7         175.0         25         1         25         18*7         18*7         175.0         25         1         25         18*7	04		.3	3.0		13.5	150.0	20	_	50.		13.5	
1.9   60.0   18.5   600.0   10   1   10.0   18.5   1   10.0   18.5   1   10.0   18.5   1   10.0   18.5   1   10.0   19.5   1   10.0   19.5   1   10.0   19.5   1   10.0	20		6.	7.0		18.7	175.0	52	-	25.		18.7	
1.9   60.0   18.5   600.0   10   1   10.   18.5   10.0	90		0.	1.0			2.0	S	-	2.		-	
-2       3.0       1.0       18.0       6       1.0       1.0         -1       11.0       3.5       50.0       50.1       50.0       3.5       1.0         -2       2.0       17.0       50.0       25       1       25.       17.0         -2       2.0       17.0       50.0       25       1       25.       17.0         -3       16.0       1236.5       19984.0       1249       1       129.       17.0         -6       30.0       25.0       25.0       1       4.2       2       1       4.2       2       1       4.2       2       1       4.2       2       1       4.2       1       1       1       1	20		1.9	0.09		18.5	60000	10	-	10.		18.5	
.1       1.0       3.5       50.0       1       50.       3.5         .0       1.0       1.0       1.0       5.0       1       5.       3.8         .2       2.0       3.4       50.0       25       1       25.       3.8         1.0       16.0       17.0       50.0       25       1       25.       17.0         2.0       50.0       17.0       50.0       1       1       12.0       15.6         2.0       50.0       75.6       960.0       1       1       12.0       75.6         2.0       50.0       1.3       27.0       1       1       1       1.0       2.0         3.3       40.0       10.4       24.0       8       1       8.       1       1.0	00		• 5	3.0		1.0	18.0	¢	-	•		1.0	
.0       1.0       .1       5.0       5       1       5.0       .1       5.0       .1       .1       .1       .1       .1       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .1       .2       .2       .1       .2       .1       .2       .2       .2       .1       .2       <	9			1.0		3.5	20.0	20	-	.05		3.5	
.2       2.0       3.8       50.0       25       1       25.       3.8         .7       2.0       17.0       12.0       25.       1       25.       17.0         1.0       16.0       1236.5       1998.0       1       12.       75.6         2.0       50.0       2.0       50.0       1       1       1       1.         1.3       27.0       1.3       27.0       1       1       1.       1.         1.3       27.0       1.3       27.0       1       1       1.       4.2       5.       1.       1.       4.2       5.       1.       1.       1.       4.2       5.       1.       1.       1.       1.       1.       1.       1.	30		••	1.0		•	2.0	S	-	3.		:	
17.0     17.0     50.0     25     17.0       11.0     16.0     1236.5     19984.0     1249.     12.0       20     50.0     2.0     50.0     12.     75.6       20     50.0     2.0     50.0     1.1     1.     1.       1.3     27.0     1.3     27.0     1     1.     1.       1.3     27.0     1.3     27.0     1     1.     1.       1.1     1.0     1.     1.     1.     1.       1.1     1.     1.     1.     1.     1.       1.1     1.     1.     1.     1.     1.       1.1     1.     1.     1.     1.     1.       1.1     1.     1.     1.     1.     1.       4.2     51.0     6.     1.     6.     1.     4.2       4.2     53.0     1.     1.     1.     4.2       5.0     5.0     5.0     5.     5.     5.       11.0     1.     1.     1.     1.     4.2       5.0     5.0     5.     1.     1.     5.       7.7     50.0     5.     1.     1.     1.       7.7     50	20		.2	2.0		3.3	20.0	52	-	25.		3.8	
16.0   16.0   1236.5   19984.0   1249   1   1249.   1235.5   1536.5   19984.0   1249   1   1249.   1235.5   1536.5   1536.0   12   1   1   1   1   1   1   1   1	01		2.	2.0		17.0	20.0	52	7	25.		17.0	
6.3       80.0       75.6       960.0       12       1       12.       75.6         2.0       50.0       1       1       1       1       1       2.0         1.3       27.0       1       1       1       1       1       1         3.3       40.0       6       1       4.2       2.9       4.2       1       4.6       2.9       4.2       1       4.6       2.9       4.2       1       4.6       2.9       4.2       1       4.2       2.9       4.2       1       4.6       1       4.6       2.9       2.9       4.2       1       4.6       1       4.6       2.9       2.9       2.9       4.2       1       4.6       1       4.6       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9       2.9	50		1.0	16.0		1236.5	19984.0	1249	-	1249.		1236.5	
2.0     50.0     1     1     1     1     1       1.3     27.0     1     1     1     1     1       3.3     40.0     6.0     6     1     6.     10.3       4.2     53.0     10.0     6.0     6     1     6.     10.6       4.2     53.0     60.0     6     1     6.     2.9       4.2     53.0     60.0     6     1     6.     2.9       11.0     180.0     10120.0     15560.0     9350.0     9350.1       11.0     64.0     55.0     1     1     1       7.7     50.0     10.0     3.9     1     1       3.0     10.0     3.9     1     1     1       12.0     204.0     1     1     1     1       12.0     204.0     1     1     1     1	00		6.3	80.0		75.6	0.096	12	-	12.		15.6	
1.3     27.0     1     1     1.3       4.1     5.0     .6     40.0     8     1     8.     .6       3.3     40.0     19.6     19.6     19.6       1.1     10.0     51.8     480.0     48     1     19.6       4.2     53.0     60.0     6     1     6.     2.9       4.2     53.0     60.0     6     1     6.     2.9       11.0     180.0     10120.0     1550.0     9350.1     9350.1       7.7     60.0     7.7     60.0     1     1     7.7       6.0     10.0     3.0     30.0     3.0     3.0       3.0     85.0     20.4     1     1     1       12.0     204.0     1     1     1     1       12.0     204.0     1     1     1     1	10		2.0	20.0		2.0	20.0	-	-	:		2.0	
3.3 40.0 19.6 40.0 B 1 B	15		1.3	27.0		1.3	27.0	-	1,	:		1.3	
3.3     40.0     19.6     240.0     6     1     6.     19.6       15.1     10.0     51.8     480.0     48     1     48.     51.8       4.2     53.0     4.2     53.0     1     1     4.2       11.0     180.0     10120.0     16560.0     1     1     4.2       7.7     60.0     1     1     1     7.7       .0     1.0     3.0     1     1     1       3.0     85.0     390.0     390.1     3.9       12.0     204.0     1     1     1     1       12.0     204.0     1     1     1     1	20		7.	2.0		9.	40.0	œ	-	8.		9.	
1.1   10.0   51.8   480.0   48   1   48.   51.8   51.8   5.9   50.0   5   1   5.0   5.9   5.0   5   1   1   1   1   1   1   5.0	40		3.3	40.0		19.6	240.0	9	-	• •		19.6	
4.2 53.0 4.2 53.0 1 1 6. 2.9  11.0 180.0 10120.0 15560.0 920 1 850. 9350.1  11.0 64.0 55.0 320.0 5 1 5. 55.0  7.7 50.0 1.0 390.0 390. 1 390.  3.0 85.0 3.0 85.0 1 1 1 1 1. 12.0  12.0 204.0 12.0 204.0 1 1 1. 12.0	01		-:	10.0		51.8	480.0	48		48.		51.8	
4.2     53.0     4.2     53.0     1     1     1     4.2       11.0     180.0     10120.0     15560.0     920.1     850.     9350.1       11.0     54.0     55.0     320.0     5     1     55.0       7.7     50.0     3.0     1     1     1       3.0     1.0     3.0     3.0     3.0       3.0     85.0     1     1     1       12.0     204.0     1     1     1     1	04			10.0		5.9	0.09	ç	-	•		5.9	
11.0     180.0     10120.0     155600.0     920     1     850.     9350.1       11.0     64.0     55.0     320.0     5     1     55.0       7.7     60.0     1     1     1.     7.7       60.0     1.0     3.0     390.0     390.     3.9       3.0     85.0     1     1     1     1       12.0     204.0     1     1     1     1	20		4.2	53.0		4.2	53.0	-	-	:		4.5	
11.0     64.0     55.0     320.0     5 .     5.       7.7     60.0     1 .     1 .     1.       .0     1.0     3.9     390.0     390.       3.0     85.0     5.0     85.0     1 .       12.0     204.0     1 .     1.	06		11.0	180.0		10120.0	5	920	-	850.		9350.1	.01
7.7 60.0 1 1 1 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	40		11.0	64.0		55.0	320.0	S	~	· 0		25.0	
3.0 85.0 5.0 85.0 1 1 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	06		7.7	0.09		7.7	0.09	-	-	:		7.7	
3.0 85.0 5.0 5.0 85.0 1 1 1. 12.0 204.0 12.0 204.0 1 1.	36		•	1.0		3.0	390.0	390	-	390.		3.9	
12.0 204.0 12.0 204.0 1 1 1.	20		3.0	85.0		3.0	85.0	-	-	:		3.0	
	09		12.0	204.0		15.0	204.0	-	-	:		15.0	

Table VII-3(a) (Continued)

	ITEM	ITEM	ITEM	1/6	1/5	1/6	1/E	CRIT	****		T/E****	DFF1C-
TAM	SQUARE	CUBE	WEIGHT	SQUARE	CUBE	WEIGHT	077		017	SOUARE	CUBE	TENCY
04670		1.4	0.9		1.4	6.0	-	1	-		1.4	
C4580		.2	2.0		4.	4.0	N	-	2.		4.	
C4690		2.0	40.0		11.7	240.0	c	-	•		11.7	
C4 790		7.7	40.0		84.6	440.0		-	::-		84.6	
C4870		6.4	85.0		44.6	6.365			7.		44.6	
C4 980		3.6	9.0		210.0	472.0	65	-	26.		200.8	3.
54930		4.	12.0		.7.	24.0	~	-	2.		1.	
C4950		1.0	0.09		1.0	60.09	-	-	-		1.0	
C4980		14.0	150.0		490.0	5250.0	35	-	32.		450.2	3.
06053		4.0	196.0		8.1	392.0	N	-	2.		8.1	
C5110		2.7	14.0		95.8	504.0	36	-	34.		9.16	2.
C5200		3.8	4.0		83.2	88.0	22	1	22.		83.2	
C5320		8.2	162.0		138.7	2754.0	11	-	17.		138.7	
C5400		7.0	150.0		132.2	2850.0	19		19.		132.2	
C5410		0.6	131.0		18.0	262.0	~		2.		18.0	
C5820		25.0	353.0		0.009	8472.0	24	-	24.		20065	
C5870		4.3	38.0		25.7	228.0	¢	1	. 9		25.7	
C5930		2.8	100.0		22.1	800.0	60	-	8.		22.1	
06650		1.5	31.0		1.5	31.0	-	-	:		1.5	
C6010		2.0	200.0		5.0	20000	-	-	:		2.0	
C6140		.2	7.0		1.3	49.0	-	-	7.		1.3	
C6215		0.9	84.0		0.9	84.0	-	-	-		0.9	
C6220		5.	7.0		6.0	84.0	12	-	12.		0.9	
C6260		11.0	5.0		11.0	2.0	-	1	-		11.0	
C6370		6.3	107.0		50.4	856.0	œ	-			50.4	
C6388		6.5	140.0		58.7	1400.0	10	-	10.		58.7	
C6390		7.2	257.0		86.2	3084.0	12	-	12.		86.2	
C6410		18.0	330.0		144.0	2640.0	60	-	8		144.0	
C6490		1.5	62.0		10.5	434.0	1	-			10.5	
C6500		1.0	12.0		5.0	0.09	S	1	2.		2.0	
C6510		6.9	0.06		34.3	450.0	S	-	3.		34.3	
09990		3.2	30.0		3.2	30.0	-		-		3.2	
C6670		•	18.0		6.	18.0	-	-	-		6.	
C6684		••	1.0		1.1	111.0	111	-	111.		1:1	
06000	38.0		1054.0	38.0		1054.0	-	•	-	38.0		
00100		20.0	153.0		20.0	163.0	-	2	-		20.0	
06200		1.4	21.0		1.4	21.0	-	2	:		1.4	
00400			16.0		• •	10.0	-	2	:		v.	
00410		9.	16.0		9.	16.0	-	~	-		9.	
00230			10.0		•3	10.0	-	2	-		•3	

Table VII-3(a) (Concluded)

JENCY				:			3.																											
CURE	125.0	0.	400						4.3	1.6	1.0	•	4.0	4.8	17.9	0.0	36.0	68.8	45.5	144.0	496.0	0.0	0.0	0.0	1.1	9.	2.0		4.2	1.3	2.0		3.4	4209.015824.0
*****REDUCED T/E**** OTY SOUARE CURE				7.55.7	71.0	938.0	400.8	1109.5																				360.0						4209.0
017	-	:	:	17.	:	7.	27.	18.	36.		-1	5.	.1.	12.	. 2	110.	12.	32.	35.	12.	e:	36.	•	•	36.	20.	. 2	8		*	2.	:	3.	3968.
3	8	~	N	8	4	8	æ	8	-	-	<b>6</b> 0	-	89	4	හ	80	80	80	89	8	8	80	8	80	60	8	-	8	80	80		~	2	
0 7		-	-	18	-	1	30	50	36	•	-	'n	-	12	2	110	12	32	35	12	ď	36	*	4	36	20	8	80	-	*	~	-	m	4051
WE IGHT	1832.0	1.0	1890.0	10260.0	2780.0	51590.0	27000.0	43000.0	108.0	28.0	10.0	5.0	68.0	84.0	216.0	0.0	324.0	480.0	840.0	600.0	0.096	0.0	0.0	0.0	72.0	20.0	0.9	3360.0	68.0	32.0	10.0	2.0	117.0	412462.0 4051
CUBE	125.0	••	4006						4.3	1.66	1.0	-:	4.0	4.8	17.9	0.0	36.0	68.8	45.5	144.0	446.0	0.0	0.0	0.0	1.1	9.	2.0		4.2	1.3	2.0		3.4	16656.6
SQUARE				828.0	71.0	938.0	540.0	1220.0																				360.0						4431.0
WEIGHT	1832.0	0.1	1890.0	570.0	2780.0	7370.0	0.006	2400.0	3.0	7.0	10.0	1.0	68.0	7.0	108.0	0.0	27.0	15.0	24.0	20.0	120.0	0.0	0.0	0.0	2.0	1.0	3.0	420.0	68.0	8.0	2.0	2.0	39.0	
CUBE	125.0	••	2006						••	4.	0.1	0.	•••	4.	8.9	0.0	3.0	2.2	1.3	12.0	62.0	0.0	0.0	0.0	•	••	1.0		4.2	٠.	1.0		:-	STALS
SOUARE				46.0	71.0	134.0	18.0	61.0																				45.0						GRAND TOTALS
TAH	00725	99100	00170	00840	06800	01020	00110	0110	E0080	E0090	E0180	E0210	E0230	E0290	E0320	E0892	00603	E0920	06603	E1060	E1090	E1155	E1156	E1157	E1180	E1240	E1260	E1480	E1530	E1760	E1990	E1960	E2030	

TODAYS DATE 03/03/76

OR INDEX(SQUARE) = 93.46

OR INDEX(CUBE) = 98.99

OR INDEX(TOTAL T/E) = 98.51

Table VII-3(b)

CONSTRAINED T/E FOR M1038 WHEN CONSTRAINED TO 85% OF AUTHORIZED T/E LIFT REQUIREMENT

INFANTRY BATTALION. MARINE DIVISION

CUBE OF PUBLISHED T/E IS 16656.65 CU FT
CONSTRAINED TO 92.5 PCT OR 15407.00 CU FT
SQUARE OF PUBLISHED T/E IS 4431.00 SO FT
CONSTRAINED TO 92.5 PCT OR 4099.00 SO FT

TAM SOU	SOUARE	CUBE	WEIGHT	SOUARE	CUBE	T/E WEIGHT	017	CRIT	710	TY SOUARE	CUBE	IENCY
2000		5.0	159.0		5.0	159.0	-	60	:		5.0	
0600		3.0	47.0		39.0	611.0	13	80	13.		39.0	
9565		0.0	0.0		0.0	0.0	-	8	:		0.0	
0320		1.0	20.0		12.0	240.0	12	8	12.		12.0	
9328		1.0	0.6		4.0	36.0	4	8	. 4		4.0	
0640		1.0	12.0		25.0	300.0	25	8	25.		25.0	
0710		1.0	42.0		1.0	42.0	-	4	.1		1.0	
A0800		2.0	94.0		5.0	94.0	-	4	1:		5.0	
0922		1.0	3.0		15.0	45.0	15	8	15.		15.0	
1180		1.0	26.0		1.0	26.0	-	4			1.0	
1240		8.0	252.0		8.0	252.0	-	4	1.		8.0	
1250		1.0	10.0		2.0	20.0	2	4	2.		2.0	
1420		11.0	93.0		22.0	186.0	8	4	2.		22.0	
1570		1.0	45.0		1.0	45.0	-	4	:		1.0	
1730		1.0	22.0		15.0	330.0	15	,00	15.		15.0	
1800		1.0	26.0		7.0	392.0	~	80			7.0	
	20.0		4190.0	140.0		8380.0	2	60	2.	140.0		
	61.0		2535.0	122.0		5070.0	2	80	2.	122.0		
1940		350.0	2575.0		20000	5150.0	2	8	2.		700.0	
0561		0.0	0.0		0.0	0.0	-	80	1.		0.0	
2010		8.0	101.0		24.0	303.0	3	60	3.		24.0	
2020		8.0	139.0		40.0	695.0	2	8	5.		40.0	
2040		1.0	23.0		3.0	0.69	3	8	3.		3.0	
2050		1.0	20.0		58.0	1160.0	58	8	58.		58.0	
	0.09		3370.0	120.0		6740.0	2	60	2.	120.0		
2184		2.0	55.0		4.0	110.0	2	8	. 2			
A2390		1.0	2.0		10.0	50.0	10	8	10.		10.0	
42480		1.0	28.0		5.0	140.0	S	8	5.		5.0	

Table VII-3(b) (Continued)

	ITEM	ITEM	ITEM	1/6	1/5	17.6	1/6	CRIT	****	*****REDUCED T/E***	*****	DEFIC-
TAM	SQUARE	CUBE	WEIGHT	SQUARE	CUBE	WEIGHT	710		710	SOUARE	CUBE	1F NCY
A2510		53.0	145.0		53.0	145.0	-	4	:		53.0	
A2580		1.0	97.0		3.0	291.0	2	8	3.		3.0	
A2660		5.0	0.06		5.0	0.06	-	80	:		5.0	
A2685		1.0	10.0		4.0	40.0	4	80	4		4.0	
A2700		1.0	20.0		1.0	20.0	-	4	:		1.0	
A2710		1.0	25.0		2.0	50.0	N	4	2.		5.0	
A2900		2.0	30.0		2.0	30.0	1	4			5.0	
A3240		1.0	15.0		3.0	45.0	<b>F</b>	4	3.		3.0	
80465	54.0		2641.0	54.0		2641.0	-	2	:	54.0		
80490		29.0	312.0		29.0	312.0	-	4	:		29.0	
80500		8.1	225.0		9.1	225.0	-	~	:		8.1	
81540		1.0	116.0		2.0	232.0	~	2	2.		5.0	
81650		13.0	355.0		26.0	710.0	~	2			26.0	
81690		173.0	0.096		346.0	1920.0	8	8	2.		346.0	
82220		4.2	140.0		4.2	140.0	-	2			4.2	
01022		.3	0.4		7.8	100.0	25	-	25.		7.8	
52030			0.9		12.0	150.0	25	-	25.		12.0	
C2040		£.	3.0		13.5	150.0	20	-	20.		13.5	
22050		8.	7.0		18.7	175.0	25	-	25.		18.7	
C2060		••	1.0		•	5.0	S	-	5.		-	
C2070		1.9	0.09		18.5	60000	10	-	10.		18.5	
C2100		• 5	3.0		1.0	18.0	9	-	•		1.0	
C2160			1.0		3.5	20.0	20	1	50.		3.5	
C2230		••	1.0			5.0	S	-	5.		-	
C2250		.2	2.0		3.8	20.0	25	-	25.		3.8	
C2310			2.0		17.0	50.0	25	-	25.		17.0	
C3020		1.0	16.0		1236.5	19984.0	1249	1	1249.	1	1236.5	
C4000		6.0	80.0		75.6	0.096	12	-	12.		75.6	
C4010		2.0	20.0		2.0	20.0	-	-	:		5.0	
24015		1.3	27.0		1.3	27.0	-		1:		1.3	
C4020		:	2.0		9.	40.0	80	-	8.		9.	
C4040		3.3	40.0		19.6	240.0	9	-	.0		10.6	
C4110		1.1	10.0		51.8	480.0	8	-	48.		51.8	
C4140			10.0		5.9	0.09	9	-	• 9		5.9	
C4250		4.2	53.0		4 • 2	53.0	-	-	:		4.2	
C4290		11.0	180.0		10120.0	165600.0	920	-	815.	8	8964.5	105.
C4340		11.0	64.0		55.0	320.0	ທ		8.		55.0	14.7
C4390		7.7	0.09		7.7	0.09	-	-			7.7	
C4436		0.	1.0		3.9	390.0	390	••	390.		3.9	
C4650		3.0	85.0		3.0	85.0	-	-	1:		3.0	

Table VII-3(b) (Continued)

	ITEM	ITEM	ITEM	1/E	TVE	1/5	1/E	CRIT	****	*****	1/E****	DEFIC-
TAM	SQUARE	CUBE	WEIGHT	SOUARE	CUBE	WEIGHT	VT0		710	SGUARE	CUBE	I S NCY
C4660		12.0	204.0		12.0	204.0	-	-	:		12.0	
C4670		1.4	0.9		1.4	0.9	-	-	:-		1.4	
C4680		.2	2.0		٠.	4.0	N	-	2.		4.	
C4690		2.0	40.0		11.7	240.0	9	-	• 9		11.7	
C4790		7.7	40.0		84.6	440.0	=	-	11.		84.6	
C4870		6.4	85.0		44.6	595.0	1	1	7.		44.6	
C4 830		3.6	8.0		210.0	472.0	69	-	55.		196.2	. 4
C4930		4.	12.0		.7	24.0	2	-	2.			
C4950		1.0	0.09		1.0	0.09	-	-	:		1.0	
C4980		14.0	150.0		490.0	5250.0	35	-	31.		430.3	•
C2030		4.0	196.0		8.1	392.0	2	-	2.		8.1	
C5110		2.7	14.0		95.8	504.0	36	1	34.		89.4	2.
C5200		3.8	4.0		83.2	88.0	22		22.		83.2	
C5320		8.2	162.0		138.7	2754.0	17	-	17.		138.7	
C5400		7.0	150.0		132.2	2850.0	61	-	19.		132.2	
C5410		0.6	131.0		18.0	262.0	2	-	2.		18.0	
C5820		25.0	353.0		0.009	8472.0	24	-	23.		585.7	:
C5870		4.3	38.0		25.7	228.0	9	-	• 9		25.7	
C5930		2.8	100.0		22.1	800.0	60	1	ě		22.1	
06650		1.5	31.0		1.5	31.0	-	-	:		1.5	
C6010		5.0	200.0		5.0	200.0	-	-	:		5.0	
C6140		• 5	7.0		1.3	49.0	~	-			1.3	
56215		0.9	84.0		0.9	84.0	-	-	:		6.0	
C6220		• 5	7.0		0.9	84.0	12	-	15.		6.0	
C6260		11.0	5.0		11.0	5.0	-	-	:		11.0	
C6370		6.3	107.0		50.4	856.0	8	-	8		20.4	
C6388		5.5	140.0		58.7	1400.0	10	1	10.		58.7	
C6390		7.2	257.0		86.2	3084.0	12	-	12.		86.2	
C6410		18.0	330.0		144.0	2640.0	80	-	9.		144.0	
06493		1.5	62.0		10.5	434.0	1	-	7.		10.5	
00590		1.0	12.0		2.0	0.09	'n	-	٥.		2.0	
01590		6.9	0.06		34.3	450.0	S	-,	5.		34.3	
09990		3.2	30.0		3.2	30.0	-	-	:		3.2	
C6670		6.	18.0		6.	18.0	-	1	1:		•	
C6684		0.	1.0		1.1	1111.0	111	-	1111.		-:	
06000	38.0		1054.0	38.0		1054.0	-	4	:	38.0		
00100		20.0	163.0		20.0	163.0		2	:		20.0	
06500		1.4	21.0		1.4	21.0	-	2	:		1.4	
00400		• •	16.0		• 5	16.0	~		:			
01400		9.	16.0		9.	16.0	-	2	:		9.	
00530		.3	10.0		•3	10.0	-	2	:		£.	

Table VII-3(b) (Concluded)

TODAYS DATE 03/02/76

OR INDEX(SOUARE) = 90.20

OR INDEX(CUBE) = 98.48

OR INDEX(TOTAL T/E) = 97.76

4099-015407-0

3926.

4431.0 16656.6 412462.0 4051

GRAND TOTALS

Table VII-3(c)

CONSTRAINED T/E FOR M1038 WHEN CONSTRAINED TO 75% OF AUTHORIZED T/E LIFT REQUIREMENT

INFANTRY BATTALION. MARINE DIVISION

C F 3	FT FT	FT	FT
E	33	80	20
11 668	16656.65	4431.00	3877.00
CONTAIL TO TON CLASS VIII CLASS II TAM ITEMS	CUBE OF PUBLISHED T/E IS 16656.65 CU FT CONSTRAINED TO 87.5 PCT OR 14575.00 CU FT	SQUARE OF PUBLISHED T/E IS 4431.00 SO FT	CONSTRAINED TO 87.5 PCT OR 3877.00 SQ FT

	ITEM	ITEM	ITEM	1/E	1/E	1/E	TZE	CRIT	****	******	T/E***	DEFIC-
TAN	SQUARE	CUBE	WEIGHT	SQUARE	CUBE	WEIGHT	OTY		410	SQUARE	CURE	IFNCY
40005		5.0	159.0		2.0	159.0	-	80	:		5.0	
A0090		3.0	47.0		39.0	6111.0	13	8	13.		39.0	
A0265		0.0	0.0		0.0	0.0	-	8	1:		0.0	
A0320		1.0	20.0		12.0	240.0	12	8	12.		12.0	
A0328		1.0	0.6		4.0	36.0	4	60	•		4.0	
40490		1.0	12.0		25.0	30000	52	8	25.		25.0	
A0710		1.0	42.0		1.0	42.0	-	4	.1		1.0	
A0800		5.0	94.0		2.0	94.0	-	4			5.0	
A0922		0.:	3.0		15.0	45.0	15	æ	15.		15.0	
A1180		1.0	26.0		1.0	26.0	-	4	:-		1.0	
A1240		8.0	252.0		8.0	252.0	-	4	1.		8.0	
A1250		1.0	10.0		2.0	20.0	2	4	2.		2.0	
A1420		11.0	93.0		22.0	186.0	2	4	2.		22.0	
A1570		1.0	45.0		1.0	45.0	-	4	1.		1.0	
A1730		1.0	22.0		15.0	330.0	15	œ	15.		15.0	
A1800		1.0	26.0		7.0	392.0	1	8			7.0	
A1900	20.0		4190.0	140.0		8380.0	2	8	2.	140.0		
A1920	61.0		2535.0	122.0		5070.0	2	8	2.	122.0		
A1940		350.0	2575.0		700.0	5150.0	2	8	2.			
A1950		0.0	0.0		0.0	0.0	-	80	-:		0.0	
A2010		8.0	101.0		24.0	303.0	3	80	3.		24.0	
A2020		8.0	139.0		40.0	695.0	2	8	5.		40.0	
A2040		1.0	23.0		3.0	0.69	ר	60	M		3.0	
A2050		1.0	20.0		58.0	1160.0	58	80	58.		58.0	
A2182	0.09		3370.0	120.0		6740.0	~	8	2.	120.0		
A2184		2.0	55.0		4.0	110.0	0	60				
A2390		1.0	2.0		10.0	20.0	10	8	10.		10.0	
A2480		1.0	28.0		2.0	140.0	S	80	٠.		5.0	

Table VII-3(c) (Continued)

MEIGHT SQUARE CUBE WEIGHT OTTY  145.0 97.0 97.0 97.0 97.0 97.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 1	SALES   CURE   WEIGHT   CT   CORP   CURE			.,,					*****	* 0000000	******	4.000
145.0 97.0 97.0 97.0 97.0 97.0 97.0 97.0 97	145.0   53.0   145.0   1   4   1   1   53.0   53.0   50.0   1   45.0   1   50.0   1	CUBE	WEIGHT	SQUARE	CUBE	WE IGHT	917	CRIT	014	SOJARE	CUBE	1ENCY
97.0 90.0 10.0 20.0	97.0 97.0 9.0 201.0 3 10 3.0 3.0 20.0 1 10.0 1 10.0 20.0 1 10.0 20.0 1 10.0 20.0 1 10.0 20.0 2	53.0	145.0		53.0	145.0	-	4	•		53.0	
26.00	10.0   1.0	1.0	97.0		3.0	291.0	m	80	3.		3.0	
2641.0	20.0 1.0 0 4.0 4.0 4 6.0 4 6.0 4.0 4.0 4.0 4.0 4.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	5.0	0.06		5.0	0.06	-	80	::		5.0	
255.0 2.0 2.0 2.0 2.0 2 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	25.00 2.00 2 4 1.0 1.0 2.00 2 5.00 3.00 2 5.00 3.00 2 5.00 3.00 2 5.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00	1.0	10.0		0.0	40.0	4	8	. 4		4.0	
255.0  2641.0  150.0  2641.0  2641.0  2641.0  2641.0  2641.0  2641.0  2641.0  312.0  313.0  3	25.0         2.0         3.0         1.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         2.0         3.0 <td>1.0</td> <td>20.0</td> <td></td> <td>1.0</td> <td>20.0</td> <td>-</td> <td>4</td> <td>1:</td> <td></td> <td>1.0</td> <td></td>	1.0	20.0		1.0	20.0	-	4	1:		1.0	
30.0	30.0         2.0         30.0         1         4         1.         2.0         2.0         2.0         3.0         45.0         3.0	1.0	25.0		2.0	20.0	2	4	2.		2.0	
2641.0 3.0 2641.0 312.0 312.0 312.0 225.0 312.0 325.0 325.0 325.0 326.0	15.0	2.0	30.0		2.0	30.0	-	4			2.0	
2641.0 2641.0 312.	2641.0         54.0         2641.0         1         20.0 <t< td=""><td>1.0</td><td>15.0</td><td></td><td>3.0</td><td>45.0</td><td>3</td><td>•</td><td>3.</td><td></td><td>3.0</td><td></td></t<>	1.0	15.0		3.0	45.0	3	•	3.		3.0	
312.0 312.0 312.0 312.0 325.0 346.0 1920.0 2	225.0         29.0         312.0         1         4         11         29.0           215.0         2.25.0 <td></td> <td>2641.0</td> <td>24.0</td> <td></td> <td>2641.0</td> <td>-</td> <td>2</td> <td>:</td> <td>40.4</td> <td></td> <td></td>		2641.0	24.0		2641.0	-	2	:	40.4		
225.0  225.0  3355.0  346.0  140.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  140.0  346.0  3	225.0         8.1         225.0         1         2         1         6.0         2.0         2.0         2.0         3.0         2.0         2.0         2.0         3.0	29.0	312.0		29.0	312.0	-	4	:		20.0	
116.0   2.0   732.0   2   2   2   2   2   2   2   2   2	116.0         2.0         232.0         2         3         4         2         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         4         2         3         3         3         3 <th< td=""><td>8.1</td><td>225.0</td><td></td><td>8.1</td><td>225.0</td><td>-</td><td>2</td><td>:</td><td></td><td>P.1</td><td></td></th<>	8.1	225.0		8.1	225.0	-	2	:		P.1	
355.0 355.0 346.0 1920.0 2 2 2 1400.0 4.2 1100 3.0 113.5 1150.0 2 2 2 1150.0 2 2 2 1150.0 2 2 2 1150.0 2 2 2 1150.0 2 2 3 1 1 2 2 3 1 1 2 2 3 1 1 2 2 3 1 1 2 2 3 1 1 2 2 3 1 1 2 2 3 1 1 2 2 3 1 1 2 2 3 1 1 2 2 3 1 1 1 2 3 1 1 1 2 3 1 1 3 3 3 3 3 3 3 3 3 1 3 3 3 3 3 3 3	355.0         26.0         710.0         2         2         2         346.0           960.0         346.0         1920.0         2         2         2         346.0           40.0         40.0         1         2         1         4.2         346.0           40.0         12.0         12.0         1         2         1         7.8           50.0         13.5         150.0         25         1         25.0         12.0           10.0         13.5         150.0         25         1         25.0         118.5           10.0         18.5         10.0         50.0         10.0         10.0         118.5           10.0         18.5         10.0         50.0         10.0         118.5         118.5           10.0         10.0         10.0         10.0         10.0         118.5         118.5           10.0         10.0         10.0         10.0         10.0         10.0         118.5           10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0	1.0	116.0		2.0	232.0	2	2	2.		2.0	
950.0  140.0  140.0  170.0  170.0  18	950.0 346.0 1920.0 2 2 2. 346.0 4.2 140.0 140.0 1 2 11. 4.2 7.2 140.0 150.0 25 1 25. 11. 4.2 7.2 140.0 150.0 25 1 25. 11. 4.2 7.3 150.0 25 1 25. 11. 15.0 13.5 150.0 25 1 25. 11. 13.5 150.0 25 1 25. 118.5 150.0 25 1 25. 118.5 150.0 25 1 25. 118.5 150.0 25 1 25. 118.5 150.0 25 1 25. 118.5 150.0 25 1 25. 118.5 150.0 25 1 25. 118.5 150.0 25 1 25. 118.5 150.0 25 1 25. 118.3 3 20.0 25 1 25. 118.3 3 20.0 25 1 25. 118.3 3 20.0 25 1 25. 118.3 3 20.0 25. 1 25. 118.3 3 20.0 25. 1 25. 118.3 3 20.0 25. 1 25. 118.3 3 20.0 25. 1 25. 1 25. 118.3 3 20.0 25. 1 25. 1 25. 118.3 3 20.0 25. 1 25. 1 25. 118.3 3 20.0 25. 1 25. 1 25. 118.3 3 20.0 25. 1 25. 1 25. 118.3 3 20.0 25. 1 25. 1 25. 118.3 3 20.0 25. 1 25. 1 25. 118.3 3 20.0 25. 1 25.	13.0	355.0		26.0	710.0	2	2	2.		26.0	
4.2 140.0 1 1 2 1 4 2 1 1 4 0 0 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1	140.0   1.	173.0	0.096		346.0	1920.0	~	2	2.		346.0	
4.0  4.0  3.0  112.0  112.0  112.0  112.0  113.5  113.5  113.0  113.5  113.5  113.0  113.5  1	4.0         7.8         100.0         25         1         25.         17.8           5.0         13.5         150.0         25         1         25.         12.0           7.0         18.7         175.0         25         1         25.         18.7           1.0         18.5         175.0         25         1         25.         18.7           1.0         18.5         600.0         10         1         10.         18.7           1.0         18.5         600.0         10         1         10.         18.5           1.0         18.5         600.0         10         1         10.         18.5           1.0         1.0         1         10.         1	4.2	140.0		4.2	140.0	-	2	1.		4.2	
3.0 12.0 150.0 25 1 2 1 150.0 25 1 2 1 150.0 25 1 1 150.0 25 1 1 1 150.0 25 1 1 1 150.0 25 1 1 1 150.0 25 1 1 1 1 150.0 25 1 1 1 1 150.0 25 1 1 1 1 150.0 25 1 1 1 1 150.0 25 1 1 1 1 150.0 25 1 1 1 1 150.0 25 1 1 1 1 150.0 25 1 1 1 1 150.0 25 1 1 1 1 1 150.0 25 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6.0         12.0         150.0         25         1         25.         12.0         13.5         150.0         50         1         50.         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         13.5         15.0         13.5         15.0         11.0         1         10.0         1         1         1 <td< td=""><td>.3</td><td>0.4</td><td></td><td>7.8</td><td>100.0</td><td>25</td><td>-</td><td>25.</td><td></td><td>7.8</td><td></td></td<>	.3	0.4		7.8	100.0	25	-	25.		7.8	
3.0  7.0  13.5  13.6  1.0  3.0  18.7  175.0  25.1  2.0  18.5  10.0  2.0  18.5  10.0  2.0  18.5  10.0  2.0  18.5  10.0  2.0  18.5  18.6  18	3.0         13.5         150.0         50         1         50.         13.5           7.0         18.7         175.0         25         1         25.         18.7           1.0         18.5         600.0         50         1         60.0         18.7           3.0         1.0         18.5         600.0         10         1         10.0         18.7           1.0         1.0         18.5         600.0         10         1         10.0         18.7         10.0           1.0         3.5         1.0         50.0         50         1         50.0         10.0 <td>••</td> <td>0.9</td> <td></td> <td>12.0</td> <td>150.0</td> <td>25</td> <td>-</td> <td>25.</td> <td></td> <td>12.0</td> <td></td>	••	0.9		12.0	150.0	25	-	25.		12.0	
7.0	7.0       18.7       175.0       25       1       25.       18.7         10.0       18.5       5.0       5       1       5.0       1       18.5       18.5       18.5       18.5       18.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5       19.3       19.5		3.0		13.5	150.0	20	-	50.		13.5	
1.0	1.0	.8	7.0		18.7	175.0	25	-	25.		18.7	
3.0	60.00         18.5         600.0         10         1         10.         18.5         10.0         10.	0.	1.0			9.0	9	-			:	
3.0 1.0 1.0 1.0 2.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 1.0 2.0 2.0 1.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	3.0       1.0       18.0       6       1       6.       1.0 </td <td>1.9</td> <td>0.09</td> <td></td> <td>18.5</td> <td>0.009</td> <td>10</td> <td>-</td> <td>10.</td> <td></td> <td>18.5</td> <td></td>	1.9	0.09		18.5	0.009	10	-	10.		18.5	
1.0	1.0 1.0 1.1 2.0 1.1 2.0 1.1 3.6 2.0 1.236.5 1.25. 1.1 3.8 80.0 1.236.5 1.9984.0 1249 1 1155. 1143.3 80.0 27.0 27.0 1.3 27.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1	.2	3.0		0.1	18.0	9	-	.9		1.0	
2.0 2.0 2.0 13.6 50.0 2.0 15.6 16.0 15.6 16.0 15.6 50.0 2.0 2.0 2.0 2.0 10.0 2.0 10.0 10.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	1.0       .1       5.0       5       1       5.0       25       3.8         2.0       17.0       50.0       25       1       25       17.0         16.0       175.6       960.0       12       1       15       17.0         27.0       2.0       1       1       1       1.3       27.0       1       1       1.3       27.0       1.3       27.0       1       1       1.3       27.0       1.3       1.3       27.0       1       1.3       27.0       1       1.3       27.0       1       1.3       1.4       1.4       1.4       1.4       1.4       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.3       1.4       1.4       1.4       1.4       1.4       1.4       1.4       1.3       1.3       1.3       1.3       1.3       1.3 <td< td=""><td>:</td><td>1.0</td><td></td><td>3.5</td><td>20.0</td><td>20</td><td>-</td><td>20.</td><td></td><td>3.5</td><td></td></td<>	:	1.0		3.5	20.0	20	-	20.		3.5	
2.0	2.0	••	1.0		-	5.0	2	-	.5		:	
2.0   17.0   50.0   25   1   2   25   1   2   25   1   2   25   1   2   25   1   2   25   1   2   25   1   2   25   1   2   25   1   2   25   1   2   25   1   2   2   2   2   2   2   2   2   2	2.0   17.0   50.0   25   1   25.   1143.3   116.0   1236.5   19984.0   1249   1   1155.   1143.3   116.0   12.0   75.6   50.0   12   1   12.0   75.6   1143.3   12.0   12.0   75.6   1143.3   12.0   75.6   1143.3   12.0   75.6   1143.3   1143.3   12.0   75.6   1143.3   1143.	•2	2.0		3.8	20.0	25	-	25.		3.8	
16.0  80.0  80.0  50.0  50.0  27.0  1.3  27.0  1.3  27.0  1.0  1.0  1.0  1.0  1.0  1.0  1.0	16.0     1236.5     19984.0     1249     1155.     1143.3       80.0     75.6     960.0     12     1     12.     75.6       50.0     2.0     1     1     1.     2.0       27.0     13     27.0     1     1     1.3       50.0     .     .     .     .     .     .       40.0     .     .     .     .     .     .       10.0     .     .     .     .     .     .       10.0     .     .     .     .     .     .     .       10.0     .     .     .     .     .     .     .     .     .       10.0     .     .     .     .     .     .     .     .     .     .     .     .       10.0     . <td< td=""><td></td><td>2.0</td><td></td><td>17.0</td><td>20.0</td><td>25</td><td>-</td><td>25.</td><td></td><td>17.0</td><td></td></td<>		2.0		17.0	20.0	25	-	25.		17.0	
80.0 50.0 50.0 2.0 5.0 40.0 10.0 51.8 480.0 10.0 51.8 480.0 10.0 51.8 480.0 10.0 51.8 480.0 60.0	80.0     75.6     960.0     12     1     12.     75.6       50.0     2.0     50.0     1     1     1.     2.0       27.0     1.3     27.0     1     1     1.     2.0       40.0     .     .     40.0     6     1     6.     10.3       10.0     2.9     .     60.0     6     1     6.     47.9       10.0     2.9     60.0     6     1     6.     2.9       10.0     4.2     53.0     1     1.     4.2       10.0     4.2     53.0     1     1.     4.2       10.0     3.0     350.0     350.0     370.0     370.0       204.0     1     1     1     1     1.0       204.0     1     1     1     1       1.0     3.0     85.0     1     30.0       204.0     1     1     1     1       1.0     1.4     1     1     1       1.0     5.     5.     55.0       5.     55.0     55.0       5.     55.0       5.     55.0       6.0     1     1     1       1.0     1     1	1.0	16.0		1236.5	19984.0	1249	-	1155.		1143.3	. 00
50.0  27.0  1.3  27.0  40.0  40.0  19.6  27.0  10.0  51.8  480.0  51.8  480.0  51.8  480.0  51.8  60.0	50.0     2.0     2.0     1     1     1     1.3     2.0       27.0     1.3     27.0     1     1     1.3     1.3       5.0     19.6     240.0     6     1     6     1     6       10.0     2.9     240.0     6     1     6     1     6       10.0     2.9     60.0     6     1     6     2.9       53.0     4.2     53.0     1     1     6.9     2.9       64.0     7.7     350.0     5     1     6.0     55.0       65.0     3.0     350.0     370.0     370.0       204.0     12.0     204.0     1     1     1       6.0     1.4     1     1     1       1.4     6.0     1     1     1       204.0     1     1     1     1       1.0     3.0     204.0     1     1     1       1.4     6     1     1     1     1       1.4     6     1     1     1     1       1.4     6     1     1     1     1       1.4     6     1     1     1     1       1.4     6 <td>6.3</td> <td>80.0</td> <td></td> <td>75.6</td> <td>0.096</td> <td>12</td> <td>-</td> <td>12.</td> <td></td> <td>75.6</td> <td></td>	6.3	80.0		75.6	0.096	12	-	12.		75.6	
57.0 57.0 57.0 57.0 57.0 57.0 57.0 57.0	27.0     1.3     27.0     1     1     1.3     1.3       5.0     .6     40.0     8     1     6.     19.6       10.0     5.9     60.0     6     1     6.     19.6       10.0     2.9     60.0     6     1     6.     2.9       10.0     2.9     60.0     6     1     6.     2.9       180.0     4.2     53.0     1     1     1.     2.9       64.0     55.0     320.0     5     1     5.     55.0       60.0     7.7     60.0     1     1     1     7.7       1.0     3.0     350.0     390.     1     1     300.     3.0       204.0     12.0     204.0     1     1     1     1     1.       6.0     1.4     1     1     1     1     1.4	2.0	20.0		2.0	20.0	-	-	:		5.0	
5.0 40.0 19.6 240.0 51.8 480.0 53.0 10120.0 55.0 105.0 64.0 64.0 7.7 60.0 10.0 204.0 12.0 204.0 12.0 204.0 13.0	5.0 40.0 19.6 240.0 19.6 10.0 2.0 40.2 10.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	1.3	27.0		1.3	27.0	-	-			1.3	
10.0	40.0       19.6       240.0       6       1       6.       19.6         10.0       21.8       480.0       48       1       44.       47.9         10.0       2.9       60.0       6       1       1.       2.9         53.0       4.2       53.0       1       1.       4.2         180.0       10120.0       165600.0       920       1       756.       8320.3         64.0       7.7       60.0       1       1       1       7.7         1.0       3.0       390.0       390.1       390       3.0         204.0       12.0       204.0       1       1       1       1.         204.0       12.0       204.0       1       1       1       1.       1.	-	2.0		9.	40.0	8	-	8.		9.	
10.0	10.0  10.0  2.9  53.0  10.0  4.2  53.0  10.120.0	3.3	0.04		19.6	240.0	9	-	.9		19.6	
53.0 2.9 50.0 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10.0 53.0 10120.0 10120.0 10120.0 10560.0 55.0 10.0 55.0 10.0 10.0 10.0 10.0 1	:	10.0		51.8	480.0	43	-			47.9	•
53.0 180.0 10120.0 165.0 55.0 180.0 55.0 180.0 7.7 50.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	53.0 180.0 10120.0 165600.0 55.0 1756. 55.0 1756. 55.0 1757. 100 100 100 100 100 100 100 100 100 10	.5	10.0		5.0	0.09	9	-	.9		5.9	
180.0 10120.0 165600.0 920 1 55.0 320.0 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	180.0 10120.0 165600.0 920 1 756. 8320.3 54.0 54.0 54.0 5.0 55.0 55.0 55.0 55.0	4.2	53.0		4.2	53.0	-	-	:		4.2	
64.0 55.0 320.0 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	64.0 55.0 320.0 5 1 5. 55.0 55.0 1.0 1.0 1.0 1.0 3.0 3.0 1.0 1.0 3.0 3.0 1.0 1.0 3.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	11.0	180.0		10120.0	165600.0	920	-	756.		8320.3	164.
60.0 7.7 50.0 1 1 1 1.0 3.9 390.0 390 1 85.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	60.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	11.0	64.0		55.0	320.0	S	-	5.		55.0	
1.0 3.9 390.0 390 1 85.0 3.0 85.0 1 1 204.0 12.0 204.0 1 1	204.0 3.0 3.00.0 3.0 1 390. 204.0 12.0 204.0 1 1 1. 6.0 1 1 1.	7.7	60.09		7.7	0.09	-	-	:		7.7	
204.0 12.0 2	204.0 12.0 204.0 1 1 1 6.0 1 1 1 6.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.	1.0		3.0	390.0	390	-	390.		3.0	
204.0	204.0 12.0 204.0 1 1 1. 6.0 1.4 6.0 1 1 1.	3.0	85.0		3.0	85.0	-	-	:		3.0	
6-0	6.0 1 1 1.	12.0	204.0		12.0	204.0	-	-	:		12.0	
0.0		1.4	0.9		1.4	0.9	-	-	:		1.4	

Table VII-3(c) (Continued)

DEFIC- IENCY								7.		;					2.																											
T/E**** CUBE	4.	11.7	84.6	44.6	193.6		1.0	397.5	8.1	84.8	83.2	138.7	132.2	18.0	545.1	25.7	22.1	1.5	5.0	1.3	0.9	6.0	11.0	50.4	58.7	86.2	144.0	10.5	5.0	34.3	3.2	6.	:		20.0	1.4	.5	9.	.3	125.0	0.	2006
*****REDUCED																																		38.0								
* * * * * * * * * * * * * * * * * * * *	2.	•	11.	7.	52.	2.	:	28.	2.	32.	22.	17.	19.	2.	22.	• •	8.	:	:	7.	:	12.	.1	8.	10.	12.	.8	7.	5.	2.	:	:		:	:	:	:	:	:	:	:	:
CRIT	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	9	2	8	2	2	2	2	2	0
1/E	~	v	=	1	29	8	-	35	2	36	22	17	19	2	54	¢	60	-	-	1	-	12	-	80	10	15	60	1	S	2	-	-	===	-	-	-	-	-	-	-	-	-
T/E WEIGHT	4.0	240.0	440.0	295.0	472.0	24.0	0.09	5250.0	392.0	204.0	88.0	2754.0	2850.0	262.0	8472.0	228.0	800.0	31.0	20000	49.0	84.0	84.0	2.0	856.0	1400.0	3084.0	2640.0	134.0	0.09	450.0	30.0	18.0	1111.0	1054.0	163.0	21.0	16.0	16.0	10.0	1832.0	1.0	1890.0
T/E CUBE	4.	11.7	84.6	44.6	210.0		1.0	490.0	8.1	95.8	83.2	138.7	132.2	18.0	0.009	25.7	22.1	1.5	2.0	1.3	0.9	0.9	11.0	50.4	58.7	86.2	144.0	10.5	2.0	34.3	3.2	6.	1:1		20.0	1.4	.5	٠.	•3	125.0	0.	2.06
TZE																																		38.0								
ITEM WE IGHT	2.0	*0.0	40.0	85.0	8.0	12.0	0.09	150.0	196.0	14.0	0.4	162.0	150.0	131.0	353.0	38.0	100.0	31.0	200.0	7.0	84.0	7.0	5.0	107.0	140.0	257.0	330.0	62.0	12.0	0.06	30.0	18.0	1.0	1054.0	163.0	21.0	16.0	15.0	10.0	1832.0	1.0	1690.0
LTEM		2.0	7.7	6.4	3.6	4.	1.0	14.0	4.0	2.7	3.8	8.2	7.0	0.6	25.0	4.3	2.8	1.5	5.0	•2	0.9	• 5	11.0	6.3	5.9	7.2	18.0	1.5	1.0	6.9	3.2	6.	•		20.0	1.4	· .	9.	£.	125.0	••	2.06
SOUARE																																		38.0								
TAM	C4680	C4690	C4 790	C4870	C4880	C4930	C4450	C4980	C5090	CS110	C5200	C5320	C5400	C5410	C5820	C5870	C5930	C5990	C6010	C6140	C6215	C6220	C6260	C6370	C6388	C6390	C6410	C6490	C6500	C6510	09993	C6670	C6684	06000	00100	00300	00400	00410	06500	00725	99100	00110

Table VII-3(c) (Concluded)

DEFIC- IENCY	'n		1.	5.	3.																				:						
CUBE						4.3	1.6	1.0	:	4.0	4.8	17.9	0.0	36.0	68.8	45.5	144.0	496.0	0.0	0.0	0.0	1:1	9.	2.0		4.2	1.3	2.0	:	3.4	3877-014575-0
*****REDUCED T/E****	596.2	70.3	860.9	441.7	1006.8																				331.7						3877.01
014	15.	-1	• 9	25.	17.	36.	*	::	2.	:	12.	2.	110.	12.	32.	35.	12.	8.	36.	;	*	36.	20.	2.	7.		*	2.	1:	B	3756.
CRIT	80	4	œ	œ	60	-	-	80		80	•	89	æ	60	8	89	8	80	60	8	60	80	8	-	8	8	8	4	2	2	
1/E 01Y	18	-	1	30	20	36	4	-	2	-	12	2	110	12	35	35	12	80	36	4	4	36	50	2	80	-	4	2	-	e	4051
T/E WE1GHT	10260.0	2780.0	51590.0	27000.0	48000.0	108.0	28.0	10.0	5.0	68.0	84.0	216.0	0.0	324.0	480.0	840.0	0.009	0.096	0.0	0.0	0.0	72.0	20.0	0.9	3360.0	68.0	32.0	10.0	2.0	117.0	412462.0 4051
T/E CUBE						4.3	1.6	1.0	:	0.4	4.8	17.9	0.0	36.0	68.8	45.5	144.0	496.0	0.0	0.0	0.0	1.1	9.	2.0		4.2	1.3	2.0	•	3.4	16656.6
SQUARE	828.0	71.0	938.0	540.0	1220.0																				360.0						4431.0
ITEM	570.0	2780.0	7370.0	0.006	2400.0	3.0	7.0	10.0	1.0	68.0	7.0	108.0	0.0	27.0	15.0	24.0	20.0	120.0	0.0	0.0	0.0	2.0	1.0	3.0	450.0	68.0	8.0	2.0	2.0	39.0	
CUBE						:	4.	1.0	••	4.0	4.	8.9	0.0	3.0	2.2	1.3	12.0	62.0	0.0	0.0	0.0	0.	0.	1.0		4.2	r.	1.0		1:1	TALS
SQUARE	46.0	71.0	134.0	18.0	61.0																				45.0						GRAND TOTALS
TAM	00840	06800	01020	01100	01160	E0080	E0090	E0180	E0210	E0230	E0290	E0320	E0892	E0900	E0920	E0990	E1060	E1 090	E1155	E1156	E1157	E1 180	E1240	E1260	E1480	E1530	E1760	E1900	E1960	E2030	

TODAYS DATE 03/02/76
OR INDEX(SQUARE) = 85.54
OR INDEX(CUBE) = 96.31
OR INDEX(TOTAL T/E) = 95.38

Table VII-3(d)

T/E ITEM DEFICIENCIES OF MIO38 WHEN CONSTRAINED TO 90%, 85% AND 75% OF AUTHORIZED T/E LIFT REQUIREMENT

TAM	N. to Constant	Authorized	Constra	Constrained T/E Quantity	Quantity	Square
Number	Nomencialure	1/E Quantity	%06	85%	75%	Loaded Items (*)
C3020	Armor, body	1249	1	•	76	
C4110	Bag, water, 36 gal	48		•	4	
C4290	Carrier, grenade, cloth	756	70	105	164	
C4880	Food container	59	က	4	7	
C4980	Heater, immersion	35	က	4	7	
C5110	Jug, vacuum, 3 gal	36	2	2	7	
C5820	Range, outfit, field	24	ı	1	2	
D0840	Trailer, amphib, cargo ½ ton	18	1	2	3	*
D1020	Truck, cargo, 1½ ton	7	. 1	•	1	*
D1100	Truck, platform, utility, ½ ton	30	8	4	5	*
D1160	Truck, utility, ½ ton	20	2	2	3	*
E1480	Rifle 106mm	8	•	-	1	*

aid is the computational power of the computer, leaving the staff planner free to apply judgmental considerations to accurately presented data. This action can also be done at any command level, from the company/battery to any higher level staff having access to the computer system supporting CALAS.

For the sample unit T/Es of Table VII-3, a value of 85 percent is selected as the acceptable constraint level. For this level a 29 percent short fall still exists. This means that the exercise of other options within CALAS is now required.

Table VII-3a, b, c, d illustrates the information the operational planner obtained from the output listings of the CONTEAM Program to assist him in making the decision as to "what" and "how much" equipment can be safely removed from a unit's T/E but still leave the unit operationally viable. The heading of the output lists the unit and its description, plus the percentage and amount the unit is being constrained in both bulk and square. The body of the listings itemizes each item of equipment in the unit's authorized T/E. For each T/E item, the square, cube, weight, T/E quantity, and criticality is printed. Next to the authorized T/E quantity is the reduced quantity and item deficiency obtained after exercising the model with the applied constraint value in the heading. Totals are given for the square, cube, and weight of the unit, both before and after the unit is constrained. At the bottom of each listing are three operational readiness indices that indicate the degree the elimination of T/E items has reduced the unit's operational readiness -- as far as square items, cube items, and the combination of both square and cube items are concerned. The reader may want to refer to Appendix F for a detailed explanation of the rationale and mathematics of the CONTEAM model and operational readiness index. By referring to Appendix C, Part 4, he may obtain a more detailed explanation of CONTEAM's output.

At this point the reader should be reminded that in assigning criticalities, the importance of an item of equipment to a unit's mission can be derived by relating its usage to a specific function of that unit and, in turn, determining the relative importance of the specific functions to the unit's combat mission. M1038 has primary functions of infantry combat/small arms employment, mobility, and communications; secondary functions of intelligence, demolition/obstacle clearance, medical, air support control, power generation, and comm/elect maintenance; and tertiary functions of supply, maintenance (except comm/elect) and service support. Any T/E item that supports M1038's primary function was assigned a criticality of 8. Criticalities of 4 and 2 were assigned to those items that supported M1038's secondary and tertiary functions. If the T/E item did not serve either the unit's primary, secondary, or tertiary function, it was given a criticality of 1. Examples of the criticality assignment can be seen by again referring to Table VII-3. TAM A0005, a radio set accessory kit, serves one of M1038's primary functions, communications, and, therefore, has a criticality of 8. A0710, a generator signal, serves the secondary function of comm/elect maintenance and has a criticality of 4.

When the planner is confronted with the reality that he lacks the lift capacity to carry a unit's, such as M1038, entire authorized T/E in the assault echelon shipping, he may consult a series of constrained T/E tables for that unit which itemizes the equipment to be left out of the AE lift for each constraint. Table VII-3 depicts the items of equipment that would be omitted from the load list of M1038 under constraints of 90, 85, and 75 percent. Because of the weighting factors applied to each assault echelon unit, explained earlier, the true constraints for M1038 are 95, 92.5, and 87.5 percent.

Table VII-3d summarizes the numbers of each T/E item that would be eliminated from the complete T/E of unit M1038, as determined by CONTEAM for the various constraints. By reviewing such a table of deleted equipment, the planner is better able to determine the maximum constraint acceptable for a unit when it is forced to reduce its normal T/E. The planner is also in the position to make manual adjustments in the constrained T/E if he deems it necessary. Suppose, for example, he observes that one E1480, a 106mm rifle, is omitted from the load list of M1038 when it is constrained to 75 percent of full strength. Further, assume he determines the omission of this item to be unacceptable. It is perfectly permissible for him to include this item in the final load list, but only after he has eliminated one or more square loaded items of comparable square. He may adjust the final constrained T/E by hand, or he may assign artificially high criticalities to those items he wishes to force into the final load list and then rerun CONTEAM.

Careful examination of Table VII-3 results in the following general characteristics of the CONTEAM Model. For TAM items that occur in a unit's T/E with authorized quantities of 1 to 20, the program will include TAMs with the highest criticality and exclude TAMs with the next-to-highest criticality when the constraint amounts to 65-75 percent of the space required to load the unit's full strength T/E. Of the TAMs with low criticality, the bulky ones will be excluded, but usually only in part. Nonpriority TAMs may be completely excluded from the constrained T/E.

For items that appear in the unit's T/E with authorized quantities of 40-1200, the model will exclude some portion of the full T/E quantity in almost every case--even for the highest criticality items. This is purely a function of CONTEAM's algorithm as it begins to favor the first units of low priority items over, say, the 100th unit of a

higher priority item. Again, experience shows these results to be useful; however, the model can be modified if the planner feels this is necessary.

Each unit in the assault echelon is submitted to constraints similar to those applied to M1038, and a unit-by-unit inspection of the tentative, constrained T/Es is made. Finally, after each unit's T/E is stripped of the items of equipment the planner determines can be left out of the assault echelon, he is in the position to determine if his constrained force is within his lift capacity.

The CCF model also prints a table of constrained cargo values for bulk and square loaded items for each unit and a table of factored cargo categories found in Appendix C. These tables are useful when evaluating the effects on unit T/Es from applying constraints. The tables should be used when evaluating the constrained T/E of Table VII-3. As an example of the information contained in Appendix C, Table VII-4(a) contains three units, showing the part of bulk cargo that is T/E and the

Table VII-4(a)

# CONSTRAINED CUBE FOR CLASSES IIW AND VIIW NONSQUARE AND VIIW SQUARE (T/E Categories Only)

		Constraint	= .75		
Unit	Weighted Code	Constrained Bulk	Bu1k	Constrained* Square	Square
м1038	1	515	589	3908	4427
M1128	1	321	367	20322	23016
M8821	3	33	53	1380	2181

<sup>\*</sup>These values include square mountout.

Table VII-4(b)

CONSTRAINED FACTORED CARGO CATEGORIES

				Constr	Constraint = .75			
Unit	Bulk Total <sup>1</sup>	Constrained T/E <sup>2</sup>	МО3	OMA <sup>4</sup>	Constrained Bulk <sup>5</sup>	Square T/E <sup>6</sup>	Constrained Square T/E <sup>7</sup>	Constrained Square <sup>8</sup>
M1038 1	1014.4	515.0	427.3	0	942.0	4426.8	3873.4	3908.0
M1128	1678.5	320.8	1312.8	0	1633.0	23015.8	20138.8	20322.0
M8821	87.0	33.3	33.8	0	67.0	2180.6	1362.9	1380.0

Total bulk in MT.

 $^2$ Constrained T/E in MT.

3 Mountout in MT.

4 Organizational Maintenance Activity (OMA) for classes IIA and VIIA nonsquare.

Social constrained bulk cargo.

6 Square loaded T/E items.

Constrained square loaded T/E items.

8 Total constrained square loaded items. reduced measurement tons of the T/E from applying the constraint (CON BULK). The T/E for square loaded items in square feet is also shown, with the reduced T/E square feet also from applying the constraint. These figures represent the amount of a unit's T/E to be loaded and the constrained allotted space available for loading provided by the weighted constraint. Table VII-4(a) also shows the weighted constraint code used by the model to compute the material reduction. Table VII-4(b) shows additional cargo categories factored from the totals. It should be remembered that the cargo is composed of T/E and mountout. Using the list of items deleted from the T/E accounting for the reduced amount of T/E contained in Table VII-3, an evaluation can be made of the acceptability of a given constraint on the reduced T/E of a unit.

## 5. Varying the Mountout

The next option to be exercised in finding the solution to the constrained loading problem is to change the DOS for the mountout carried by the AE. Since the run parameters for the MAGTF data were 15 DOS for the AE, a change to 10 DOS will be tried to determine the significance of the reduction in lift short fall. Table VII-5 presents the CCF Model results from this change. It is noted that the unconstrained short fall from this option is 32 percent, indicating that a 5 DOS reduction in mountout permitted total loading to occur at 76.5 percent constraint instead of at 70.8 percent for 15 DOS. Graphical results are found in Figure VII-3. Here again, the planner consults Table VII-3 to evaluate the T/E reduction occurring at 77 percent, when constrained loading is indicated, along with the desirability of limiting accompanying supplies to 10 DOS for the AE.

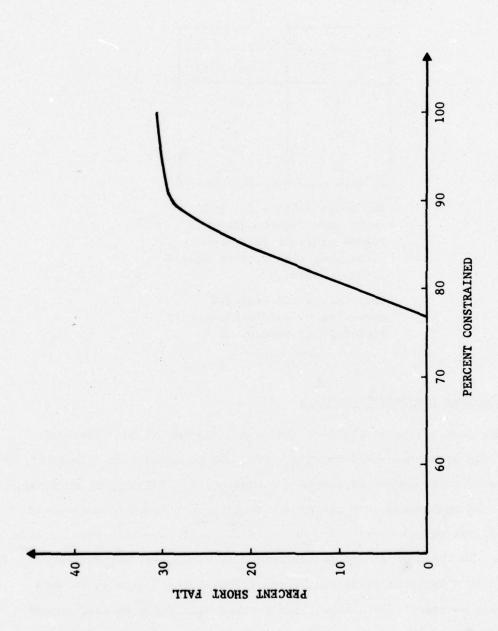


FIGURE VII-3. WEIGHTED CONSTRAINED UNIT LOADING VERSUS PERCENT SHORT FALL FOR AE UNITS USING 10 DOS MOUNTOUT

Table VII-5
WEIGHTED CONSTRAINED UNIT LOADING
VS PERCENT SHORT FALL

cent
Constraint
100%
90
85
80
77

<sup>\*</sup>The short fall is for bulk cargo since square cargo is loaded at about 88 percent permitting reallocating square space to bulk.

## C. Changing the Force Structure

The next option available to the staff planner is the elimination of certain units and their functions from the AE troop list. Those eliminated units would, of course, be embarked in AFOE support shipping. It must be emphasized that the option to eliminate certain units would exist if the actual mission and expected tactical situation permits such action. In the analysis of the notional MAF deployment without the effects of a tactical situation, certain units are eliminated to show tradeoffs between reduced total lift requirements and a reduced amount of material eliminated from the included units. In other words, an evaluation must be made of the relative advantages to be gained from

Constraints are weighted according to unit's mission as explained in Section VI.

eliminating whole units, thus changing the force structure and decreasing the materiel eliminated from remaining units as opposed to greater reductions from all original units and a possible change in the amount of accompanying supplies.

The units chosen for elimination are listed in Table VII-6. These units are characterized by the possibility that their deployment ashore may not be required for a sufficient period of time to permit their being embarked and unloaded from the AFOE support ships. The action to remove units from the AE troop list and include them in the AFOE constitutes the phasing of units or detachments into the objective area at a later time-after unloading of AFOE units begins. Since there is some risk that the eliminated units may be required ashore before, say D+5, the factors affecting the earliest unloading times for the AFOE are revelant to the study. Analysis of unloading assault shipping and the beach support and cargo handling problems ashore were therefore included in the study. Results from this analysis and the practicality of phasing ashore certain original AE units from AFOE support ships will be presented in later subsections.

### 1. Third and Fourth Echelon Maintenance Elimination

Possible candidates for phased entry into the objective area are the units and detachments of the maintenance battalion, FSSG. Instead of deploying these organizations ashore from assault shipping, two maintenance contact teams for each area of maintenance, i.e., engineer, motor transport, ordnance, communication/electronics, are included in the assault echelon. Each contact team would consist of one vehicle and two experienced technicians with the necessary equipment and some highly demanded repair parts. Repair of equipment would be generally restricted to component replacement. The maintenance concept for the FSSG provides

Table VII-6

ELIMINATED AE UNITS

Function	Unit	Quantity	Description
CSS/Maintenance	M3223X M3233F		Det MT Maintenance Company MT Maintenance Company /-/
	M3243X	1	Engineer Maintenance Company
	M3247F	1	H&S Company /-/ Maintenance Bn
	M3253X	1	Electronic Maintenance Company
Force Engineer	M0305	1	Support Company /-/ Engineer Spt Bn
	M0307	1	Hq Company /-/ Engineer Spt Bn
	M3751X	1	Bulk Fuel Company, Engineer Spt Bn
	M3753X	2	Engineer Company, Engineer Spt Bn
Combat Support	M4193	1	175 Gun Battery
	M4201	1	Searchlight Battery
	M4226	1	Hq Battery, Forward Air Group
	M8621X	1	Missile Battery
Aviation CSS	M8821	2	MATCU
	M8914X	2	H-MS (single site)
	M8921	2	MABS (single site)

for contact teams as a part of normal maintenance procedures. Additional personnel from the maintenance battalion would be required to coordinate the preliminary maintenance effort. The landing force supply of the AE includes a large pool of operationally ready float items and secondary reparables for replacement of "wash out" end items and components. In effect, this option provides for a minimum size detachment from maintenance battalion to conduct emergency repairs and end item replacement during the period from D-Day to about D+3 to D+7 when the MAF maintenance organizations are unloaded and put into operation. The time phased deployment of maintenance unit increments are dependent on the timing of the unloading of assault shipping. As stated, a discussion of this problem is presented later.

The tradeoff in lift requirements is presented in Table VII-7. The reduction in square loading requirements will have a significant impact on overall lift requirements when combined with the other options to be discussed for AE troop list modification. These results, of course, are for a notional MAF structure without the specification of a mission. The reduction in lift obtained in this analysis demonstrates how incremental phasing of units into the objective area reduces lift requirements for the AE embarked in assault shipping, permitting minimum support levels for committed units during a short period of time. A specific mission and scheme of maneuver ashore in an actual operation will, of course, dictate the bounds on tailored maintenance detachments which are included in the AE and phased ashore from the AFOE at some later time.

## 2. Motor Transport Functions

The greatest demand for square loaded space in assault ships is derived from the number of vehicles embarked. Motor transport assets provide tactical mobility for combat units, mobility for unit cargo,

Table VII-7

AMPHIBIOUS LIFT TRADEOFF FROM SUBSTITUTING MAINTENANCE
CONTACT TEAMS FOR MAINTENANCE UNITS IN THE AE

Unit	Bulk/MT	Square
M3223X	571	11276
M3243X	814	7131
M3233F	43	1455
M3247F	127	1975
M3253X	210	2741
Total	1765	24578
8 Contact teams*		1480
Net lift reduction	1765	23098

<sup>\*</sup> Contact team materiel is mobile loaded in one vehicle per team.

supply point distribution capability for artillery and tank units, and logistic mobility in support of the development of beach support (BSA) and logistic support areas (LSA) ashore. In the area of constrained amphibious lift assets, excess motor transport included in embarked materiel cannot be tolerated. Therefore, careful planning must be exercised when preparing a troop list for an actual operation to include only those motor transport assets that must be landed from assault shipping. Incremental phasing of excess vehicles or detachments of motor transport units into the objective area via the AFOE after considering time delays constitutes this alternative course of action. A major consideration is the expected time when sufficient terrain in the objective area is controlled to permit the utilization of vehicles ashore to any great degree.

An analysis<sup>1</sup> of the number of vehicles required to conduct beach clearing operations sufficient to prevent congestion in the beach support area and to permit movement of material smoothly from the BSA to the LSA provides the source for determining the minimum number of vehicles for this function. Table VII-8 lists these vehicle quantities.

Table VII-8

EQUIPMENT NECESSARY TO SUPPORT
BEACH CARGO HANDLING FUNCTION

Equipment	Quantity
Rough terrain forklift	20
Beach crane	6
2½-ton truck	182
5-ton truck	48
12-ton semi	20
Total 5-ton equivalents	179

When comparing the quantities of Table VII-8 to the vehicles in the CSS units of the AE, a sufficient number of vehicles and forklifts were included. Table VII-9 shows these quantities. Since many of these vehicles are not part of a motor transport organization, their use in the logistics mobility function must be assumed for at least three days.

The CSS structure and its detachments have been designed at minimum support levels, indicated by the values in Table VII-9. No reduction in these vehicles by units was indicated. In fact, a shortage of fourteen 5-ton equivalents is observed. The remaining vehicles may also be obtained from other units temporarily to keep the total number of vehicles embarked in the AE at a minimum. When AFOE units begin to

Table VII-9

LOGISTIC SUPPORT VEHICLES AE

Equipment	Quantity
Forklifts	41
2½-ton trucks	184
5-ton trucks	72
12-ton semi	1
Total 5-ton equivalents	165

land, a sufficient number of vehicles are included in the CSS structure<sup>2</sup> to perform all missions. The scenario for this study included the landing of two RLTs by helicopter. Because of this, a total of five CH-46 squadrons are embarked in assault shipping. These helicopters will also be available to provide some tactical and logistical mobility to the AE after the lift of assault troops is completed, and before the landing of additional motor transport assets. Here again, the existence of a mission and tactical situation will prescribe tailored motor transport detachments. As a matter of interest, the original notional MAF AE had 483 5-ton equivalents in vehicles from all units.

## 3. The Force Engineer Function

Force engineer units have been included in the AE troop list of the CSS notional MAF. In addition, the Division Support Group has an engineer battalion performing the combat engineer function, and the Naval Beach Group has the Naval Amphibious Construction Battalion for engineer operations in the beach areas. Under certain circumstances, force engineer units may be phased into the objective area from the AFOE without loss of any combat capability to the AE. The tradeoff in reduced lift requirements is shown in Table VII-10.

Table VII-10

AMPHIBIOUS LIFT TRADEOFF FROM PHASING FORCE ENGINEER UNITS INTO THE AOA FROM AFOE SUPPORT SHIPS

Unit	Bulk/MT	Square
1 M0305F	212	11914
1 M0307F	24	571
1 M3751X	2220	7847
2 M3753X	1602	17768
Total	4058	38100

Phasing these units into the objective area at a later time provides a significant reduction in lift requirements for the AE.

## 4. The Combat Support Function

Certain combat support functions provided by units included in the AE may also be candidates for phased deployment into the objective area. The units selected for phased deployment are listed in Table VII-11.

Table VII-11

COMBAT SUPPORT UNITS SELECTED FOR PHASED DEPLOYMENT

Unit	МТ	Square
M4226	677	8661
M4201	67	2019
M4193	417	10497
M8621X	115	4831
Total	1276	26008

Phasing these units provides another significant reduction in the lift requirements of the AE.

Most of these reductions constitute the field artillery group (FAG) with one 175mm gun battery. Two general support batteries were included with the AE, i.e., one 8" howitzer battery and one 175mm gun battery. The division artillery regiment also includes three 155mm howitzer batteries. Limited naval gunfire ships and the planned close air support serve as other means of fire support for the landing force. The mission and tactical situation will provide the deciding factors for phasing the FAG units into the objective area.

In the case of the light antiaircraft missile battery, deployment tactics generally prohibit one battery deployed alone without the usual control agencies from the tactical air control system. The degree of air defense added by including one battery is generally not significant. Many arguments for and against, including the battery in the AE, could be advanced. The tradeoff in lift requirements is evident from Table VII-11.

#### 5. The Aviation CSS Units

Certain aviation units are present in the AE to be landed for the purpose of operating a Short Air Field for Tactical Support (SATS), or expeditionary airfield. Other units provide intermediate level maintenance when operating ashore to the aircraft squadrons initially embarked in the LPAs or LHAs. Current Marine Corps policy, as well as the assault shipping short fall, prohibits loading SATS equipment in assault shipping. The units providing intermediate level maintenance do not perform their primary function while embarked in assault shipping since all the AE aircraft operate from the LPHs and LHAs. The possibility exists for phasing the units in Table VII-12 into the objective area from AFOE support ships without loss of operational capability to the AE.

Table VII-12

AVIATION CSS UNITS SELECTED FOR PHASED DEPLOYMENT

Unit	MT	Square
2 M8914X	360	9602
2 M8821	174	4362
2 M8921	6476	34474
Total	7010	48438

The tradeoffs in reduced amphibious lift requirements from phasing the units in Table VII-12 are very significant.

# 6. The Effect of Incremental Phasing of Units Into the Objective Area

The tradeoff in lift requirements from phasing units ashore from AFOE support ships in the preceding section is presented in Figure VII-4. The curve in this graph indicates a reduction in total lift requirements which are from 77,624 to 63,704 measurement tons, and from 786,926 to 654,815 square feet. The percent short fall in loading assault shipping is reduced from 39 to 9 percent. A weighted constraint of 93 percent enables loading of the AE.

While the extent of phasing certain units and their functions ashore from the AFOE support ships, presented here, may be greater than would be acceptable under an actual operational commitment, the dramatic effect in reduced lift requirements of removing these units from the AE troop list is inescapable. Figure VII-5 compares the curve of the CSS notional MAF AE constrained loading analysis, from Figure VII-1, with the reduced AE force structure of Figure VII-4. The effect of any variations considered acceptable to the commander and his staff in the

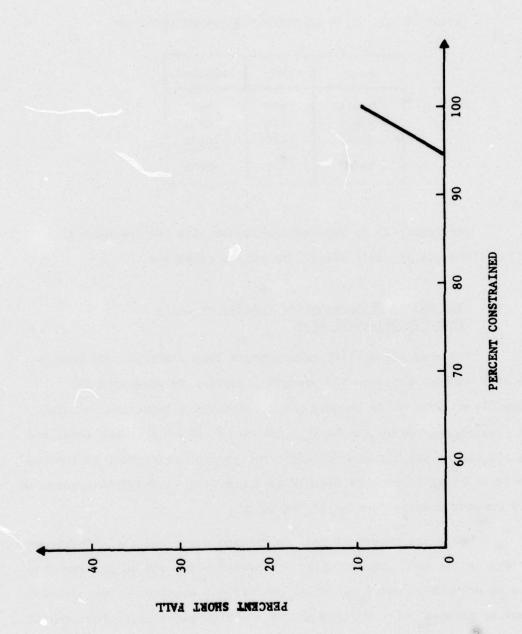
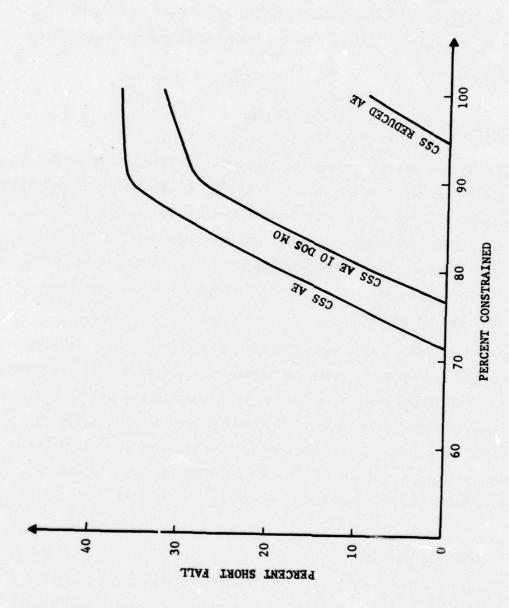


FIGURE VII-4. WEIGHTED CONSTRAINED UNIT LOADING VERSUS PERCENT SHORT FALL FOR REDUCED AE FORCE STRUCTURE



COMPARING THE AE OF THE CSS NOTIONAL MAF WITH THE REDUCED AE FIGURE VII-5. WEIGHTED CONSTRAINED UNIT LOADING VERSUS PERCENT SHORT FALL FORCE STRUCTURE

force structure can be visualized from the two curves of Figure VII-5. The combinations of changing the troop list, the DOS of mountout, and an acceptable constraint level provide the procedure for solving the constrained amphibious lift problem. With a change in the scenario to include airlift, an additional curve may be constructed on the same graph as Figure VII-5 to indicate that effect on the constrained loading problem.

# D. The Timing Problem in Phasing Materiel Into the Amphibious Objective Area

The time when ships carrying the AFOE should arrive in the objective area would be dependent on the unloading rate of assault shipping, which, in turn, permits unloaded ships to depart, limiting the number of ships in the area. Two additional considerations are the ability of organizations controlling the beach to keep cargo moving into logistic support areas without congestion, and the availability of Navy crews to unload common user sealift ships.

The MMROP states that a number of AFOE support ships will arrive in the objective area on D-Day, with the remainder arriving by D+5. It has been previously noted that the unloading rate of assault ships, to a large degree, controls the timing factor of how long after D-Day AE troop units and detachments phasing ashore from the AFOE will be landed. Therefore, an analysis of the problems of unloading assault shipping becomes relevant to the constrained amphibious lift problem.

## 1. The GAMUT Simulation

SRI has conducted a number of studies of amphibious assault landing craft for the Naval Ship Systems Command<sup>3</sup>. The analytical support for these studies was provided by a computer simulation model called

GAMUT. This model, "...simulates all of the principal actions in an amphibious assault, including the activities of LVTs, landing craft, helicopters, and ships. It assesses attrition, monitors the status of off loading and of delivery to the shore, and collects statistics useful in analysis". One of the outputs from GAMUT needed in this study are the offloading rates of amphibious assault ships. In order to add the additional dimension of timing to the phasing of units into the objective area from the AFOE, GAMUT runs were made using MAGTF lift data in order to compute the unloading rates for the assault ship types used in this analysis. Runs were made using conventional landing craft with standoff distances of 5 and 25 nautical miles (nmi), and with advanced landing craft using a 25-nmi standoff distance. Table VII-13(a) lists the input parameters for runs 1 and 2 for conventional landing craft. Table VII-13(b) lists the input parameters for run 3 using advanced landing craft.

## 2. Simulated Results

Results from runs 1 and 3 are contained in Tables VII-14 and VII-15. The rates for only run 2, using conventional landing craft at a 5-nmi standoff distance, are listed in Table VII-16. At a 25-nmi standoff distance, the LVTs must be transported to the line of departure by the ships in which they are embarked. When using advanced landing craft, the LVTs were also carried to the line of departure, but by the advanced landing craft.

The obvious difficulties of this procedure for the conventional landing craft at 25 nmi run tend to reduce its usefulness. Unloading times for this run were therefore not presented.

Table VII-13(a)

# PROGRAM GAMUT INPUT PARAMETERS: RUNS NO. 1 AND NO. 2

	Type 1	Type 2	Type 3	A11
	Craft	Craft	Craft	Craft
Craft	LCM6	LCM8	LCU	
Number	111	34	40	185
Speed (kts)	8	8	10	
Capacity (pounds)	68,000	120,000	380,000	
	Type 4	Type 5	Type 6	A11
	Helo.	Helo.	Helo.	Helo.
Helicopter	UH-1N	Сн-46	СН-53	
Number	0	90	63	153
Speed (kts)	130	130	150	
Capacity (pounds)	2,500	4,900	8,600	
Special situation at 20	hours			
Standoff distance, naut	ical miles	s Run	No. $1 = 25$	5, Run No. $2 = 5$
Sea state		03		
Number of small craft d	eckloaded	48		
Percent of cargo availa	ble to he	los 50		
Beach slots, ACVs		0		
Beach slots, LPHs		32		
Number of LST causeways		4		
Time to install causewa	ys (minute	es) 240		

LVTs discharged near the waterline by well-ship. General unloading starts after 350,000 sq ft of vehicles have been offloaded. Attrition rates decrease exponentially with time.

Table VII-13(b)

# PROGRAM GAMUT INPUT PARAMETERS: RUN NO. 3

	Type 1	Type 2	Type 3	A11
	Craft	Craft	Craft	Craft
Craft	C30	P125	Jeff(B)	
Number	92	0	70	162
Speed (kts)	50	35	50	
Capacity (pounds)	30,000	125,000	150,000	
	Type 4	Type 5	Type 6	A11
	Helo.	Helo.	Helo.	Helo.
		1010.	He 10:	ile to:
Helicopter	UH-1N	CH-46	CH-53	
Number	0	90	63	195
Speed (kts)	130	130	150	
Capacity (pounds)	2,500	4,900	8,600	
Special situation at 2	0 hours			
Standoff distance, nau		es 25		
Sea state		03		
Number of small craft	deckloads	32		
Percent of cargo avail	able to he	elos 50		
Beach slots, ACVs		32		
Beach slots, LPHs		0		
Number of LST causeway	rs	4		
Time to install causew	ays (minut	es) 240		

All LVTs preloaded on craft.

LVTs discharged near the waterline by craft.

General unloading starts after 350,000 sq ft of vehicles have been offloaded.

Attrition rates decrease exponentially with time.

Table VII-14

SHIP UNLOADING RATES AND TIMES: CONVENTIONAL LANDING CRAFT (Run No. 1, 5-nmi Standoff)

	Ship No.	Туре	Tons (short tons)	Rate (tons/hr)	Hours	
1	30	LKA	3,006	88	34	
2	31	LKA	3,031	88	34	
3	32	LKA	3,006	88	34	
4	34	LKA	1,455	88	17	
5	48	LKA	1,653	88	19	
6	49	LKA	1,094	88	12	
7	33	LPA	644	88	7	
8	47	LPA	1,722	88	20	
9	2	LHA	3,156	74	43	
10	2	LHA	3,156	74	43	
11	2	LHA	3,156	74	43	
12	2	LHA	3,156	74	43	
13	7	LPD	1,330	64	21	
14	8	LPD	1,383	64	21	
15	9	LPD	1,197	64	19	
16	10	LPD	1,257	64	20	
17	11	LPD	1,110	64	17	
18	12	LPI	1,305	64	20	
19	41	Total	1,011	64	16	
20	42	LPD	1,281	64	20	
21	43	LPD	1,152	64	18	zes
22	44	LPD	1,331	64	21	I
23	46	LPD	1,329	64	21	
24	13	LSD)	.,,,,	-		
25	14	LSD		ied 48 LVTs w		
26	15	LSD (		immediately	offloaded (n	ot
27	16	LSD	counted in to	ns/hr rate)		
28	17	LSD	140	21	6	
29	18	LSD	221	21	10	
30	19	LSD	221	21	10	
31	50	LSD	221	21	10	
32	51	LSD	221	21	10	
33	54	LSD	221	21	10	
34	55	LSD	221	21	10	
35	20	LST	737	28	26	
36	21	LST	737	28	26	
37	22	LST	737	28	26	
38	23	LST	737	28	26	
39	24	LST	737	28	26	
40	25	LST	737	28	26	
41	26	LST	737	28	26	
42	27	LST	737	28	26	
43	28	LST	737	28	26	
	29	LST	737	28	26	
44				28	26	
44 45	56	LST	737	20	20	
	56 57	LST	834	28	30	
45						
45 46	57	LST	834	28	30	
45 46 47	57 58	LST LST	834 834	28 28	30 30	
45 46 47 48	57 58 59	LST LST LST	834 834 737	28 28 28	30 30 26	
45 46 47 48 49	57 58 59 60	LST LST LST LST	834 834 737 737	28 28 28 28	30 30 26 26	
45 46 47 48 49 50	57 58 59 60 61	LST LST LST LST LST	834 834 737 737 826	28 28 28 28 28	30 30 26 26 30	
45 46 47 48 49 50 51	57 58 59 60 61 3	LST LST LST LST LST LPH	834 834 737 737 826 903	28 28 28 28 28 28	30 30 26 26 30 18	
45 46 47 48 49 50 51 52	57 58 59 60 61 3	LST LST LST LST LST LPH LPH	834 834 737 737 826 903 810	28 28 28 28 28 28 49	30 30 26 26 30 18	
45 46 47 48 49 50 51 52 53	57 58 59 60 61 3 4	LST LST LST LST LST LST LPH LPH	834 834 737 737 826 903 810 836	28 28 28 28 28 28 49 49	30 30 26 26 30 18 17	
45 46 47 48 49 50 51 52 53 54	57 58 59 60 61 3 4 5	LST LST LST LST LST LST LPH LPH LPH	834 834 737 737 826 903 810 836 780	28 28 28 28 28 49 49	30 30 26 26 30 18 17 17	

Table VII-15

SHIP UNLOADING RATES AND TIMES: ADVANCED LANDING CRAFT (Run No. 3, 25-nmi Standoff)

Ship No.	Туре	Tons (short tons)	Rate (tons/hr)	Hours
30	LKA	3,006	82	37
31	LKA	3,031	82	37
32	LKA	3,006	82	37
34	LKA	1,455	82	18
48	LKA	1,653	82	20
49	LKA	1,094	82	14
33	LPA	644	82	7.85
47	LPA	1,722	82	21
2	LHA	3,156	84	37
2			84	37
2	LHA	3,156		
	LHA	3,156	84	37
2	LHA	3,156	84	37
7	LPD	1,250	67	19
8	LPD	1,299	67	19
9	LPD	1,112	67	17
10	LPD	1,176	67	18
11	LPD	1,031	67	15
12	LPD	1,225	67	18
41	LPD	935	67	14
42	LPD	1,203	67	18
43	LPD	1,072	67	16
44	LPD	1,251	67	19
46	LPD	1,202	67	18
13	LSD	-,		
14	LSD			
15	LSD			
1)				
16	LSD	Fach ton	/ - 1 10 THE	
16 17	LSD LSD		ied 12 LVTs w	
16 17 18	LSD LSD LSD	the LVTs were	immediately o	
16 17 18 19	LSD LSD LSD		immediately o	
16 17 18 19 50	LSD LSD LSD LSD	the LVTs were	immediately o	
16 17 18 19 50 51	LSD LSD LSD LSD LSD	the LVTs were	immediately o	
16 17 18 19 50 51	LSD LSD LSD LSD LSD LSD LSD	the LVTs were	immediately o	
16 17 18 19 50 51 54	LSD	the LVTs were counted in to	immediately ons/hr rate)	offloaded
16 17 18 19 50 51 54 55	LSD LSD LSD LSD LSD LSD LSD LSD LSD LSD	the LVTs were counted in to	immediately ons/hr rate)	offloaded
16 17 18 19 50 51 54 55 20 21	LSD	the LVTs were counted in to	immediately ons/hr rate)	offloaded
16 17 18 19 50 51 54 55	LSD LSD LSD LSD LSD LSD LSD LSD LSD LSD	the LVTs were counted in to	immediately ons/hr rate)	offloaded
16 17 18 19 50 51 54 55 20 21	LSD	the LVTs were counted in to	immediately ons/hr rate)  28 28	26 26
16 17 18 19 50 51 54 55 20 21	LSD	the LVTs were counted in to 783 783 783	immediately ons/hr rate)  28 28 28	26 26 26 26
16 17 18 19 50 51 54 55 20 21 22 23	LSD LSD LSD LSD LSD LSD LSD LSD LST LST LST LST	783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28	26 26 26 26 26 26
16 17 18 19 50 51 54 55 20 21 22 23 24 25	LSD LSD LSD LSD LSD LSD LSD LSD LST LST LST LST LST	783 783 783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28 28 28	26 26 26 26 26 26 26
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26	LSD LSD LSD LSD LSD LSD LSD LSD LST LST LST LST LST LST LST	783 783 783 783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27	LSD LSD LSD LSD LSD LSD LSD LSD LST LST LST LST LST LST LST LST LST	783 783 783 783 783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28	LSD LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26 26 26 26
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29	LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56	LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26 26 30
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57	LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	28 28 28 28 28 28 28 28 28 28 28 28 28 2	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58	LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	28 28 28 28 28 28 28 28 28 28 28 28 28 2	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59	LSD LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	28 28 28 28 28 28 28 28 28 28 28 28 28 2	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59 60	LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	1mmediately (28 28 28 28 28 28 28 28 28 28 28 28 28 2	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59 60 61	LSD LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	28 28 28 28 28 28 28 28 28 28 28 28 28 2	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59 60	LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	1mmediately (28 28 28 28 28 28 28 28 28 28 28 28 28 2	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59 60 61	LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59 60 61 3	LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	1mmediately ons/hr rate)  28 28 28 28 28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59 60 61 3 4 5	LSD LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	1mmediately ons/hr rate)  28 28 28 28 28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59 60 61 3 4 5 5 36	LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26 26 26 26 2
16 17 18 19 50 51 54 55 20 21 22 23 24 25 26 27 28 29 56 57 58 59 60 61 3 4 5	LSD LSD LSD LSD LSD LSD LSD LSD LSD LST	783 783 783 783 783 783 783 783 783 783	immediately ons/hr rate)  28 28 28 28 28 28 28 28 28 28 28 28 28	26 26 26 26 26 26 26 26 26 26 26 26 26 2

Table VII-16

UNLOADING RATES FOR CONVENTIONAL LANDING CRAFT
AT A 25-NMI STANDOFF DISTANCE

Ship Type	Rate (ton/hr)
LKA	50
LHA	39
LPD	29
LSD	28
LST	28
LPH	48

In reviewing Tables VII-14 and VII-15, the important fact obtained is that the longest time for unloading is 43 hours for the LHA and 37 hours for the LKA using advanced landing craft at 25-nmi standoff distance. The conventional landing craft run at a 5-nmi standoff distance indicates 34 hours for the longest unloading time. These times would convert to days, depending on the hours unloading crews could be worked and prevailing climatic conditions such as wind, surf, and sea state. If the hours worked were 18, all ships of the force would be unloaded by mid D+3, or 2.39 days. If more hours per day were worked, the days for unloading would be reduced. This information establishes the earliest time for beginning the unloading of AFOE support ships. This data also assumes that combat operations ashore gained control of sufficient terrain to organize the necessary beach and logistic support areas to facilitate cargo handling without undue congestion. As established in a previous paragraph, simulations conducted at SRI to support the landing craft studies of the beach cargo handling operations have verified that the unloading rates determined from the GAMUT simulation can be accommodated at the beach, given the required numbers of vehicles and materiel handling equipment.

VII-46

a previous paragraph, simulations conducted at SRI to support the landing craft studies of the beach cargo handling operations have verified that the unloading rates determined from the GAMUT simulation can be accommodated at the beach, given the required numbers of vehicles and materiel handling equipment.

The data in Tables VII-15 and VII-16 may be used by amphibious staff planners, along with the results from the CCF Model and the constrained unit T/E lists to determine the most operationally ready force for loading into the available amphibious lift capacity. In an actual operation, having decided to phase various units initially assigned to the AE into the objective area via the AFOE support ships, the commander may find them being landed before D+5, based on the finding of this analysis.

While the unexpected situations that occur in combat may create sufficient confusion in the objective area to negate some of the advantages derived from an application of the results of this study, use of the foregoing techniques nevertheless constitute a powerful aid to the staff planner by constructing the best advanced planning posture from available information.

#### E. The Effect on Amphibious Lift From Materiel Adjustments

In accordance with the first objective of the study, the impact of new material or planned items on the constrained amphibious lift problem will be presented in this section. The description of the research work done to determine material adjustments was presented in Section V.

Three areas of material adjustments were included.

## 1. New Family of Shelters

The effect on amphibious lift requirements from introducing the new family of shelters into the appropriate troop units of the MAF, as presented in Section V, was found to be a very small increase in bulk and square loaded space. The data from Table V-7 indicated that only .4 percent for bulk and .3 percent for square feet were required to incorporate these items of equipment.

# 2. Planned Items

Because of the few planned TAM items having embarkation data available, no significant effect on the constrained amphibious lift problem can be determined at this time.

## 3. Adjusted Mountout Calculations

The analysis of usage data conducted during this study, as presented in Section V, developed adjusting factors for a recomputation of mountout. With the application of these factors within the CCF Model, the mountout in bulk and square feet can be recomputed as though the original combat active replacement factors (CARF) contained in the TAM had been increased to reflect these adjusting factors.

The adjusting factor for the CARF values obtained from the 1968 TAM to be used in the CCF Model is 2.38 for both bulk and square. The constrained amphibious lift problem is then resolved for this new statement of mountout. Figure VII-6 contains the results from this run of the CCF Model.

The 2.38 value for the corrective factor applied within the CCF Model has very little effect on the loading problem. The increase in percent short fall obtained from multiplying 2.38 by the mountout for classes II and VII for each unit was .36 percent, which is insignificant.

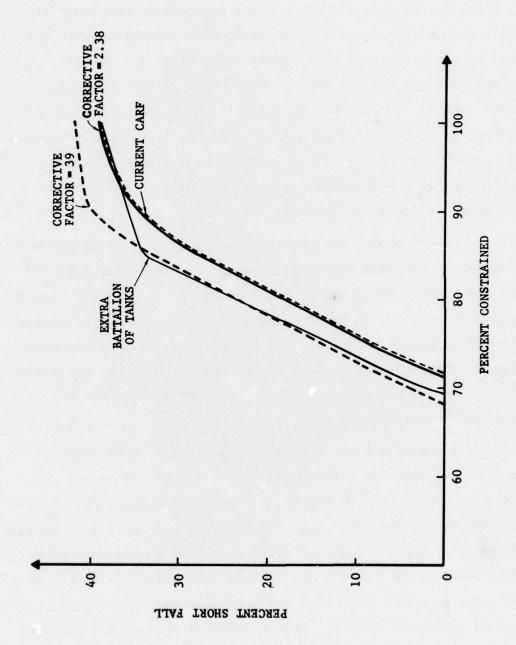


FIGURE VII-6. WEIGHTED CONSTRAINED UNIT LOADING VERSUS PERCENT SHORT FALL FOR ADJUSTED MOUNTOUT

When using the corrective factor of 39 obtained from Vietnam data for classes II and VII nonsquare, and 1.09 for square loaded items, the unconstrained percent short fall was increased to 42. This jump in total lift requires an applied constraint of 68 percent for unit loading, which may be cutting unit T/Es below acceptable levels. However, this representation of mountout may be closer to a realistic requirement than current amounts. For the assault echelon, supply classes IIW and VIIW mountout currently is .157 percent of total bulk cargo, and .839 percent for square loaded cargo, which is used for replenishment of T/E items in all units of the AE for 15 days. The remaining 45 DOS of mountout for the AE are carried by the AFOE.

No Middle East war loss rates were available for calculations in the study. The high losses of large square loaded items reported from that conflict would have a severe effect on the loading problem if any attempt were made to increase the mountout for these items carried by the AE in assault shipping. With the option of carrying any augmentation for square loaded mountout in AFOE support shipping, the phasing of these items ashore from the ships could start by late D+2, as demonstrated in Subsection E.

It is of interest to determine the effect on the loading problem of including an extra battalion of tanks as part of the mountout in the AE. When adding 66 E1850s and 4 E1860s to mountout, an increase of 20,476 square feet of mountout results. Figure VII-6 also illustrates this result. The run of the CCF Model generating the data for this curve used current mountout data, except for the addition of the 20,476 square feet. The curve for this run of the model requires a constraint of just under 70 percent for loading. This addition of mountout does not have a dramatic effect on the loading problem when considered alone.

It must be pointed out that the adjustment of the troop list for the AE would probably be required to compensate for this increase in mountout, which would permit the use of a higher constraint value for solving the loading problem.

Since the reduction of the CARF values in the TAM during 1972, very little mountout is required by allowances. Commander exceptions to the quantities carried in the TAM may have compensated for the extremely low allowances to some degree. It should also be noted that the CARF values in the TAM are the same for all units regardless of mission. It would appear appropriate to determine the CARF for individual units, and include this data element in the Equipment Allowance File (EAF), rather than the Item Data File (IDF), permitting the value assigned to reflect the unit's mission and expected usage rates.

# F. Amphibious Lift Requirements for the Deployed MAB and MAU

The most common force levels requiring embarkation planning are the MAU and MAB. Experience gained from mounting out a MAB for contingency deployments or training exercises consistently reveals the requirement to plan the loading of units into a shipping capacity considerably less than the initially desired lift requirements. A constrained amphibious lift problem exists with these force level organizations as well.

Many cold war operations have found amphibious forces committed to an area via the sea by first landing the forward deployed MAU, quickly reinforced by the parent MAB, and finally brought to MAF strength level at some later time.

This section will present lift requirements of the MAU and MAB obtained from troop lists provided to SRI as part of the MAGTF Project. These requirements will be compared with the assault shipping lift capacities defined for the MAU and MAB in the MMROP. The constrained

amphibious lift problem will be presented for the MAB case. Finally, the lift requirements of the residual MAF from first deploying the MAU/MAB to the objective area will be presented.

## 1. MAU Lift Requirements

Table VII-17 provides a notional troop list and the lift requirements for a MAU computed from the MAGTF System. The MMROP states that MAU lift requirements would require about 4-7 ships. The lift requirements in Table VII-17 would require about 5 ships, depending on the ship types selected.

### 2. The Constrained Amphibious Lift Problem of the Notional MAB

Since the MAU is part of the MAB, the lift problem facing the MAB will be considered as including the MAU, even though the MAU may be at a different geographic location initially.

The MAB troop list and lift requirements provided to the MAGTF Project is shown in Table VII-18. A total of 55,398 measurement tons and 582,442 square feet are required for this force. The DOS for mountout was set at 30 for the MAGTF run producing the results. Both the MAU and MAB troop units did not include the new CSS structure with a few exceptions. Some slight reduction in lift may have been possible if the entire troop list had been converted to the new structure. Most of the units contained in this force are detachments and therefore originally tailored to provide a wide range of support functions.

The MMROP states that a force of 16-21 assault ships would be required to lift a notional MAB. Because of the task organized structure of a specifically tailored MAB, this number of ships may be adequate. However, the lift requirements of the notional MAB presented in Table VII-18

Table VII-17
MARINE AMPHIBIOUS UNIT (MAU) TROOP LIST

	Unit	Unit Type Code	Quantity*	МТ	PAS	Square	Description
Command Element	м01000	CCVAA	1	55	75	1355	Hq, MAU Command Element
	M0101U	PGLAA	1	9	11	321	Det SCAMP for MAU
	M0102U	M0102	1	5	8	214	Det Force Recon for MAU
	M0110B	PUBEC	1	35	46	680	Det Radio Bn for MAU/MAB
Ground Combat Element	M1013	OGVAA	4	182	207	0	Inf Co, Inf Bn (Rein)
	M1037	9GUAA	1	570	402	4780	H&S Co, Inf Bn (Rein)
	M0200U	M0200	1	1	4	0	Det Hq Co, Inf Regt for MAU
	M1103	1HMAA	1	559	126	4842	105 How Btry (Rein) D/S Bn
	M0201U	9HLEB	1	9	22	177	Det Hq Btry, D/S Bn for MAU
	M0203U	4HXAA	1	21	43	263	Eng Plt (Rein), Eng Co, Eng Bn
	M0202U	4HVEC	1	1	8	0	Det Eng Spt Co, Eng Bn for MAU
	M0204U	PHSAA	1	11	24	214	Recon Plt (Rein), Recon Co
	M0205U	M0205	1	1	3	. 0	Det H&S Co, Recon Bn
	M0206U	FJQEB	1	11	9	280	Det Col Plt, C/C Med Bn
	M0207U	2SSAA	1	174	22	1847	Tank Plt (Rein), Tank Co
	M0208U	9SNEC	1	1	5	0	Det H&S Co, Tank Bn
	M0209U	2 TYAB	1	52	35	3297	LVT Plr (Rein), Amtrac Co
	M0210U	9 TWEB	1	1	7	0	Det H&S Co, Amtrac Bn
Logistic Support Unit	M0300U	M0300	1	340	13	10485	Hq. LSU
as a support	M0301U	9CXAA	1	1	3.	0	Det Div Hq, Hq Co, Hq Bn
	M0302U	M0302	1	1	7	0	Det Ser Co (Disb), Hq Bn
	M0303U	QDEC	1	1	7	0	Det MP Co, Hq Bn
	M0204U	PHSAA	1	1	2	0	Recon Plt, Recon Co
	M0305U	UJVAA	1	12	35	0	Trk Plt, Trk Co, MT Bn
	M0207U	2SSAA	1	1	8	0	Tank Plt, Tank Co
	M0307U	FJBEB	1	1	3	0	Det H&S Co. Med Bn
	M0308U	FTFEB	1	1	3	0	Det Dental Co
	M0309U	9JLAA	1	8	29	0	SP Plt, SP Co, SP Bn
	M0310U	9JJEC .	1	9	31	0	Det H&S Co, SP Bn
	M0311U	JJEEB	1	33	36	0	Det Sup Co, Ser Bn
	M0312U	HJFEB	1	3	12	0	Det Maint Co, Ser Bn
	M0313U	UJCEB	. 1	1	6	0	Det Trk Co, Ser Bn
	M0314U	HVRL1	1	1	9	0	Det Ord Maint Co, Maint Bn
	M0315U	HVRL2	1	1	4	0	Det MT Maint Co, Maint Bn
	M0316U	HVRL3	1	1	4	0	Det Elect Maint Co, Maint Bn
	M0317U	JVJE1	1	1	2	0	Det Ammo Co, Sup Bn
	M0318U	JVJE2	1	4	20	0	Det Bulk Fuel Co, Sup Bn
	M0319U	JVJE3	1	1	2	0	Det Sup Co, Sup Bn
	M0320U	JVJE4	1	1	4	0	Det H&S Co, Sup Bn
	M0321U	9VCEC	1	2	9	0	Det Comm Co, H&S Bn
Air Combat Element	M0600U	м0600	1	630	372	9404	Air Combat Element
Naval Beach Party	M0701U	M0701	1	872	142	40913	Naval Beach Party
Total				4171	2441	79072	

<sup>\*</sup>Amount shown is for one (1) unit; multiply by Quantity for total lift requirement.

Table VII-18

MARINE AMPHIBIOUS BRIGADE (MAB) 1ROOP LIST

	Unit	Unit Type Code	Quantity*	MT <sup>†</sup>	PAS	Barrels†	Square †	Description
Command Element	м0100в	CCFAA	1	173	225	6	3735	Hq, MAB Command Element
	M0101B	M0101	1	5	17	0	0	Det Div Hq, Hq Co, Hq Bn
	M0103B M0104B	PYFEB	1	7 12	12	1	688	CI Team /-/
	M0104B	PGKAA VYBEB	1	21	25 34	0	0 914	Det SCAMP
	M0106B	6UHEC	1	43	76	5	1916	Det Civil Affairs Group Det Comm Bn for MAB
	M0109B	M0109	1	2	- 4	0	0	Radar Becon Team, Comm Co
	M0110B	PUBEC	i	13	46	1	680	Det Radio Bn for MAU/MAB
Ground Combat Element	M1013	OGVAA	12	159	207	1	0	Rifle Co, Inf Bn
	M1037	9GUAA	3	546	402	9	4742	H&S Co, Inf Bn
	M1096	9GSAA	1	188	184	13	4658	Hq Co, Inf Regt
	M1103 M1126	1 HMAA 9HLAA	3	536 250	126 203	5	4804	105 How Btry, D/S Bn
	M1143	M1143	1	778	126	6	7151 6171	Hq Btry, D/S Bn
	M0201B	M0201	1	3	95	0	1455	155 How Btry, G/S Bn Det Hq Btry, G/S Bn
	м0202В	9неев	1	411	15	1	278	Det Hq Btry, Arty Regt
	м0203В	1SJGA	1	271	55	2	2128	8" How Plt, 8" How Btry
	M1373	4HWAA	1	102	135	2	799	Engr Co, Engr Bn
	M0204B	4HVEB	1 :	462	48	11	7113	Det Engr Spt Co, Engr Bn
	M0205B	M0205	1	12	13	0	163	Det H&S Co, Engr Bn
	м0206в	M0206	1	5	6	0	214	Det H&S Co, Recon Bn
	M1423	PHRAA	1	420	85	1	69	Recon Co, Recon Bn
	M0207	PTMAA	1	11	15	0	316	Det Force Recon Co
	M1653	UJUAA	1	63	79	9	8540	Truck Co, MT Bn
	M0208B	M0208	1	5	5	0	61	Det H&S Co, MT Bn
	M4233	2SRAA	1	1111	110	12	7035	Med Tank Co, Tank Bn
	M0209B M4652	9SNEB	1	15 236	12 229	. 0	346	Det H&S Co, Tank Bn
	M0210B	2TXAB 9TWEC	1	. 2	31	39	15846 1584	Amtrac Co, Amtrac Bn Det H&S Co, Amtrac Bn
Logistic Support Group	м0300в	9СКАА	1	9	37	1	414	Hq, LSG
	M0301B	M0301	1	10	32	2	817	Det Comm Bn for LSG
	M0302B	9GDEF	1	7	7	0	0	Det Serv Co (Disb), Hq Bn
	м0303в	M0303	1	5	4	0	0	Det Div Hq, Hq Co (Postal)
	M0304B	QGDEB	1	14	30	1	489	MP Plt, MP Co, Hq Bn
	M1523	FJQAA	1	96	98	4	2869	C/C Co, Med Bn
	M0305B	M0305	1	18	29	4	1532	Det H&S Co, Med Bn
	M0306B	M0306	1	11	19	0	0	Det Hosp Co
	M0307B	M0307	1	10 216	34	0	1122	Det Sup Surg Co
	M0308B M0309B	9JBEB	1	190	175	3 9	1132 6310	Det H&S Co, Serv Bn
	M0310B	HJFEB JJEEC	1	303	119	3	2700	Det Maint Co, Serv Bn Det Sup Co, Serv Bn
	M0311B	UJCEC	1	70	40	7	6145	Det Truck Co, Serv Bn
	M1863	9ЈКАА	1	61	66	1	575	Shore Party Co, SP Bn
	M0312B	9JJEB	1	433	78	8	6456	Det H&S Co, SP Bn
	M0313B	M0313	1	17	16	1	800	Det H&S Co, Maint Bn
	M0314B	M0314	1	48	68	2	2396	Det Ord Maint Co, Maint Bn
	M0315B	M0315	1	812	184	35	47690	Det Mt Maint Co, Maint Bn
	M0316B	M0316	1	347	40	30	13721	Det Elect Maint Co, Maint Bn
	M0317B	M0317	1	319	41	15	7910	Det Engr Maint Co, Maint Bn
	M0318B	M0318	1	7	24	0	0	Det Gen Sup Maint Co, Maint I
	M0319B	M0319	1	20	16	1	311	Det H&S Co, Sup Bn
	M0520B	M0320	1	72	112	1	297	Det Sup Co, Sup Bn
	M0321B	M0321	1	775	80	7	1154	Det Ration Co, Sup Bn
	M0322B M0323B	M0322	1	725	96	6	2085	Det Bulk Fuel Co, Sup Bn
	M0323B M0324B	M0323 M0324	1	110	78 91	1 4	495 2530	Det Ammo Co, Sup Bn
	M0324B M0325B	M0324 M0325	1	9	46	1	369	Det H&S Co, H&S Bn Det Comm Co, H&S Bn
	M0325B	M0326	1	326	66	3	3331	Det Spt Co, H&S Bn
	M0327B	M0327	1	203	88	16	26015	Det Truck Co, H&S Bn
	M4353	4SZAA	i	234	165	10	8927	Engr Co, Engr Bn
	M0328B	9SYEB	1	66	33	4	3221	Det Serv Co, Engr Bn
	M0329B	9SXEB	1	16	22	0	70	Det Hq Co, Engr Bn
	M4252	FTFAA	1	82	71	5	1800	Dental Co
	м0330В	9TQEB	1	12	6	0	153	Det H&S Co, MT Bn
	M4643	UTSAA	1	145	82	10	10250	Truck Co, MT Bn, Force Trps
	M0331B	UTREA	1	34	26	3	5752	Det Transport Co, MT Bn

Table VII-18 (Concluded)

	Unit	Unit Type Code	Quantity*	MT <sup>†</sup>	PAS	Barrels <sup>†</sup>	Square <sup>†</sup>	Description
Air Combat Element	M0601B	CLDEB	1	17	7	3	0	Det MWH for MAB
	M0602B	8LPEB	1	120	60	6	3408	Det MWHS for MAB
	M0603B	8MLEC	1	108	77	12	637	Det H&MS, MWSG
	M0604B	8MNEB	1	191	45	46	22223	Det WERS for MAB
	M8631	7LSAA	1	626	271	41	14900	MACS, MACG
	M0605B	7LREC	1	74	62	10	3088	Det MASS, MACG
	M0606B	8LPEC	1	11	20	6	0	Det H&HS, MACG
	M0607B	M0607	1	44	72	2	4368	Det MWCS, MACG
	M0608B	M0608	1	160	102	3	1555	Det FAAD Btry, MACG
	M0609B	M0609	1	592	165	119	8144	Det VMCJ (3 RF-4/3 EA-6A)
	M8813	8NJAA	1	448	484	32	6555	H&MS, MAG (VA/VF/VA (AW))
	M8820	8NKAA	1	4468	479	67	19701	MABS, MAG (VA/VF/VA (AW))
	M8821	7NLAA	2	83	73	6	2181	MATCU, MABS
	M8849	3NMAB	1	2115	320	239	6831	VMFA (12 F-4J)
	M8855	3NSAB	1	3863	227	124	7619	VMA (16 A-4M)
	M8857	3NUAA	1	3526	355	181	9343	VMA (AW) (12 A-6A)
	M8859	3NSAB	1	2896	372	224	6394	VMA (20 AV-8A)
	M8914	SPCAA	1	294	405	7	5522	H&MS, MAG (VH)
	M0610B	3PFEC	1	192	80	7	1636	Det VMO (4 OV-10)
	M8921	SPDAA	1	3145	390	33	17252	MABS, MAG (VH)
	м8937	3 PNAA	2	1277	248	48	3591	HMM (18 CH-46E)
	M8944	3PLAA	1	1411	345	92	4488	HMH (21 CH-53D)
	M8964	3PQUA	1	1185	278	33	14503	HML (21 UH-1N)
	M8970	3PUAB	1	1208	303	32	4473	HMA (18 AH-1J)
	M8621	3LYAA	1	333	120	7	6573	Missile Btry, LAAM Bn
	M0611B	8LXEB	1	2212	211	20	14584	Det H&S Btry, LAAM Bn
laval Support Forces	M0701B	M0701	1	2628	428	0	88184	Naval Beach Group
	M0702B	M0702	1	4894	763	0	53658	Naval Mobile Construction Bn

<sup>\*</sup>Amounts shown for one (1) unit; mulitply by Quantity for total lift sum.  $^{\dagger}$ MT = 55398 B1 = 1831 Sq = 582442 Computed totals have been adjusted for removal of obsolete TAMs.

were processed through CALAS, and an unconstrained lift short fall of 53 percent was obtained when using a 34-ship force, the approximate number of ships in one fleet. In order to analyze the size of the MAB and ascertain what units comprise the cargo, Table VII-19 was prepared. The aviation combat element constitutes 56 percent of the force due to the units providing support for the installation of a SATS site. The Naval Mobile Construction Battalion detachment for a MAB is also included to support construction of the SATS site.

When faced with planning the embarkation of a MAB, the staff planner would proceed to fit the MAB into whatever size ship force was made available, as previously described for the AE of the MAF. After developing the desired troop list based on the information available, he would process this force through MAGTF and analyze the amphibious lift status from the output of CCF Model. Table VII-20 shows the values for the lift short fall for the constraints used. It is obvious from these results that the lift requirement far exceeds the capacity of the 34-ship force, not to mention a short fall from a 21-ship force. A drastic reevaluation of the troop list is therefore necessary. The small effect of applying the constraints in Table VII-20 is due to the large number of detachments included in the list of units. In a case like this, the CFF Model user will probably code certain detachments for application of constraints as well, and allow CALAS to select the optimally constrained operational ready force, but not until he first reduces the troop list. In addition, other means for transporting the large combat aviation element of the MAB would be a possibility.

A run of the CFF Model was conducted by first eliminating the units contained in Table VII-21. The units selected consist of those whose functions may either not be needed immediately, arrive by other transportation means, or be performed in some other way. In any case,

Table VII-19

MAB UNIT CARGO CATEGORIES

Element/Force	<u>MT</u>	Percent of Total	<u>Square</u>	Percent of Total
Command element	276	0.48%	7,933	1.30%
Ground combat element	9,499	16.83	92,565	15.21
Logistics support group	7,189	12.74	170,842	28.07
Air combat element	31,959	56.62	195,341	32.10
Naval support forces	7,522	13.33	141,842	23.31

Table VII-20

WEIGHTED CONSTRAINED UNIT LOADING VS PERCENT SHORT FALL FOR A NOTIONAL MAB TO BE LOADED IN A 34-SHIP FORCE

# Percent

Short Fall	Constraint
53	100
52	90
51	85 .
50	75
49	70
48	65

<sup>\*</sup>Constraints are weighted according to a unit's mission, as explained in Section VI.

Table VII-21
UNITS SELECTED FOR REDUCED MAB TROOP LIST

Unit	MT	Sq
M0321B	775	1,154
м0323в	110	495
M0324B	1346	2,530
м0316в	347	13,721
м0315в	876	47,690
M8820	4468	19,201
M8821	166	4,362
м8914	294	5,522
M8921	3145	17,252
M8621	333	6,573
M0702B	4894	53,658

the logistics planner will make his selection from the best information available. Figure VII-7 presents the results of constrained loading using the reduced MAB troop list. The relatively flat slope of the curve is due to applying constraints to essentially a small number of units. The planner could increase the number of units, i.e., detachments, and spread the T/E reductions through more units, or he could make greater reductions in the troop list.

## 3. Follow-on Deployment of the MAF

The residual units of the MAF requiring lift to proceed to the objective area of the deployed MAB would depend for the most part on turnaround assault shipping, airlift, or common user sealift. A notional residual force was constructed by the project team. Totals for this force are listed in Table VII-22. The troop list and unit lift requirements for the AE are listed in Table VII-23. These values are based on computing mountout for 15 DOS.

## 4. The MAB Embarked in SMLS Configured Assault Shipping

The possibility exists that the MAU and MAB may deploy configured for Seaborne Mobile Logistic Support (SMLS). The loading problem when considering ships prepared for SMLS support becomes more constrained due to the loss of cargo space for landing force materiel. The Marine Corps study of SMLS indicates that six ships would be configured for SMLS support functions. Estimates of loading these ships reveal that broken stowage factors would be reduced from 0.8 to 0.5. A MAB configured for SMLS support would have an altered troop list that eliminated certain units and functions from deploying ashore. The troop list in Table VII-21 containing units to be deleted from the MAB include maintenance detachments. The results from the altered MAB troop list run of the CCF Model could be reduced even further if justified by the expected situation facing the SMLS configured MAB.

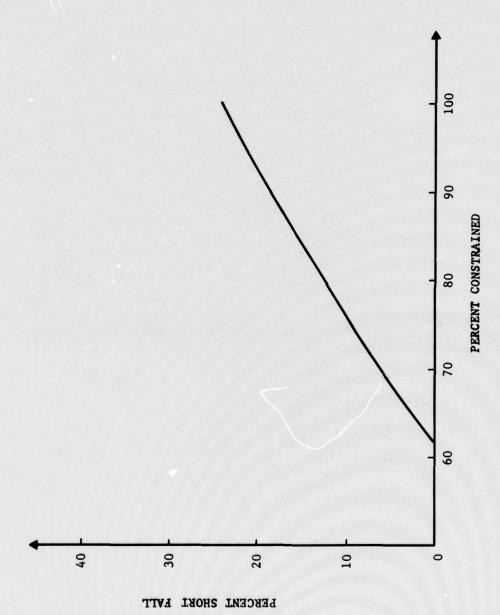


FIGURE VII-7. WEIGHTED CONSTRAINED UNIT LOADING VERSUS PERCENT SHORT FALL FOR THE MAB REDUCED TROOP LIST WITH 34 SHIP FORCE

Table VII-22

LIFT REQUIREMENTS FOR THE RESIDUAL MAF

AFOE

$$\frac{\text{MT}^*}{306,036}$$

<sup>\*</sup>This figure includes the cube of square loaded items when loading in common user sealift.

Table VII-23 FOLLOW-ON RESIDUAL ASSAULT ECHELON OF MAF

Unit	Quantity*	MT <sup>†</sup>	PAS	Barrels <sup>†</sup>	Square <sup>†</sup>
M4623M	1	1805	161	824	500
M1096	2	188	184	491	6344
M1038	6	1018	1230	453	4748
M1128	2	1733	707	1170	28184
M4233	2	914	110	453	6583
M1423	3	449	85	19	131
M1373X	3	72	121	75	1105
M4652	3	111	229	1491	15414
M1864X	1	389	244	755	12732
MO-01F	1	6482	914	66	2701
M1.196	1	981	278	1208	17502
M1363X	1	2747	202	1830	31463
M4237	1	867	313	774	16966
M4903	3	35	120	38	610
M4907	1	96	182	358	6346
M3857X	1	457	287	1245	11044
M3853X	3	59	103	113	1916
M1427	1	116	130	283	6522
M8625X	. 1	209	278	208	3669
M1988	1	740	1040	925	17591
M1377X	1	130	131	94	794
M1867X	1	263	173	340	6614
M4654	1	227	253	943	11628
CMD-GP	1	1688	1566	3931	85570
M8612X	1	399	388	1283	16658
M8631X	1	1068	244	2302	13867
M8640X	1	337	197	943	7998
M8615X	1	198	158	302	2893
M8937X	1	1217	241	1811	3189
M8943X	2	1291	298	3057	3927
M8964X	1	1109	269	1245	2789
M8968X	1	1333	217	1472	3879
M8859X	1	2001	363	8642	5464
M3447F	1	113	337	358	5832
M3343F	1	10	136	19	427
M3313F	1	2954	140	0	22677
M3323F	1	8	47	19	458
M3442F	1	1111	202	472	11201
M1985X M0601F	1	89 35	143 212	415	12616
	The second second			0	0
M0604F	1	668	257	906	11024
M4112	1	673	225	736	14584
M4193	2	425	177	528	10581
M4201 M4226	1	67 678	120 177	170 528	2035 8730
M3223X	1	621	280	491	
M3223X M3233F	1	43	125		11365
M3247F	i	127	55	57 38	1455 1975
		The state of the s		The second secon	
M3243X M3253X	1	1043 234	191 190	189 75	7188 2763
M0305F	1	212	120	736	11914
M0303F M0307F	1	24	82	38	
M3751X	1	2224	315	755	571 7909
M3751X	1	1034	· · · · · · · · · · · · · · · · · · ·		
M3753X M8914X	2	183	144 359	434 189	8955 4839
M8921	1	3245	390	1283	17374
M8821	2	87	73	208	2198

 $<sup>^{*}</sup>$ Amounts Listed are for one (1) unit; multiply by Quantity for total lift requirement.

MT = 58000 B1 = 59621 Sq = 660760
Computed totals have been adjusted to remove obsolete TAMs.

## G. Assault Follow-on Echelon Lift Requirements

AFOE troop list and lift requirements are listed in Table VII-24. This list shows the cargo configured for loading in common user sealift. The mountout is computed for 60 DOS and includes 45 DOS for the AE. An increased lift requirement for material eliminated from the AE for constrained loading is included. The study was not vitally concerned with the AFOE lift requirements beyond establishing if a shipping constraint would exist for this material as well.

### 1. Commerical Ship Assets

Research was conducted into common user sealift assets that may be available to lift a notional AFOE force. Information obtained<sup>3</sup> indicated that over 60 commercial ships, on the average, are less than six days from the ports of embarkation usually used by Marine Corps units. While time must be allowed for ship unloading before they are available for loading AFOE units, sufficient time appears to exist for meeting a 30-day warning period to sailing date. Since the availability of these ships depends on decisions made at the highest national level, no speculation on ship availability is presented here. Table VII-25 presents a list of ship capacities obtained from data supporting the study in Reference 3 to illustrate ship capacities with respect to AFOE lift requirements. Approximately 24 ships from this list are needed to lift the AFOE.

## 2. Common User Sea Lift Notional Ship Planning Data

Planning data obtained from NAVMAT P4000-2 provides the notional lift characteristics for common user sealift assets. Table VII-26 gives an analysis of the notional AFOE lift requirements with respect to common user sealift characteristics. The data for passenger ships includes

Table VII-24 CSS AFOE LIFT REQUIREMENTS

	*				
Unit	Quantity	MT+	Pas	Barrels	Unit Descriptor
M4722	1	154	16	2	CI Team
M4392	1	561	53	8	TOPO Plt
M0602F	1	30	66	0	Det Hq, MAW
M8620X	1	5456	325	79	H&S Btry, LAAM Bn
M8621X	3	722	115	27	Missile Btry, LAAM Bn
M8710X	1	3967	515	95	H&MS, MWSG
M8715X	1	50303	503	139	Trans Sqdn
M8714X	1	41585	377	116	Engr Sqdn
M3755N	1	21281	253	103	Engr Spt Co, Engr Spt Bn
M3751X	1	3550	315	41	Bulk Fuel Co, Engr Spt Bn
M3752X	1	7258	139	12	Bridge Co, Engr Spt Bn
M3851X	3	517	71	9	Dental Co
M4903	1	194	120	3	MP Co, MP Bn
M4643N	1	24526	264	67	Trk Plt, Trk Co
M4644X	1	31014	238	57	Trans Co, MT Bn, FSSG
M4647X	1	3302	156	26	H&S Co, MT Bn, FSSG
M3853X	1	331	103	6	Med Co, Med Bn, FSSG
M3854X	1	253	239	7	Hosp Co, Med Bn, FSSG
M3753X	1	5629	144	24	Engr Co, Engr Spt Bn
M3233N	1	3478	158	12	Det MT Maint Co
M3247N	1	5839	152	63	H&S Co /-/ Maint Bn
M3313N	1	527	405	10	Supply Co /-/ Supply Bn
M3323N	1	1349	142	5	Ration Co /-/ Supply Bn
M3343N	1	1661	268	10	Ammo Co /-/ Supply Bn
M3347X	1	2113	379	33	H&S Co, Supply Bn
M3443X	1	1311	375	17	Comm Co, H&S Bn, FSSG
M3447N	1	3498	521	66	H&S Co, Supply Bn
M3442N	1	3861	388	38	B&P Co, H&S Bn
M3444N	1	448	179	6	MP Co, H&S Bn, FSSG
M3445N	1	392	268	4	Svc Co, H&S Bn, FSSG
M0702	1	388	763	0	Mobile Const Bn
M0603F	1	13	4	0	Det Hq, MAW
M8712	1	224	4	2	MWWU
M8652	1	2833	122	625	VMCJ (7 RF-4/17 EA-6)
M8780X	1	2184	419	634	VMGR (12 KC-130)
M8813X	3	1515	449	13	H-MS MAG (VA/VF)
M8855	2	7598	227	265	VMA (20 A-4)
M8857X	2	6632	347	382	VMA (AW) (12 A-6A)
M8848X	4	3634	377	650	VMFA (15 F-4J)
M0605F	1	643	77	5	Det MWHS

<sup>\*</sup>Amount shown is for one (1) unit; multiply by Qty for total lift requirement)

<sup>†</sup>MT = 281,414 Barrels = 6,356
VII-65

Table VII-25

COMMERCIAL SHIPS AVAILABILITY AND CAPACITY

	Ship No.*	Days	Speed	мт
1	6646	1	16.0	18,400
2	8703	2	20.0	16,284
3	10703	2	20.0	19,233
4	30603	2	20.8	27,055
5	30044	1	23.0	20,441
6	29781	2	21.0	27,050
7	9743	2	20.0	16,275
8	29734	2	23.0	20,441
9	6949	2	20.0	15,850
10	22543	2	20.0	14,586
11	15492	1	16.0	20,268
12	6682	1	17.0	18,792
13	6686	2	17.0	28,631
14	11690	2	16.0	18,639
15	11098	1	17.0	31,789
16	60335	2	23.0	25,672
17	32600	2	21.5	34,100
18	31227	1	23.0	44,690
19	37720	2	23.0	25,672
20	62809	2	23.0	44,609
21	63822	2	23.0	35,000
22	63823	1	23.0	35,000
23	30170	2	23.3	38,473
24	11109	2	17.0	19,000
25	21814	2	20.0	13,643
26	28595	2	20.0	23,670
27	13176	2	16.5	19,825
28	11681	2	16.5	19,825
29	6670	3	16.0	18,400
30	6671	3	16.0	18,400
31	5637	3	15.5	24,847
32	11114	3	17.0	18,792
33	37792	3	32.8	58,375
34	27617	3	22.0	32,395
35	33964	3	22.5	41,415
36	22392	4	20.0	18,443
37	21451	4	20.0	19,425
38	25928	4	21.0	18,300
50	23720		21.0	10,500

Table VII-25 (Concluded)

	Ship No.	Days	Speed	MT
39	11107	4	17.0	15 107
40				15,107
	60474	4	33.0	58,375
41	22235	4	20.0	16,072
42	60472	5	33.0	58,375
43	30008	5	22.0	33,275
44	13589	5	20.0	27,591
45	29197	5	22.0	33,275
46	31820	5	23.0	44,690
47	28726	5	23.0	29,315
48	62810	5	23.0	44,609
49	62808	5	23.0	44,609
50	61691	5	22.0	43,388
51	36051	5	22.5	41,415
52	35880	5	22.5	41,415
53	37282	5	22.5	41,415
54	11676	5	16.5	19,825
55	27454	6	20.0	18,747
56	25039	6	20.0	18,747
57	11668	6	16.0	17,330
58	11119	6	17.0	31,789
59	60602	6	20.0	
60	38082			16,072
60	36062	6	33.0	58,375

<sup>\*</sup>Source: Project SEA EXPRESS<sup>5</sup>.

 $<sup>^{\</sup>dagger}$ Sailing days from U.S. (USMC access) ports.

# Table VII-26

# AFOE LIFT REQUIREMENTS

Passengers = 13,011
Measurement Tons, Cargo = 306,036
Barrels of Bulk Fuel = 635,600

# Notional Ships Required

Passenger Ships = 9 Cargo Ships = 40 Tankers = 3 2000 MTs of cargo, in addition to the troop lift capacities. On the basis of this planning data, a group of 52 ships would be required to lift the AFOE.

In general, the fly-in echelon of the AFOE would require sealift for only half of the computed cargo for those units of the fly in echelon in Table VII-24. Cargo reductions for the airlift portion of these units could be accomplished if a detailed loading analysis was desired.

#### 3. Containerization

The problems of loading AFOE cargo into containers for lift by container ships will become a problem in the 1980s. Containers were not considered in this study due to the emphasis placed on the assault echelon by the study objectives. It is of interest to note that the MAGTF System is capable of determining cargo suitable for containerization when the need should arise.

#### I. Summary

The materiel presented in this section has demonstrated the use of CALAS to solve the constrained amphibious loading problem using a systematic computerized mathematical methodology. The solution procedure included the exercising of various options available to the user of the system. These options include the use of system features that reduce the AE either by (1) horizontal cuts, i.e., reducing the unit's T/E by a series of constraint values or by reducing the DOS for mountout; by (2) vertical cuts, i.e., reducing the troop units of the force from those to be loaded into assault shipping; or (3) by a combination of both options. The effect of varying input from the possible need to increase the statement of mountout to be carried by the AE of the MAF on the constrained amphibious lift problem was also presented.

The effect of combining these options on the constrained lift problem is demonstrated in Figure VII-8, where the following options were exercised:

- (1) Modified troop list
- (2) Increased mountout from Vietnam data and an extra battalion of tanks
- (3) Weighted application of constraints to unit T/Es.

The CCF model run using these options provides data indicating that a 78 percent T/E reduction in combination with the first two options was necessary to load the available ships. If these ships quantities are reduced due to breakdown or enemy action, a greater loading problem will exist.

The feasibility of vertical cuts of the AE, which are really units designated for phased entry into the objective area from the AFOE support ships, were shown to be dependent on the unloading times necessary for the assault shipping. Simulation results showed that only a 2- to 3-day delay may be required before phased units are landed and deployed ashore.

The application of CALAS to the constrained loading problem of the MAB was also provided. The magnitude of the constraints necessary to load the MAB was shown to be dependent on the size of the force structure selected for the MAB. The supplies and equipment to accompany the notional troop list for the MAB obtained from the MAGTF Lift Model resulted in lift requirements too large for a 34 ship force.

The lift problem for the AFOE was shown to exist without the need to apply CALAS. Sufficient ships from the common user sealift pool exist to lift this force. The need for timely arrival at the objective area to begin unloading when crews and landing craft are available cannot be over emphasized. This facilitates the rapid phasing ashore of originally designated AE units.

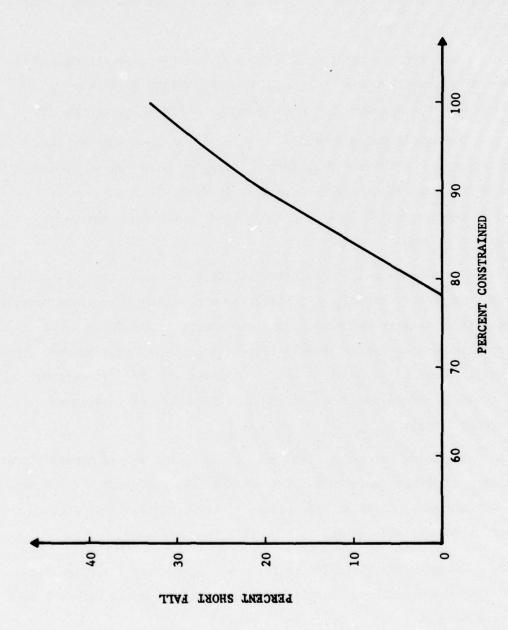


FIGURE VII-8, WEIGHTED CONSTRAINED UNIT LOADING VERSUS PERCENT SHORT FALL FOR MODIFIED TROOP LIST AND MOUNTOUT INCREASE FROM VIETNAM DATA AND EXTRA TANKS

## J. Conclusions

The analysis conducted in this section has provided support for the conclusions presented herewith. The subsections from which these conclusions derive are indicated.

- 1. The lift requirements for the notional MAF AE are larger than can be satisfactorily reduced by applying constraints to full units in order to fit into assault shipping capacity. (Subsection B, page 28.)
- 2. The use of CALAS installed within an automated command and control system provides the computational support necessary to systematically determine the optimal operationally ready force in a short period of time during the planning phase of an amphibious operation. (Subsection B, page 2.)
- 3. The Constrained T/E Embarkation Analysis Model using the criticality factors denoting all items importance to a unit's function provides a practical systematic methodology for reducing a unit't T/E when its lift requirements must be constrained by limited assault shipping assets. This analytical procedure may also be used to compute lift requirements for airlift when a percentage reduction of unit T/E materiel is desired. (Subsection B, page 7.)
- 4. An assessment of the time phased deployment ashore possibilities for combat and combat service support units within the MAGTF Mission provides the greatest potential for optimizing the utilization of limited amphibious assault ship assets. (Subsection C, page 29.)
- 5. Based on GAMUT simulation results, the potential for landing the AE from the amphibious assault force used in this study within 3 days is a real possibility. (Subsection D, page 46.)
- 6. Units may begin unloading from AFOE support ships from D+2 on. (Subsection D, page 46.)

- 7. The unloading rates simulated by GAMUT can be supported by unit's handling cargo transfer operations at the beach. (Subsection D, page 47.)
- 8. The statement of mountout for supply classes IIW and VIIW computed from current combat active replacement factors (CARF) may be inadequate to support future expected combat losses. (Subsection E, page 51.)
- 9. The practice of using the same value for CARF for mountout calculations regardless of the different missions of units in the force results in an inadequate statement of mountout or prepositioned war reserve material. (Subsection E, page 51.)
- 10. Significant amphibious lift short falls will exist when attempting to load a MAB whose troop list is the size of the notional MAB into a 34-ship force, and, to a greater extent, a 21-ship force. (Subsection F, page 51.)
- 11. Sufficient ships are available to lift the AFOE of the MAF from common user sealift assets. (Subsection G, page 69.)

## REFERENCES

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- 4. "Seaborne Mobile Logistic System (SMLS): Volume I Executive Summary"; "Volume II Amphibious Task Unit/Marine Amphibious Unit (ATU/MAU) Analysis"; "Volume III Amphibious Task Group/Marine Amphibious Brigade (ATG/MAB) Analysis"; Marine Corps Development and Education Command (1 June 1974).
- 5. "Project SEA EXPRESS Navy Accelerated Sealift Study: Part I U.S. Rapid Reinforcement Capability"; Part II The Impact of Attrition"; Office of the Chief of Naval Operations (25 July 1974).

### VIII A WEIGHT AND CUBE CONTROL PROGRAM

## A. Requirements

The third objective of the research study reported on herein is to determine the actions necessary to establish a viable weight and cube control program for landing force materiel. The purpose of this program is to ensure that lift requirement considerations be given major attention during the materiel acquisition process.

## B. Background

For many years materiel acquisition programs have been the subject of continuing analysis, review, and evaluation. The addition of complex and expensive systems and materiel has continued to increase significantly, to a point where major improvements in the Marine Corps' Materiel acquisition process are essential if operational readiness is to be maintained within the constraints of projected scarce resource levels.

A reduction in the number of naval ships dedicated to amphibious operations has seriously constrained the amount of amphibious lift of the assault echelon (AE) of the MAF. Therefore, it is important that, early in the acquisition process, individual systems or items of materiel be subjected to a logistic supportability evaluation. Such evaluations should be based not only on the direct effects the addition, removal, or replacement of new items of materiel have on the total weight, square, and cube of landing force materiel, but also on the secondary effects of fuel consumption, repair parts, and personnel requirements.

## C. Areas of Emphasis

The Marine Corps' acquisition process emphasizes the need for simulating, modeling, and prototyping the proposed items of materiel to demonstrate their overall effect on the Fleet Marine Force. Early application of integrated logistic support principles is stressed in the acquisition procedure.

## D. Major Materiel Acquisition Phases

Normally, an item of materiel slated for introduction into the Marine Corps progresses through the four following phases after the decision to consider the item for acquisition has been initiated:

- (1) Conceptual phase
- (2) Full scale engineering development phase
- (3) Production/procurement phase
- (4) Development and support phase.

Insofar as new equipment development is concerned, the most important phase for weight and cube considerations is the conceptual phase. Here exploratory and advanced development constitute the main areas of investigation. At this stage of development, the new item will be sufficiently defined to establish weight, dimensional data, and operating characteristics, such that estimates of fuel requirements and repair part usage may be established.

The CG MCDEC is the principal agent for the CMC in executing the "conceptual phase." He is responsible for advising the CMC of the results derived from this phase and for recommending the systems and items of material that have potential application to the Marine Corps' operational needs.

It logically follows that the CG, MCDEC would be a primary user of a weight and cube control program.

## E. MAGTFs Role in the Materiel Acquisition Process

Program MAGTF is ideally designed to play a major role in the "conceptual phase" of the materiel acquisition process. Already included in the data base is the majority of the information needed to determine the effects of new materiel acquisitions upon lift requirements. The MAGTF data base contains the T/Os and T/Es for all standard and nonstandard Marine Corps units. As explained in section V, the data base contains physical characteristics of each T/E item. Therefore, it becomes a relatively simple procedure to structure notional MAFs, MABs, and MAUs to conform to MMROP and MLRP troop lists and to determine the overall effect on the amphibious lift requirements of the MAGTF of interest. Equally simple is the addition, deletion, or replacement of items within a unit's T/E and the alteration of their physical characteristics within the MAGTF data base for restructuring the unit.

A notional organization such as a MAB or MAU can be processed through the MAGTF system first with its existing T/E, and then with the same T/E altered to reflect the addition, deletion, or replacement of items. The impact of these alterations upon the overall cube, square, and weight of the organization can be made by comparing the two runs. In addition, the secondary effects, such as fuel consumption, repair part consumption, replacement quantities, and personnel changes, can be examined from the output listings of Program MAGTF.

The following discussion is a step-by-step description of how the MAGTF System was utilized to provide a comparative analysis and evaluation of replacing existing shelters and shelter transport in a notional MAF with a new family of shelters, along with the transport utilized to convey the new shelters. The principal findings from this analysis will be the overall effect the shelter replacement has on the total cube, square, and weight of the MAF.

This analysis is presented to show the role that Program MAGTF can play in both the "conceptual phase" of the materiel acquisition process and in a weight, square, and cube control program. Section V has already covered the results of this effort.

## 1. Updating MAGTF SYSTEM and EQUIP Files

Before Program MAGTF could be utilized for the comparative analysis, it was necessary to obtain the physical characteristics of the new shelters, the new logistic trailers, and the new 6-ton truck tractor.

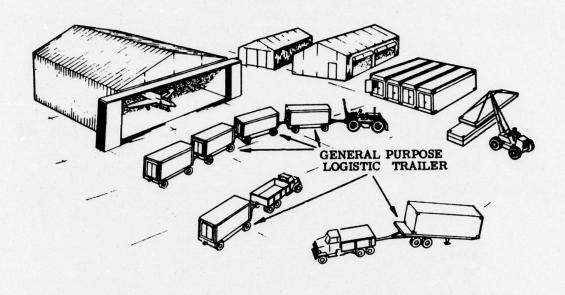
Once these physical characteristics were obtained, VALU cards were prepared, containing this dimensional data, then the MAGTF EQUIP file was updated. The next step was to update the SYSTEM File with the new equipment. In the cases of the new shelters, the individual systems to be added consisted of only each individual new shelter. However, in the case of the new truck tractor, the new system to be added included not only the truck tractor but also fuel, lube, and grease consumption rates, as well as class IX usage rates.

After updating the SYSTEM and EQUIP Files, Program CREATE was run to place this new data on the randomly accessible files to be read by Program MAGTF.

Figure VIII-1 is an illustration of the new family of proposed Marine Corps shelters, logistic trailers, and truck tractors.

## 2. Shelter Replacement Allowances

A table of shelter replacement allowances showing for each existing shelter the type and quantity of the replacement shelter(s) was constructed. Table VIII-1 is an extraction from that table. When replacing existing hard shelters it was sometimes necessary to replace one existing shelter with two or more replacement shelters to ensure equivalent square foot work space availability.



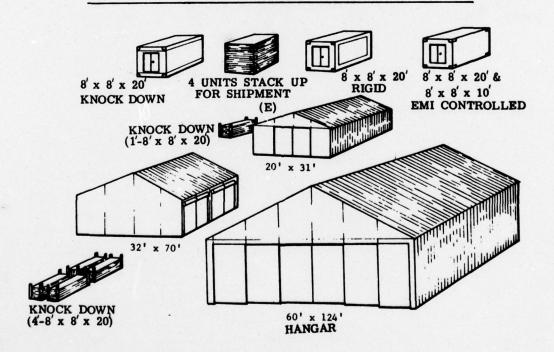


FIGURE VIII-I. PROPOSED FAMILY OF SHELTERS AND TRANSPORT

Table VIII-1

SAMPLE OF EXISTING HARD
SHELTER/NEW SHELTER REPLACEMENT ALLOWANCES

T/E	Existing Shelter	Existing	R	eplacemen	nt Allowance	
No.	TAM No.	T/E Allowance	Knockdown	Rigid	20' EMI*	10' EMI*
M1126	E1036	1		2		
M1743	A2320	4				4
	A2340	2				2
	A2350	2				2
	B1960	1		1		
	B2595	1	1	2		
	D0270	4		8		
M4392	B1312	2	4	6		
M3253	A0175	2				4
	A2696	1			1	
	E1038	1		1		

 $<sup>^{*}</sup>$ EMI=electromagnetic isolation

Table VIII-1 is an example of how the replacements are made for existing shelters. For example, unit M1126 has a T/E quantity of one E1036, a meteorological station, that is to be replaced by two of the new rigid shelters.

## 3. Transport Replacement Allowances

In determining the new logistic trailer replacement allowances, the rule of one trailer per five shelters was followed. The ratio of one truck-tractor per one and one-half logistic trailers was followed in determining the quantity of new 6-ton truck-tractors that would be needed to convey the new shelters.

A table (not shown) similar to Table VIII-1 was constructed, showing the transport replacement allowances for each T/E transport item affected by the addition of the new shelters.

## 4. <u>Unit-by-Unit Replacement of Existing Shelters with New</u> Family of Shelters

A unit-by-unit, shelter-by-shelter worksheet was prepared to tally the replacement of existing shelters with the new shelter replacements. The worksheet was divided into two sections: one for the assault echelon and one for the assault follow-on echelon. Totals for each type of shelter to be removed, as well as totals for each type of replacement shelter, were obtained. Table VIII-2 shows a portion of the worksheet.

## 5. <u>Unit-by-Unit Replacement of Existing Transport with</u> New Transport

Included in Table VIII-2 are quantities of the TAM items of transport to be deleted from a unit's T/E, along with the replacement quantities of trailers and 6-ton truck-tractors.

VIII-8

Table VIII-2

SAMPLE.
UNIT-BY-UNIT REPLACEMENT ALLOWANCES FOR EXISTING HARD SHELTERS AND TRANSPORT WITH
NEW SHELTERS AND TRANSPORT

	E1670																												
	E1660				2			2						7															
	D0310 D0320			-	2							1		7					3				1				3	7	11
s	D0310			1	2							1		7				,	3				1				3	1	11
llowance	C6440																									2		2	2
Existing Allowances	C6410																												
Ex	B2595				2									,	7								1					1	3
	B1960				1									,	7										1			-	3
	B1950														,														1
	B1460																												
-	20. EM1								-	1			3	ď	,					6	2							=	16
.es	10. EM1		65		80	7	-		22	1	2		36	169	601				2	11	2	2			2			24	193
Replacement Allowances	RIGID		7		25			18	3			3		04	60		,	0	12			14	10			2	12	80	149
acement	KNOCK- DOWN													4	0		,	t	3	2		8	2				1	20	26
Repl	TRK- TRAC		7	-	7			2	2	-	-		9	38	07				2	3		2	1	1			3	17	42
	LOC		80	-	9			7	4	1	-		10	6.7	74				7	2		7	2	-			5	56	89
		ur.																											
		Assault Echelon	CMD-ELEM	M8921	M1743	M0303F	M1867	M3223	M3253	M8621	M8821	M8615	M8631	TOTAL AE	TOTAL AE	Toda	7000	M4 392	M8820	M8620	M8621	M8710	M8715	M8821	M0306F	M3213	M0313F	TOTAL AFOE	TOTAL MAF

## 6. MAGTF Input

Two approaches were possible in using Program MAGTF for the shelter analysis. The first approach was to run the assault echelon and then the assault follow-on echelon of the MAF with the existing shelters, and then rerun each echelon with the existing shelters and transport deleted and the new shelters and transport included. The big disadvantage to this approach was the long running time and the larger expense of running a full MAF-sized problem through MAGTF.

The second approach was to prepare separate runs; the first for the additions to, and the second for the deletions from each of the echelons of the MAF, and then perform a simple subtraction to obtain the net effect the introduction of the new set of shelters would have on the square, cube, and weight of the assault echelon and the assault follow-on echelon of the MAF.

Table VIII-3 is a partial listing of the MAGTF input data deck for each of the four MAGTF runs that were necessary to perform this analysis.

## 7. MAGTF Output

Tables VIII-4, 5, 6, and 7 contain examples of the output of Program MAGTF. Although the results of all four runs were used for the analysis, only a small portion of the output from one run is shown.

The reader can see that the total class VII square computed using the existing shelters and transport shown at the bottom of Table VIII-4 is 32,097 square feet. Comparing this number with the result of the run (not shown) using the new replacement shelters and transport, an increase is found of about 8,500 square feet obtained by introducing the new shelter system into the assault echelon.

## Table VIII-3

## MAGTF INPUT DATA CARDS FOR EXISTING/REPLACEMENT SHELTER ANALYSIS

	Run 1		
BASIC UNIT NAME SYSTEMS SYSTEMS SYSTEMS	-	SHELTER-AE 1 A0010 2 A0060 2 A0175	
SYSTEMS ASSAULT ECHELON UNIT	=	3 E1730 SHELTER-AE	
3101	Run 2		Existing Shelter and Transport Deletions
BASIC UNIT NAME	-	SHELTER-AFOE	
SYSTEMS	-	5 A0270	
SYSTEMS .	=	1 A1110	
SYSTEMS	=	1 E1790	
ASSAULT ECHELON UNIT	•	SHELTER-AFOE	
	Run 3		
BASIC UNIT NAME	-	NEW-AE-SHELTERS	
SYSTEMS	-	45 NEWLOGTRLRS	
SYSTEMS .	-	83 NEW SHLTR-RIG	New AE Shelter and Transport Additions
ASSAULT ECHELON UNIT	=	NEW-AE-SHELTERS	

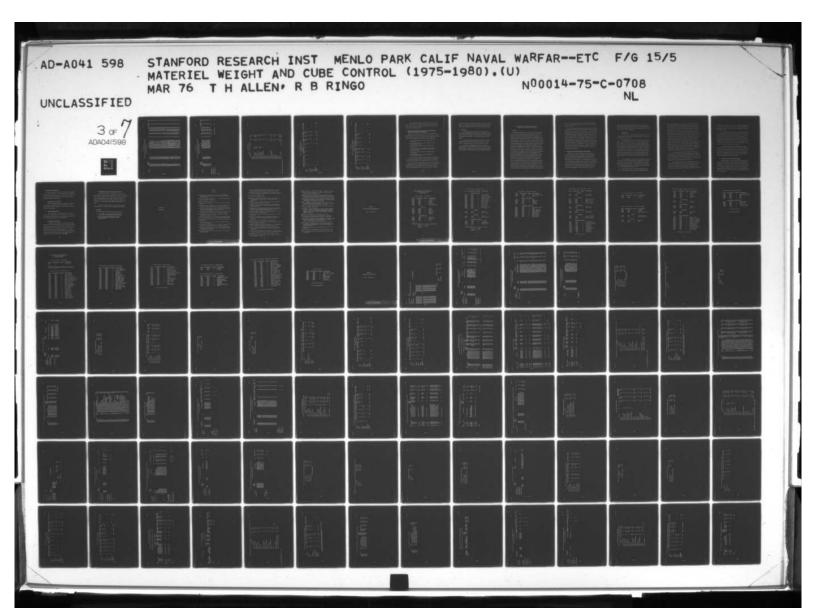
STOP

## Table VII-3 (Concluded)

## MAGTF INPUT DATA CARDS FOR EXISTING/REPLACEMENT SHELTER ANALYSIS

## BASIC UNIT NAME = NEW-AFOE-SHELTERS SYSTEMS = 20 NEWSHLTR-KNOCK New AFOE Shelter and Transport ASSAULT ECHELON UNIT = NEW-AFOE-SHELTERS STOP

			L85			•	•	•	•	•	•	•	•	•		• •	.0	•	•	• •			•	•	•		•	•	•	•	0	• •			•	•	•	•	•	;
PAGE 2			******CARGO******			•	•	•	••	•0	•	•	•	•	•	• •	•	• 0	• 0	•		•	•	2160.	•	• •	•	•	• 0	•	•	•	•	•	•	•	•	•	•	• •
			LAS NML			4400 NO	ON TOOLI		`.					33575. YES						21500 YES				83700. YES		12280. YES				5500.		SOUN YES			5215. YES		•	475.	4215. YES	
			SQ FT			88.	• 0 1	236.	236.	.0H	•	160.		320						• 02					968				352.	192.	1564.	99.	20	82.	82.	82.	82.	82.	82.	• 70
			710			<b>:</b> ,	• •	. ~	2.	1:	2.	2.	2.	17.			4	8.	÷.	:-	4	::	10.	27.	•	2	;	.2	2.	n' :	<b>D</b>	: -	: -	•	-	-	:	<b>:</b> .	•	• •
Table VIII-4	ISSUE OF MAJOR EQUIPMENT FOR SHELTER-AE	SQUARE LOADED EQUIPMENT	DESCRIPTION			AIRBORNE-MOBILE DIRE	TALK SOUTION IN TOURS	SHELTR NO 1, CALIB C	SHELTR NO 2, CALIB C	CALIHRATION SHOP.TRA	CENTAL OFFICE TELEPH	TEL SB AN/MTA-3, CEN	TEL TERMINAL GRP, CE	COMMUNICATIONS, CENT	OTOPOSTON FINDING BI	ELECTRONIC MONITOR A	INTERCEPT FACILITY H	LIGHT INTERCEPT FACT	RADAR, COURSE DIRECT	MAN DADAR SET ANTES	PADTO DIRECTION FIND	RADIO SET AN/TRC-97	SHELTER, ELECTRICAL	RIELECTRONIC	SHOP, ELECTRONIC, AN	SHOP. ELECTRONIC. AN	MUNITOW FAC	SIGNAL MONITOR FACIL	TRK. W/SHLTR, SIGNAL	TRLR. SIGNAL MONTR F	M CENTRL	ANITYALS I HIT	ON THE GO SOLVEY	OP HUT	OP HUT	OP HUT	1 do .	111	ANATANIB NO 1 SAHOT	2
	INITIAL ISSUE OF M	SQUARE	91			06743A	06/45A	042948	04294R	07507A	05921A	05921A	05921A	029584	04185A	05615A	03844B	07306A	01435A	02466A	023330	040410	000008	05476A	028190	010100	04954A	05851A	05851A	05851A	03485R	04019A	0401040	04019A	04019A	04019A	04019A	04019A	04019A	04014
20			CONTROL NUMBER OR FSN			A0010	40060	A0175A	A0175B	A0177	A0240	A0240A	A0240B	A0270	08204	A0525 A0625	A0860	A0865	A1350	A1460	41001H	A2091	A2310	A2320	A2340	A2360	A2392	A2394	A2394A	423948	A2440	A2530	406.00	A2530C	A25300	A2530E	A2530F	A2530G	A2530H	ACC301
DATE 2			CATEGORY	WEAPONS (CLASS VIIW)	OTHER CLASS VIIW													v	11	I-	12			,																



INITIAL ISSUE OF MAJOR EQUIPMENT FOR SHELTEH-AE SGUARE LOADED EQUIPMENT

BG0 * *																																														
**************************************	-	.0	•	•	••	•	.0	•	.0	.0	.0		•	•	•	•0	.0	•	•	.0	.0	.0	•	.0	•0	.0	.0		•	.0	•	•	•	•				•	.0	.0	0	.0	•	.0	.0	•
	NML	YFS	YES	YES	YES	YES	YES	YES	YES	YES	YFS	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	02	0	2	Ç	YES	YFS	0	ç	S	2	S	ON	ç	S	Ç	ç	ç	Ç	YES	02	ON
	LAS	5000	2920.	3810.	3450.	3900.	1300.	3494.	4021.	3991.	3921.	4106.	4271.	3841.	3841.	3851.	3831.	2981.	5100.	.0064	4844.	4800.	1130.	5040.	3400.	.0	32000.	32000.	5150.	33670.	14180.	21030.	16230.	28380.	65560.	19200.	66320.	88200.	111900.	200904.	106632.	108180.	12184R.	2	133144.	ċ
	SO FT	82.	82.	A2.	82.	A2.	26.	82.	82.	82.	82.	82.	82.	H2.	82.	82.	82.	82.	85°	95.	82.	82.	80.	102.	89.	•	316.	316.	.0A	360.	176.	226.	238.	213.	200	586.	848.	1326.	1098.	2025	1092.	1092.	1448.	112.	720.	•
	QTY	:	1.	1.	:	:	-	1:		:	.1	1:	1:	-	1:	:	-:	1.	:		:	:	:	2.	:	-:	1.	:	1:	2.	-1	:	5.	:	2	2.	;	• 9	•	12.	• 9	•	8.	:	*	<b>.</b>
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CONTRUL	OR FSN		A2530K	A2530L	A2530M	A2530N	A25300	A2530P	A25309	A2530R	A2530S	A2530T	A2530U	A2530V	A2530W	A2530X	A2530Y	A2530Z	A2540A	A2540B	A2540C	A2540D	A2540E	A2540F	A2540G	A2620	A2620A	A2620B	A2696	A3230	B1200	81455	81940	81950	81960	86295	00270	00200	DOSTOA	003108	00350	00330	01190	E0560	16	E1680
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550 FT 658. 658. 543. 282. 7243. 724. 724.

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2160.

32097. 2388466.

32097. 2388406.

VIII-14

OTHER CLASS VIIW

TOTAL CLASS VIIN

50

SHELTEH-AE	
FOR	
CARGO	
GENERAL	

CATEGORY CLASS I
CLASS IIIW (MARCORP)
CLASS VII NON-SQUARE

READ AN INPUT CARD. CARD IS...STOP

MOUNT OUT (CLASS III) FOR SHELTER-AE

# ORGANIZATIONAL LOAD

	500	CANS	.eeeeeees GAL CANSe. DOS CANS GALLONS	ANS **	DOS CANS GALLONS POUNDS		GALLONS POUNDS	DRUMS	GALLONS CU FT POUNDS	GALLONS CU FT POUNDS	SUNDO	***084	PACK	***ORY PACKAGES**
DIESEL	6	0		:	•		•	53.	2809.	583.	22498.			
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a,	•					.0	•	•	•	•	•0			
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DATE

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MOUNT OUT (CLASS III) FOR SHELTER-AE

## LANDING FORCE SUPPLIES

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CATEGORY	500	DRUMS	GALLONS	CU FT	CU FT POUNDS	500	DOS GALLONS CU FT POUNDS	C0 F1	POUNDS	500	DOS CU FT POUNDS	POUNDS
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MOGAS	~	15.	795.	165.	5667.	œ	3110.	417.	19002.			
a,	N	•	•	•	•	13	••	•	• 6			
KEROSENE	N	:	53.	111.	414.	æ	••	•	•0			
LUBE	10	ů.	270.	55.	2322.					0.0	•	••
LUBE (IIIA)	10	•	•	ċ	•							
CLASS IIIW (MARCORP)	10	•	•	•	•					10		208.
TOTAL		43.	2284.	473.	473. 17742.		7517.	7517. 1007.	49806.		7.	208.

This procedure was repeated to find the square increase in the assault follow-on echelon. Similar calculations are made for cube and weight. Additionally, fuel consumption and repair part utilization can be compared in an identical manner.

## F. The Effect of Introducing the Proposed New Shelter System Into the Lift Requirements of the Notional MAF

If the new system of shelters is adopted by the Marine Corps, the following impacts on the lift requirements of the notional MAF will result. These impacts are derived from a comparative analysis between the existing system and the replacement system of shelters using Program MAGTF.

- An increased 8,500-square-foot lift requirement for the assault echelon
- An increased 5,400-square-foot lift requirement for the assault follow-on echelon
- An increased 13,900-square-foot lift requirement for the entire MAF
- A 25 percent increase in the gallons of fuel required for both the assault echelon and the assault follow-on echelon of the MAF
- An increased 1,900-cubic-foot lift requirement for the assault echelon
- An increased 600-cubic foot lift requirement for the assault follow-on echelon.

The increases in square and bulk resulting from the introduction of the new shelter system were judged to be insignificant when compared with the total lift requirements of all landing force material in the MAF.

The increase in fuel requirements was found to be the result of freeing transports that were previously dedicated to shelters by introducing trailers to convey the new shelters by the use of the 6-ton tractor. Unlike the old dedicated vehicles, the new 6-ton tractor is capable of assisting in other logistic needs when not pulling trailers loaded with shelters. As a result, the new truck tractor is used many more hours per day than the dedicated vehicles and, therefore, consumes more fuel.

## G. Conclusions

- 1. The comparative analysis between the existing/replacement shelter systems performed with the assistance of Program MAGTF to determine the effects upon amphibious shipping requirements has demonstrated the usefulness of the program in a cube, square, and weight control program.
- 2. The "conceptual stage" of system and material acquisition by the Marine Corps could utilize Program MAGTF to determine the total effects of the new acquisition on the lift requirements of the MAF.
- 3. The utility of Program MAGTF may also be used in the "conceptual phase" of system and material acquisition to investigate the secondary effects of the acquisition, such as fuel consumption, repair parts requirements, ammunition consumption, and personnel requirements.

## IX AMPHIBIOUS STAFF PLANNING AND THE CONSTRAINED AMPHIBIOUS LIFT ANALYSIS SYSTEM (1985)

## A. General

The Constrained Amphibious Lift Analysis System (CALAS) developed during the course of conducting the Materiel Weight and Cube Control Study provided a systematic computational procedure to optimize the operational readiness of a MAGTF when required to be embarked into less amphibious assault shipping than needed for the specified MAGTF materiel. At the beginning of the project, no attempt was made to develop computer software requiring installation on a Marine Corps computer system. Those computer programs planned for development within the study were expected to be used to analyze data, perform necessary calculations, and to provide information necessary to gain insight into the complex problems presented by the study objectives. However, the solution to the problem of finding a practical means of temporarily eliminating items from unit T/Es necessary to reducing units' cargo requirements without decreasing the real operational readiness, resulted in the development of the Constrained T/E Embarkation Analysis Model whose capabilities became practical, relatively easy to use, and produced useful results in the constrained T/E listings and computed ordinal operational readiness index. With this development late in the study, the framework for a solution procedure involving all the earlier computer models was identified in such a way that the entire group of computer models formed the system called CALAS. It was then determined that CALAS was the type of system that could be installed as a computer assisted decision aid to the amphibious staff planner, where the computational power of its models could be combined with the experience and judgment of the commander and

staff, to rapidly identify the extent of a constrained ship loading problem for any size MAGTF, and then find the best solution within the existing constraints.

The difficulties associated with installing and utilizing computerized mathematical models developed during operations research studies for Headquarters, U.S. Marine Corps, is well recognized. While no deliberate attempt was initially made to provide models requiring such installation in an environment having no organization to perform such functions, the obvious long term usefulness of CALAS requires that a computer environment be identified for it to operate within. Furthermore, the solution options offered in this study for loading the notional CSS MAF into constrained shipping are certainly of interest in emphasizing the nature of problems to be faced by MAF commanders. However, the availability of CALAS to actually assist the commander and his staff in solving a real time problem is of much greater importance. Therefore, installation of CALAS in some USMC computer environment today and/or in the future demands careful consideration.

## B. CALAS Within an Automated Command and Control System

The definition of the future Automated Data Systems (ADS) to support Marine Corps information requirements is now being analyzed within on-going studies. The development of the Marine Tactical Command and Control System (MTACCS) is also in progress. While it is not possible to state the precise computer hardware/software structure that these systems may ultimately take, the residence of a software system such as CALAS within the future ADS structure is entirely feasible. It is the operational configuration of the future ADS structure to support CALAS that is proposed in the following discussion. Whether there will be one Management Information System (MIS) supporting

administrative information requirements and the subsystems comprising MTACCS being available in garrison and deployed, or two separate systems each supporting specifically designated subsystems operating side by side is not of concern to this presentation.

## 1. CALAS and MIS

The time is 1985. A warning order has been received by CG of the MAF involving a possible combat mission for a MAGTF to deploy by sea to a specified area in the world.

The commander and his staff select a troop list to execute the mission. The G-4 prepares an input list for the MAGTF subsystem within CALAS to generate the lift requirements. A computer terminal placed in the G-4 office is used to input the troop list and the necessary days of supply formatted for the MAGTF Program. When the input list is entered, the G-4 operator executes the MAGTF Program. The version installed has been modified so that it executes in less than three hours, depending on the number of units in the troop list. Should the force be a MAF, then the MAGTF run would consist of only the assault echelon units so that output would be immediately available for determining the assault shipping requirements. The run for the AFOE would be executed at a later time.

In this environment, the MAGTF output listings would be directed to be printed at the Force Automated Services Center (FASC), if desired, but any page of the printed listing could be presented on the computer terminal scope--also when desired. A disk file would have been created by the MAGTF Program containing the factored cargo data needed for input to the Constrained Cargo Factoring Model (CCF).

The G-4 determines from the Commander Amphibious Task Force (CATF) or appropriate type commander the number of amphibious assault

ships to be made available. With this information, the input ship file (which always contains all USN available ships on the MIS) for the CCF Model is modified for the simulated loading problem. The G-4 operator then executes the CCF Model for no constrained loading unless previous experience indicates a lift short fall will be certain. In this case, the CCF Model can be run with constrained values from 100 to 60, or as desired by varying the constraint file within the MIS through the terminal. The results from the CCF Model are printed on the scope, and the G-4 observes that a short fall of some significant magnitude exists. He also observes the short fall computed from each constraint. He finds that, after constraining the T/E by 70 percent, all the ships are loaded. However, he would like to rerun the CCF Model, changing the DOS for mountout. After observing the combined effect of constraining unit T/Es and reducing mountout, he now examines the constrained T/E listings for any units of interest as computed from the Constrained T/E Embarkation Analysis Model (CTEAM) for the constraints used. These listings indicate the equipment to be eliminated from the unit load and put in assault shipping, be left behind, or carried in follow-on shipping.

In reviewing the eliminated T/E listing of units for the constraint value of interest, any TAM items designated for elimination that the staff planner considers essential for the mission assigned can have their criticality factor changed within the input file for the CTEAM Model. The model can continue to be reprocessed until the unit or units eliminated T/E listing meets the needs of the mission.

After making T/E adjustments and reviewing results, the G-4 may now present recommendations to the CG for alterations of the troop list based on the results produced by CALAS. Depending on the CG's decision, the G-4 may either have an acceptable constrained loading problem solution or be required to make further adjustments to the troop

list and resolve the problem, in total or only partially, through CALAS. He is now ready to issue the warning order to subordinate commands. The important fact is that all these calculations and adjustments were made in less than 5 hours.

At each level of command, the same type of terminal is available to the staff, and the constrained loading problem may be solved for a reduced size problem pertinent to each command level. For instance, the CO BLT may be interested in looking at the T/E presented by the MAGTF Program to compare the lift requirement developed from authorized allowances for an infantry battalion with what he has on hand for some appropriate action. The criticality factors used in the system may be of more interest to this level and could be altered as needed to recompute the constrained T/E from the latest adjustments.

The description presented here assumed that all programs constituting CALAS were installed on the MIS, that all data files were resident on the MIS data base and accessed by the programs as needed, that all system job control commands were resident on the system, and that execution commands were structured to be easily used by terminal operators. Nothing presented here is beyond the current technical operational capability of USMC computer systems.

## 2. Development of MIS Information Requirements

Studies conducted to develop information requirements for an MIS have had great difficulty. Perhaps an approach to determining MIS requirements is the study of problems within functional areas seeking useful solution. As in this study, the definition of information requirements that may be incorporated into an MIS may very well arise from independent study of the functional problem. This approach may suggest the procedure to follow in defining information requirements for other functional problems.

## C. Implementation Considerations

As previously indicated, installation of CALAS on a USMC computer system is entirely possible. It could be installed in the current MAF FASC environment and converted later to an MIS environment. There are a number of implementation tasks that would have to be accomplished. These tasks are briefly described below.

## 1. Program Conversion to IBM 360

All CALAS programs were developed to support the analysis of the current study, and were written for the CDC 6400 SRI computer.

Certain program statements would have to be modified and tested for an IBM 360 before installation.

## 2. MAGTF Improvement Project

The current version of the MAGTF Program is still less efficient than is possible for minimum time operation. A proposal has been submitted to HQMC to conduct the improvement task so that the system could operate efficaciously on the MAF computers.

## 3. MAGTF Data Base Maintenance

The validity of CALAS depends on the accuracy of the MAGTF data base. MAGTF has been operational for just over one year. Experience gained during this period has demonstrated the need to have an ongoing program to maintain the currency of the files. SRI has also submitted a proposal to provide maintenance support for this effort. Included in this proposal are certain modifications to the peripheral programs updating the data base that will improve completeness and reduce the current level of manual update requirements.

## 4. Development of Criticality Factors for All FMF T/Es

For the current study, only a sample of 10 units were coded which assigned criticality factors to TAM items in the T/Es. This coding was all done to current unit T/Es. Since the shift to the new CSS structure for the final analysis of the study, these coded T/Es were also obsolete, but had to be used. For implementation, all current FMF T/Es would have to be coded using the same guidance followed during this study.

There will no doubt be additional tasks defined for system implementation should a detailed study of requirements be authorized.

## D. Conclusions

The following conclusions from this section are presented.

- It is feasible to implement CALAS on USMC computer systems to function as a computer assisted decision aid.
- (2) Current USMC computer installation work loads will dictate the timing of installing CALAS on USMC computer systems.

Appendix A

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## Appendix A

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Appendix B

TROOP LISTS AND SAMPLE MAGTE OUTPUT

Part 1: Troop Lists

## MARINE AMPHIBIOUS FORCE (MAF) TROOP LIST FOR MAGTF LIFT REQUIREMENTS (NOTIONAL MAF)

Assault Echelon: Command Element\*

T/O No.	Unit Type Code	Multiple	Unit Descriptor
4623M	PTLAA	1	For Recon Co
4722M	PYDAA	2	CI Team
4732M	PUEAA	2	SCC Team
4918M	CS2AA	1	HQ MAF
4919M	9BUAA	1	H&S Co, MAF
4998M	VYBAA	1	Civil Affairs Group
	Radio	<u>Bn</u>	
4735M	PU1AB	1	EW Co
4735A	PU2AB	1	Aug EW Co
4736M	PU3AB	1	Opns Co
4736A	PU4AB	1	Aug Opns Co
4737M	PU5AB	1	H&S Co
4737A	PUBAB	1	Aug H&S Co
	Communica	ations Bn	
4863M	6UNAA	1	Comm Spt Co
4873M	6UMAA	1	Long Lines Co
4883M	9UK AA	1	Comm Co
4886M	9UJAA	1	HQ Co

<sup>\*</sup> MAGTF data base designation for entire Command Element:

T/O No. = CMD-GP Unit type code = CS2AA

Multiple = 1

Assault Echelon: Ground Combat Element

<u>T/O No.</u>	Unit Type Code	Multiple	<u>Unit Descriptor</u>
	Marine D	ivision /-/	
1038M	9GUAA	9	Inf Bn, Inf Regt
1096M	9GSAA	3	HQ Co, Inf Regt
1128M	9HLAA	3	D/S Arty Bn, Arty Regt
1196M	9HE AA	1	HQ Btry, Arty Regt
1378M	4HTAA	1	Engr Bn, MARDIV
1423M	PHRAA	4	Recon Co, Recon Bn
1427M	9HQAA	1	H&S Co, Recon Bn
1653M	UJUAA	3	Truck Co, MT Bn
1657M	9JTAA	1	H&S Co, MT Bn
1883M*	6GJAA	1	Comm Co, HQ Bn
1903M*	QGHAA	1	MP Co, HQ Bn
1985M*	9GGAA	1	Serv Co, HQ Bn
1986M*	M1986	1	Div HQ, HQ Co, HQ Bn
1987M*	9GLAA	1	HQ Co, HQ Bn
	<u>Ta</u>	nk_Bn	
4233M	2SRAA	4	Med Tank Co
4237M	9SNAA	1	H&S Co, Tank Bn
	АМТ	DAC Do	
	AMI	RAC Bn	
4652M	2TXAB	4	AMTRAC Co
4654M	9TWAA	1	H&S Co, AMTRAC Bn
	Field Art	illery Group	
	Fleid Alt	IIIely Gloup	
4112M	1SHGA	1	8" How Btry
4193M	1SKGA	2	175 Gun Btry
4201M	1YK AA	1	Searchlight Btry
4226M	9SGAA	1	HQ Btry, FAG

<sup>\*</sup> MAGTF data base designation for all units noted:

T/O No. = 1998M

Unit type code = 9GDEJ

Multiple = 1

### Assault Echelon: Aviation Combat Element

<u>T/O No</u> .	Unit Type Code	Multiple	Unit Descriptor
0601F	CLDAA	1	HQ /-/ Marine Air Wing
0604F	8LK AA	1	MWHS /-/
	Marine Air (	Control Grou	<del>īb</del>
8612M	8LZAA	1	MWCS
8615M	8LPAA	1	H&HS, MACG
8625M	3LTAA	1	FAAD Btry
8631M	7LSAA	1	MACS/MTDS
8640M	7LRAA	1	MASS, MACG
	2nd Marine A	Air Group (	<u>/H)</u>
8621M	3LYAA	1	Missile Btry, LAAM Bn
8821M	7NLAA	2	MATCU
8859M	3NSAA	1	VMA (V) (20AV-8A)
8914M	8PCAA	2	H/MS (single site)
8921M	8PDAA	2	MABS (single site)
8937M	3PNAA	3	HMM (18 CH-46)
8944M	3PLAA	3	HMH (18 CH-53A)
8964M	3PQAA	2	HMM (21 UH-1N)
8968M	3PFAA	1	VMO (18 OV-10A)
8970M	3PU AB	1	HMA (18 AH-1J)

Assault Echelon: Combat Service Support Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor	
Medical Bn				
1523M	FJQAA	4	C/C Co, Med Bn	
1557M	9ЈРАА	1	H&S Co, Med Bn	
	Servi	ce Bn		
0300F	м0300	1	HQ Force Log Serv	
0301F	JJEAA	1	Supply Co, Serv Bn	
0303F	9ЈВАА	1	H&S Co, Serv Bn	
1743M	HJFAA	1	Maint Co, Serv Bn	
1753M	UJCAA	1	Truck Co, Serv Bn	
175511	OJGAN	•	rrack oo, berv bu	
	Shore Pa	arty Bn		
1863M	9JKAA	3	SP Co, SP Bn	
1867M	9JJAA	1	H&S Co, SP Bn	
	Military 1	Police Bn		
4903M	QURAA	3	MP Co, MP Bn	
4907M	9UQAA	1	H&S Co, MP Bn	
	Facia	oor Po		
	Engine	eer Bn		
0305F	9SYAA	1	Serv Co /-/ Engr Bn	
0307F	9SXAA	1	HQ Co /-/ Engr Bn	
4353M	4SZAA	2	Engr Co, Engr Bn	
	Det Force S	ervice Regt		
0312F	HVTGA	1	Det MT Maint Co	
0314F	9VSAA	1	Det H&S Co, Maint Bn	
0322F	JVLAA	1	Det Supply Co, Sup Bn	
0324F	JVPAA	1	Det Ration Co	
0326F	JVMAA	1	Det Ammo Co	
0332F	JVGAA	1	Det Support Co	
0701F	M0701	1	Naval Beach Group	
3223M	HVYGA	1	Ord Maint Co	
3243M	HVQGA	i	Engr Maint Co	
3253M	HVUGA	1	Elec Maint Co	
		1	Bulk Fuel Co	
3333M	JVNAA	1	bulk ruel Co	

<sup>-</sup> Total Assault Echelon -

Assault Follow-On Echelon: Command Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
4392M	4TBAA	1	TOPO Plt
4722M	PYDAA	1	CI Team

Assault Follow-On Echelon: Aviation Combat Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
0602F	CLDAA	1	Det HQ MAW
0605F	8LKAA	1	Det MWHS
8820M	8NK AA	3	MABS, MAG VA/VF/VA (AW)
	LA	AM Bn	
8620M	8LXAA	1	H&S Btry, LAAM Bn
8621M	3LYAA	2	Missile Btry, LAAM Bn
	MWSO	G /-/	
8710M	8MLAA	1	H&MS, MWSG
8715M	8MN AA	1	WERS

Assault Follow-On Echelon: Combat Service Support Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
3333P	JTCAA	1	Sep Bulk Fuel Co
4343M	4SUAA	1	Bridge Co
4512M	FTGAA	1	Hosp Co
4552M	FTFAA	4	Dental Co
4592M	FJJAA	1	Sep Surgical Co
4903M	QURAA	1	MP Co
	Det Serv	vice Bn	
0302F	JJEAA	1	Det Sup Co
0304F	9JBAA	1	Det H&S Co
	Motor Tran	sport Bn	
4643M	UTSAA	3	Truck Co
4644M	UTRAA	1	Transport Co
4647M	9TQAA	1	H&S Co
	Engine	er Bn	
0306F	9SYAA	1	Det Service Co
0308F	9SXAA	1	Det HQ Co
4353M	4SZAA	2	Engr Co
	T	D / /	
	Force Servic	e Regt /-/	
0313F	HVTGA	1	MT Maint Co /-/
0315F	9VSAA	1	H&S Co /-/ Maint Bn
0323F	JVLAA	1	Supply Co /-/ Supply Bn
0325F	JVPAA	1	Ration Co /-/ Supply Bn
	JVMAA	1	Ammo Co /-/ Supply Bn
0333F	JVGAA	1	Support Co /-/ H&S Bn
0702F	M0702	1	Mobile Constr Bn
3213M	HVXGA	1	GS Supply Maint Co
3346M	9VK AA	1	H&S Co, Supply Bn
3403M	JVHAA	1	Longshoreman Co, H&S Bn
3413M	UVEAA	1	Truck Co, H&S Bn
3443M	6VFAA	1	Comm Co, H&S Bn
3447M	9VDAA	1	H&S Co, H&S Bn
	3333P 4343M 4512M 4552M 4592M 4903M 0302F 0304F 4643M 4644M 4647M 0306F 0308F 4353M 0313F 0315F 0323F 0325F 0327F 0323F 0325F 0327F	3333P JTCAA 4343M 4SUAA 4512M FTGAA 4552M FTFAA 4592M FJJAA 4903M QURAA     Det Serve   O302F JJEAA     O304F 9JBAA     Motor Transe   4643M UTSAA     4644M UTRAA     4647M 9TQAA     Engine   O306F 9SYAA     O308F 9SYAA	3333P

<sup>-</sup> Total Assault Follow-On Echelon -

Fly-In Echelon: Aviation Combat Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
0603F	CLDAA	1	Det HQ Marine Air Wing
8652M	3QJAB	1	VMCJ (7 RF-4, 7 EA-6)
8712M	8LE AA	1	MWWU
8780M	3MQAA	1	VMGR
8821M	7NLAA	3	MATCU
	Det 3rd Marine	Air Group (	VF/VA)
8813M	Det 3rd Marine A	Air Group (N	<u>VF/VA)</u> H-MS MAG (VA/VF)
8813M 8849M			
	8NJAA	3	H-MS MAG (VA/VF)
8849M	8NJAA 3NMAC	3 4	H-MS MAG (VA/VF) VMFA (15 F-4J)
8849M 8855M	8NJAA 3NMAC 3NSAB	3 4 2	H-MS MAG (VA/VF) VMFA (15 F-4J) VMA (20 A-4)

- Total Fly-In Echelon

\*\*\* Total Notional MAF \*\*\*

### MARINE AMPHIBIOUS FORCE (MAF) TROOP LIST FOR MAGTF LIFT REQUIREMENTS (CSS NOTIONAL MAF)

CSS Assault Echelon: Command Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
CMD-GP*	CS2AA	1	Command Group

<sup>\*</sup>MAGTF data base designation "CMD-GP" includes all units noted in the notions! MAF shown in Part 1 of this appendix.

CSS Assault Echelon: Ground Combat Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
1038M	9GUAA	9	Inf Bn, Inf Regt
1096M	9GSAA	3	HQ Co, Inf Regt
1128M	9HLAA	3	D/S Arty Bn, Arty Regt
1196M	9HE AA	1	HQ Btry, Arty Regt
1363X	4HYAA	1	Engr Spt Co, Cbt Engr Bn, DSG
1373X	4HWAA	4	Engr Co, Cbt Engr Bn, DSG
1377X	9ннаа	1	H&S Co, CBT Engr Bn, DSG
1423M	PHRAA	4	Recon Co, Recon Bn
1427M	PHQAA	1	H&S Co, Recon Bn
1862X	UJUAA	1	Truck Co, H&S Bn, DSG
1863X	9JYAA	1	Log Spt Co, H&S Bn, DSG
1864X	M1864	1	Svc Co, H&S Bn, DSG
1867X	M1867	1	HQ Co, H&S Bn, DSG
1988M	9GDEJ	1	HQ Bn, MARDIV
4112M	1SHGA	1	8" How Btry
4193M	1SKGA	2	175 Gun Btry
4201M	1YK AA	1	Searchlight Btry
4226M	9SGAA	1	HQ Btry, FAG
4233M	2SK AA	4	Medium Tank Co
4237M	9SNAA	1	H&S Co, Tank Bn
4623M	M4623	1	Force Recon Co
4643F	M4643	1	Det Trk Co, MT Bn
4652M	2TXAB	4	AMTRAC Co (LVTP-7)
4654M	9TWAA	1	H&S Co, AMTRAC Bn

CSS Assault Echelon: Combat Service Support Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
0305F	9SYAA	1	Spt Co /-/ Engr Spt Bn
0307F	9SXAA	1	HQ Co /-/ Engr Spt Bn
0701F	M0701	1	Det B&P Co
3223X	HVYGA	1	Ord Maint Co
3233F	HVTGA	1	MT Maint Co /-/
3243X	HVWG A	1	Engr Maint Co
3247F	M3247	1	H&S Co /-/ Maint Bn
3253X	HVUGA	1	Elec Maint Co
3313F	M3313	1	Det Supply Co, FSSG
3323F	M3323	1	Det Ration Co, FSSG
3343F	M3343	1	Det Ammo Co, FSSG
3442F	M3442	1	Det B&P Co, H&S Bn
3447F	M3447	1	H&S Co, Sup Bn
3751X	M3751	1	Bulk Fuel Co, Engr Spt Bn
3753X	4SZAA	2	Engr Co, Engr Spt Bn
3851X	FTFAA	1	Dental Co
3853X	FJQAA	4	Med Co, Med Bn, FSSG
3857X	9JPAA	1	H&S Co, Med Bn, FSSG
4903M	QURAA	3	MP Co, MP Bn
4907M	9UQAA	1	H&S Co, MP Bn

CSS Assault Echelon: Aviation Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
0601F	CLDAA	1	HQ /-/ Marine Air Wing
0604F	8LK AA	1	MWHS /-/ Det
8612X	8LZAA	1	MWCS, MACG Planning
8615X	8LPAA	1	H&HS, MACG Planning
8621X	3LYAA	1	Missile Btry, LAAM Bn
8625X	3LTAA	1	FAAD Btry, MACG, MAW Planning
8631X	7LSAA	1	MACS/MTDS Planning
8640X	7LRAA	1	MASS, MACG Planning
8821M	7NLAA	2	MATCU
8859X	3NSAA	1	VMA (V)
8914X	8PCAA	2	H-MS (single site)
8921M	8PDAA	2	MABS (single site)
8937X	3PNAA	3	HMM (18 CH-46)
8943X	3PLAA	3	HMH (18 CH-53A)
8964X	3PQAA	2	HML
8968X	3PFAA	1	VMO (18 OV-10A)
8970X	3PU AB	1	HMA (18 AH-1J)

<sup>-</sup> Total CSS Assault Echelon -

### CSS Assault Follow-On Echelon: Command Element

T/O No.	Unit Type Code	Multiple	Unit Descriptor
4392M	4TBAA	1	TOPO Plt
4722M	PYDAA	1	CI Teams

### CSS Assault Follow-On Echelon: Aviation Element

T/O No. Unit Type Code Multiple Unit Descript	or
0602F CCDAA 1 Det HQ, Marin	e Air Wing
0605F 8LKAA 1 Det MWHS	
8620X 8LXAA 1 H&S Btry, LAA	M Bn
8621X 3LYAA 2 Missile Btry,	LAAM Bn
8710X 8MLAA 1 H&MS, MWSG	
8714X M8714 1 Engr Sqdn	
8715X 8MNAA 1 Trans Sqdn	
8820X 8NKAA 3 MABS, MAG VA/	VF/VA (AW)
8821M 7NLAA 3 MATCU	

CSS Assault Follow-On Echelon: Combat Service Support Element

3752X 45UAA 1 Bridge Co, Engr Spt Bn		Unit Type Code	Multiple	Unit Descriptor
3247N       9VSAA       1       H&S Co /-/ Maint Bn         3313N       JVLAA       1       Supply Co /-/ Supply Bn         3323N       M3323       1       Ration Co /-/ Supply Bn         3343N       JVMAA       1       Ammo Co /-/ Supply Bn         3347X       9VKAA       1       H&S Co, Supply Bn         3442N       M3442       1       B&P Co, H&S Bn         3443X       6VFAA       1       Comm Co, H&S Bn, FSSG         3444N       M3444       1       MP Co, H&S Bn, FSSG         3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	0702F	M0702	1	Mobile Const Bn
3313N       JVLAA       1       Supply Co /-/ Supply Bn         3323N       M3323       1       Ration Co /-/ Supply Bn         3343N       JVMAA       1       Ammo Co /-/ Supply Bn         3347X       9VKAA       1       H&S Co, Supply Bn         3442N       M3442       1       B&P Co, H&S Bn         3443X       6VFAA       1       Comm Co, H&S Bn, FSSG         3444N       M3444       1       MP Co, H&S Bn, FSSG         3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	3233N	HVTGA	1	Det MT Maint Co
3323N       M3323       1       Ration Co /-/ Supply Bn         3343N       JVMAA       1       Ammo Co /-/ Supply Bn         3347X       9VKAA       1       H&S Co, Supply Bn         3442N       M3442       1       B&P Co, H&S Bn         3443X       6VFAA       1       Comm Co, H&S Bn, FSSG         3444N       M3444       1       MP Co, H&S Bn, FSSG         3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	3247N	9VSAA	1	H&S Co /-/ Maint Bn
3343N       JVMAA       1       Ammo Co /-/ Supply Bn         3347X       9VKAA       1       H&S Co, Supply Bn         3442N       M3442       1       B&P Co, H&S Bn         3443X       6VFAA       1       Comm Co, H&S Bn, FSSG         3444N       M3444       1       MP Co, H&S Bn, FSSG         3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	3313N	JVLAA	1	Supply Co /-/ Supply Bn
3347X       9VKAA       1       H&S Co, Supply Bn         3442N       M3442       1       B&P Co, H&S Bn         3443X       6VFAA       1       Comm Co, H&S Bn, FSSG         3444N       M3444       1       MP Co, H&S Bn, FSSG         3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	3323N	M3323	1	Ration Co /-/ Supply Bn
3442N       M3442       1       B&P Co, H&S Bn         3443X       6VFAA       1       Comm Co, H&S Bn, FSSG         3444N       M3444       1       MP Co, H&S Bn, FSSG         3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	3343N	JVMAA	1	Ammo Co /-/ Supply Bn
3443X       6VFAA       1       Comm Co, H&S Bn, FSSG         3444N       M3444       1       MP Co, H&S Bn, FSSG         3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	3347X	9VK AA	1	H&S Co, Supply Bn
3444N       M3444       1       MP Co, H&S Bn, FSSG         3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	3442N	M3442	1	B&P Co, H&S Bn
3445N       M3445       1       Svc Co, H&S Bn, FSSG         3447N       9VDAA       1       H&S Co, Sup Bn         3751X       JTCAA       1       Bulk Fuel Co, Engr Spt Bn         3752X       45UAA       1       Bridge Co, Engr Spt Bn	3443X	6VFAA	1	Comm Co, H&S Bn, FSSG
3447N         9VDAA         1         H&S Co, Sup Bn           3751X         JTCAA         1         Bulk Fuel Co, Engr Spt Bn           3752X         45UAA         1         Bridge Co, Engr Spt Bn	3444N	M3444	1	MP Co, H&S Bn, FSSG
3751X JTCAA 1 Bulk Fuel Co, Engr Spt B 3752X 45UAA 1 Bridge Co, Engr Spt Bn	3445N	M3445	1	Svc Co, H&S Bn, FSSG
3752X 45UAA 1 Bridge Co, Engr Spt Bn	3447N	9VDAA	1	H&S Co, Sup Bn
HE CONTROL (CONTROL CONTROL CO	3751X	JTCAA	1	Bulk Fuel Co, Engr Spt Bn
3753x 45ZAA 1 Engr Co. Engr Spt Bn	3752X	45UAA	1	Bridge Co, Engr Spt Bn
2,331	3753X	45ZAA	1	Engr Co, Engr Spt Bn
3755N M3755 1 Engr Spt Co, Engr Spt Bn	3755N	M3755	1	Engr Spt Co, Engr Spt Bn
3757N M3757 1 H&S Co, Engr Spt Bn	3757N	M3757	1	H&S Co, Engr Spt Bn
3851X FTFAA 3 Dental Co	3851X	FTFAA	3	Dental Co
3853X M3853 1 Med Co, Med Bn, FSSG	3853X	M3853	1	Med Co, Med Bn, FSSG
3854X M3854 1 Hosp Co, Med Bn, FSSG	3854X	M3854	1	Hosp Co, Med Bn, FSSG
4643N UTSAA 1 Trk Plt, Trk Co	4643N	UTSAA	1	Trk Plt, Trk Co
4644X UTRAA 1 Trans Co, MT Bn, FSSG	4644X	UTRAA	1	Trans Co, MT Bn, FSSG
4647X 9TQAA 1 H&S Co, MT Bn, FSSG	4647X	9TQAA	1	H&S Co, MT Bn, FSSG
4903M QURAA 1 MP Co, MP Bn	4903M	QURAA	1	MP Co, MP Bn

<sup>-</sup> Total CSS Assault Follow-On Echelon -

CSS Fly-In Echelon

T/O No.	Unit Type Code	Multiple	Unit Descriptor
0603F	CLDAA	1	Det HQ, Marine Air Wing
8652M	3QJAA	1	VMCJ (7 RF-4 / 17 EA-6)
8712M	8LEAA	1	MWWU
8780X	3MQAA	1	VMGR (12 KC-130)
8813X	3NJAA	3	H-MS MAG (VA/VF)
8848X	3NMAC	4	VMFA (15 F-4J)
8855M	3NS AB	2	VMA (20 A-4)
8857X	3NUAA	2	VMA (AW) (12 A-6A)

- Total CSS Fly-In Echelon -

\*\*\* Total CSS Notional MAF \*\*\*

Appendix B

TROOP LISTS AND SAMPLE OUTPUT

Part 2: Sample Output

DATE 2

•						
T/O DESIGNATOR	M1038					
NAME	INFANTRY BATTAL	INFANTRY BATTALION.INFREGT.MARDIV	>			
COMPONENT OF						
CONSISTING OF	UNIT NAME		TOTAL	TOTAL FOR COMPONENT	LENT	
SYSTEM NAME E0892 SYSTEM NAME E1155 SYSTEM NAME K4810 SYSTEM NAME K4800 SYSTEM NAME C3340 SYSTEM NAME C3255 SYSTEM NAME C3430 SYSTEM NAME A1950 SYSTEM NAME A1950 SYSTEM NAME A1950 SYSTEM NAME A1950 SYSTEM NAME K4180 SYSTEM NAME C3330 SYSTEM NAME C3330	M1013  OUE S  DOE S  DOE S  OOF S  W1037  M1037  DOE S  DOE S	NOT EXIST.				
		PERSONNEL		OFF I CER	ENL ISTED	TOTAL
			MARCORP	\$	11117	1162
			NAVY	n	65	89
			GRAND TOTAL	<b>*</b>	1182	1230

## INITIAL ISSUE OF MAJOR EQUIPMENT FOR MI038

### SOUARE LUADED EQUIPMENT

8380. NG CU FT CO FT FT CO FT
100000000000000000000000000000000000000

DATE

INITIAL ISSUE OF MAJOR EQUIPMENT FOR MIG38

### NUN-SQUARE LOADED EQUIPMENT

	CONTROL				******	
CATEGORY	OR FSN	2	DESCRIPTION	410	CU FT	LBS
URGANITATIONAL WONS						
		04706A	MORTAR, INFANTRY, 60	12.	144.	.009
	E1090	V61500	MORTAR, INF. 81MM, W29	•	*96*	•096
OTHER CLASS VIIW						
	A1083	05975C	NIGHT VISION SIGHT.	36.	36.	468.
	A3275	03448A	WEAPON SIGHT, INFRA-	16.	16.	448.
	A0005	041774	ACCESSORY KIT. RADIO	:	2.	159.
	A0090	04531A	BATTERY CHARGER PP-6	13.	39.	6111
	A0320	000044A	CONTROL RADIO SET. A	12.	12.	240.
	A0328	06692A	. CONVERTER FREQUENCY	:	:	36.
	A0490	047048		25.	25.	300.
	A0710	00124C	SIGNAL .	:	:	45.
	A0800	000368	GENERATOR SIGNAL. AN	:	5.	**6
	A0922	03449A	METASCOPE. ASSEMBLY.	15.	15.	45.
	A1086			:	12.	156.
	A1087	07098A	NIGHT VISION SIGHT.	*	20.	236.
	A1180	043100	OSCILLOSCOPE. AN/USM	:	:-	26.
	A1240	00251B	POWER SUPPLY, PP-388	:		252.
	A1250	07021A	POWER SUPPLY PP	8.	2.	20.
	A1420	05867A	RADAR SET AN/PPS-6	2.	22.	186.
	A1570	02394A	RADIAC COMPUTER INDI	•	:	<b>4</b> 5.
	A1730	04616A		15.	15.	330.
	A1800	04617A		7.		392.
	A1940	07009A	SET.	2.	100	5150.
	A2010	03816A	SET.	ë.	24.	303.
	A2020	03817A		2.	40.	695.
	A2040	06828A	SET	3.	3.	.69
	A2050	05916A	RADIO SET. AN/PRC-77	58.	58.	1160.
	A2150	04622A	RADIO SET. ANVARC-47	2	:	220.
	42240	A11210	SACIO IERRINAL SELAN	• ,	:.	• • • • • • • • • • • • • • • • • • • •
	42390	067154	STONAL I AND FOLLOWER		:	• • •
	A2480	00276A	SWITCHBOARD, TELEPHO			140
	A2580	00092A	TELEGRAPH TERMINAL G	3.	3.	291.
	A2660	A14000	TELF TYPEWRITER SET.	:	3.	•06
	A2685	06963A	TERMINAL. TELEGRAPH-	:	:	*0*
	A2700	04680A	KIT.	:	:	20.
	A2710	04679A	KIT.	2.	2.	20.
	A2900	003168	TEST SET. RADAR, TS/	:	2.	30.
	A3280	07096A	VOLTMETER ANJUSH-328	3.	3.	45.
	81360	03965A	MOTOR GENERATOR, PU-	:	8	255.
	C6215	V ₩ 6890	SPRAYER AND DUSTER.	:	•	84.

## INITIAL ISSUE OF MAJOR EQUIPMENT FOR MI038

18

DATE

## NON-SQUARE LOADED EQUIPMENT

DESCRIPTION
CIRCLE . AIMING . M2
COMPRESSUR, RECIPROCA
QUADRANT. FIRE CONTR
TELESCOPE, DASERVATI
FREQUENCY METER, ANY
GENERATUR SIGNAL . AN
MULTIMETER. ELECTRON
MULTIMETER AN/PSM-4E
_
PUBLIC ADDRESS SET.
RADIAC SET. AN/PDR-2
RADIAC METER. IM-174
TELEPHONE SET, TA-31
TEST SET, RADIO, AN
-
-

2118. 19672.

INITIAL ISSUE OF SECONDARY EQUIPMENT AND SUPPLIES FOR M1038

POUNDS	357399.	15.	357414.	245.	245.	357659.
CU FT	24945.	°G	24950.	15.	15.	24965
CATEGORY	CLASS IIW (TYPE 1)	CLASS IIW (TYPE 2)+	TOTAL CLASS IIW	CLASS IV (TYPE 2)*	TOTAL CLASS IV	TOTAL INITIAL ISSUE

\* NON-CONSUMABLES ONLY

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CATEGORY

POUNDS 0.

CU FT

INITIAL ISSUE PLUS MOUNT OUT (90 DAYS) OF SECONDARY EQUIPMENT AND SUPPLIES FOR MID38

TOTAL

OPERATING STOCKS OF MI038

POUNDS 76112. 76112.

CU FT

CATEGORY

CLASS 1XW 1466.

TOTAL 1466.

18

QUANTETY	ż		12.		35.	2.		36.	12.	40.	291.	29.	938.
DESCRIPTION	CL VII RIFLE, 106MM, M40AIC, W/E -MT		CL VII MORTAR. INFANTRY. 60MM M89/M2	IORT AR. INF. 81 MM. M29 W/E	MACHINE GUN 7.62MM M60	DISPERSER, RIOT CONTROL AGENT.		AUNCHER, GRENADE, 40MM, M79 W	CL II LAUNCHER, ROCKET, 66MM M-202	LAUNCHER, RKT. 351N, M20A1BI W/F	PISTOL. AUTO. CAL 45. MIGITAL.	PROJECTOR, PYROTECHNIC, HAND.	RIFLE. S.SMM. MISAI. W/E
UPPLY	Ę		111	- 117	- 11	=		1 11	1 11	- 11	11	11	11
SUPPLY	3		5	7	5	5		5	5	5	7	C	200
2	033288		04705A	00519A	02705A	03893A		02627A	07265A	005088	00526A	00530A	5538A
	•		ò	ŏ	ö	0		ö	0	ŏ	ŏ	ŏ	5
CONTROL NUMBER OR FSN	E1 ◆ 8 0		E1060	E1090	E0990	E0320		E0890	E0900	E0920	E1180	E1240	E1440 A
		NS	W	E	W	W	S	W	W	W	W	ш	A
CATEGORY	ORGANIZATIONAL WPNS SQUAKE LUADED	URGANIZATIONAL WPNS					INDIVIDUAL WEAPONS						

DATE

CU FT	49856.
	ALLUWANCE
CATEGORY	STAL INITIAL ALLUWANCE

NML INITIAL ALLOWANCE

92089. 626857.

7890.

POUNDS

DATE

	POUNDS	•	•	3644. 119925.	922.	120847.	8856.	3401.	2011.
	CU FT	•	•	3644.	48.	3691.	349.	215.	118.
	s00	0	•	15	15		15		15
R M1038	CU FT POUNDS	• 0	•	19950.	615.	80565.	5904.	132.	79. 1341.
VIII) FO	***LANFOR SUPPLIES*** DOS CU FT POUNDS	•	•	2429.	32.	2461.	232.		.62
O CLASS	***LAN	•	•	01	01		01		01
MOUNT OUT (CLASS I. CLASS VI. AND CLASS VIII) FOR MIG38	CU FT POUNDS	•	•	39975.	307.	40282.	2952.	3269.	670.
SS 1. CLA	**************************************	•	•	1215.	16.	1230.	116.	207.	39.
UT CCLA	500	•	•	S	S		v		<b>I</b> O
MOUNT O	CATEGORY	CLASS I(A RATIONS)	CLASS I(B RATIONS)	CLASS I(MCI)	CLASS I(TRIOXANE)	TOTAL CLASS I	CLASS VIERAT SUPP)	CLASS VIII(MED/DEN)	CLASS VIIIIMED REPLI
	J	CLASS	CLASS	CLASS	CLASS	TOTAL	CLASS	CLASS	CLASS

GALLONS DRGANIC WATER CARRYING CAPACITY FOR MID38

CUNTAINER

S GAL CANS

1950.

1950. TOTAL DRGANIC CAPACITY

6

## MOUNT OUT (WATER) FOR MI038

GAL/MAN TOT GAL

ORGANIC REQUIREMENT	JIREMENT	3.00	3690
ORGANIC CAPACITY	ICITY		1950

DATE

18

MOUNT OUT (CLASS II REPLENISHMENT. CLASS IV. CLASS IX AND CLASS X) FOR MI038

	*****	******************	*******	****	****LANFOR SUPPLIES***	LIESAN	*****	**************************	*******
CATEGORY	500	DOS CU FT POUNDS	POUNDS	500	DOS CU FT POUNDS	POUNDS	500	CU FT	DOS CUFT POUNDS
CLASS II* (TYPE I)	v	29.	318.	0.	-69	635.	9	88	953.
CLASS 11W (TYPE 2 NON-CONSUMABLES)	v	•	:	07	•	•		•	•
TUTAL CLASS IIW		29.	318.		- 65	635.		88.	953.
CLASS IV	'n	•	:	01	•	•	13	•	•
CLASS 1XW	v	15.	353.	01	10 1451.	75758.	1.5	1466.	76112.
TOTAL		**	44. 671.		1510. 76393.	76393.		1554.	1554. 77054.

MOUNT OUT (CLASS 111) FOR M1038

### URGANIZATIONAL LOAD

	500	DOS CANS GALLONS.	CAL C	ANS .	PUUNDS	GALLONS POUNDS	RS	DRUMS	GALLONS CU FT POUNDS	GALLONS CU FT	POUNDS	CU FT POJNOS	AGF 500
DIESEL	c	24.		120.	1079.	:	•	35.	1855.	385.	14857.		
MOGAS	S	102.		510.	+136.	•	•	136.	7208.	1496.	51361.		
4	•					:	•	•	•	•	•		
KERUSENE	S	;		20.	176.			÷	159.	33.	1243.		
LUBE	n							:	• 86•	66	*180	:	:
LUBE								:	:	:	:		
CLASS IIIW	v							:	:	•	•	20.	596.
TOTAL		130.		.059	5391.	•	•	183.	9708.	2013.	71661.	20.	. 296.

DATE

MOUNT DUT (CLASS III) FOR MID38

LANDING FORCE SUPPLIES

		***************************************	**************************************	UMSesses	*******	****	**************************************	LK*****	********	0****	AY PACK	**********
CATEGORY	500	DRUMS	GALLONS	GALLONS CUFT POUNDS	POUNDS	500	DOS GALLONS		CU FT POUNDS	. 500	CU FT	DOS . CU FT POUNDS
DIESEL	~	18.	954.	198.	7641.	œ	2735.	367.	19119.			
MOGAS	~	.65	3127.	649.	22290.	•	12190.	1633.	74481.			
đ	N	•	•	•	•	13	:	:	;			
KERUSENE	8	•	318.	•99	2486.	•	208.	28.	1420.			
LUBE (1114)	•	:	756.	154.	6502.					2	•	•
LUBE (111A)	01	•	•	•	•							
CLASS IIIW	2	•	:	•	•					2	39.	1193.
TOTAL		97.	5155.	1067.	38919.		15133.	2028.	95020.		.95	1193.

MOUNT OUT (CLASS VW) FOR MI038

## TOTAL REQUIREMENT = BASIC ALLOWANCE PLUS 15 DOA

# ONGANIZATIONAL LOAD = BASIC ALLOWANCE PLUS 5 DOA

## MOUNT DUT (CLASS VW) FOR M1038

	LANEDR	Sab leafis	SCHEON	•0	•0	,		9.	72500.	.0	30040.	212940.	•0	ċ	. 405.	.0	0.			• 0			11920.	.0	0.	.0	.0	.0	•0	.0	•0	0.	·c	0.0	0.0	.0
	EXCESS		ROUNDS	.0006	558.	716.	758.	96 40.	2067.	6434.	1227.	5927.	184.	154.	148.	22.	12.	40.	.04	*0*		12.	80.	16.	16.	16.	80.	80.	80.	36.	36.	36.	36.	36.	36.	36.
		*******	POUNDS	228.	312.	208.	236.	376.	6979.	791.	1073.	16216.	232.	188.	219.	.64	•1.	47.	47.	47.	27289.	164.	11136.	136.	136.	136.	114.	110.		132.	132.	128.	201.	132.	110.	110.
		.0AD****	CU FT	5.		2.	8.	16.	74.	• 0	26.	378.	12.	8.	3.	3.	1.	2.	2.	2.	556.	5.	449.		3.	3.	3.	3.	3.	3.	3.	3.	;	3.	3.	3.
		**** CAD LOAD ****	PACKAGES	*	:	:	:	:	93.	7.	16.	225.	:	;	3.	:	:	:	:	:		;	192.	:		:	2.	2.	2.	2.	2.	5.	3.	2.	2.	2.
		********	ROUNDS		•009	800	800	16000.	74400.	14000.	26240.	378000.	192.	2000	•099	48.	16.	50.	-09	20.		112.	6144.	64.	64.	. 64	160.	160.	160.	72.	72.	72.	108.	72.	72.	72.
ORGN	LOAD	RORMT	ROUNDS	1000	42.	84.	42.	6360.	72333.	7566.	25013.	372073.	8.	46.	512.	26.	*	10.	10.	10.		1000	6064.	48.	*8*	48.	80.	*0°	80.	36.	36.	36.	72.	36.	36.	36.
	TOTAL	RORMT	ROUNDS	•0006	54.	108.	54.	7080.	147000.	10476.	56280.	590940.	8.	-65	1152.	26.	*	10.	10.	10.		100	18064.	48.	48.	48.	80.	80.	80.	36.	36.	36.	72.	36.	36.	36.
ROUNDS	PER	PACKAGE	HOUNDS	.0000	150.	200.	2000	*000*	800.		1640.				220.	48.	16.	50.	50.	50.		28.	32.						80.						36.	36.
			DESCRIPTION	CORD DETONATING REI			FIRING DEVICE DEMO	FUZE BLASTING TIME		CTG CAL .45 BALL MI	CTG 5.56MM TRACER M	CTG 5.56MM BALL M19	ADAPTER GREN PROJ M	ADAPTER CHEN PROJ M	CTG CAL.50 SPOTTER-	ADAPTER GREN PROJ M	ADAPTER CHEM GREN P		GREN HD ILLUM MKI M	FLARE SURFACE TRIP	GRENADE HAND SMUKE	GRENADE HAND SMK YE	GRENADE HAND SWK RE	SICNAL FLLUM AZC DS	SIGNAL ILLUM AZC DS	SIGNAL ILLUM AZC D	SIGNAL ILLUM GRO RF	SIGNAL ILLUM GRD WH	SIGNAL ILLUM GRD RE	SIGNAL ILLUM GRD WH	SIGNAL ILLUM GRD GR	SMK	SIGNAL SMK GRD GREE			
			21000	0M456A	0M526A	0M627A	OM630A	OM6 70A	0A131	0A475	04058	04071	06803	06806F	0A574	06803A	90890	068060	068060	06806F	TOTAL	06895	01495												01.323	0L324
		90	CLASS	-	-	-	-	-	-	-	-	-	-	_	-	-	-	-	-	-	-	7-11	11-0													11-0

MOUNT DUT (CLASS VW) FOR MI038

ANTIGOTO II II FLORISA			250	:75.	•		27.		••		1346.	882.	1599.	892.			212.	576.	2880.	160.	966			576.			•	
EXCESS LENGTON CAPATED SUBMERS ROUNDS FECTORS			• •	: :	16.		• 01		16.		210.	186.	:	18.	30.	118.	19.	•	•0	•				•			19560.	
SUNUOA	12991.		1916.	3621.	378.	9735.	82.	82.	• *	94.	1060.	848.	17223.	4920.	1016	2288.	2360.	6240.	28037.	5808.	3752	,	92899.	+ 968.	968.		*00*	•00•
**************************************	• • • •		30.	75.	•	239.	.2.	2.	°2	2.	26.	21.	497.	.5.	96.	69	160.	149.	156.	130.	95.		2474.	23.	23.		780.	780.
**************************************		;	24.	71.	•		2.		<b>5</b>		20.	16.	307.	•00	120	***	20.	104.	528.	48.	28.			22.			:	
ROUNDS			216.	213.	144.		32.		32.		1440.	1152.	921.	540.	-041	1320.	300	312.	1584.	- 96	56.			352.			20000-	
LOAD ROAMT ROUNDS		;	216.	212.	128.		22.		16.		1230.	996	920.	522.	173	1202.	281.	312.	1584.	96.	56.			352.			440.	
TUTAL ROAMT ROUNDS		•	576.	588.	128.		-65		•		2826.	2034.	2520.	1422.	272	1205.	512.	888	4464.	256.	152.			928.			• 096	
ROUNDS PER PACKAGE ROUNDS		•	, ,	3.	16.		.91		16.		72.	72.	e e	•	15.	30.	15.	3.	3.		2.			. 61		٠	20000	
DESCRIPTION		***************************************	CTG GOMM SMK MP M30	CTG BINN SMK WP M37	HO AND RIFL		GREN HD SMK HC AN-M		GREN HD INCENDIARY		M406	CTG 40MM HE M397 W/	ROCKET HEAT 3.5INCH	CTG GOMM ILLUM MB3A	BOCKET HEAT WALCHD	GREN HAND FRAG M67	RUCKET HEAT W/LCHR	BIMM ILLUM M3		CTG 106MM HE. AT M3	CTG 106MM APERS-T -			FUZE PHOXIMITY. M53			CAP BLASTING NUNE	
31000	TOTAL		03030	00276	06937	TOTAL	11-E 06930	TOTAL	00690	TOTAL	89580	08569	009H0	08627	00005 0H557A	06881	0H557	0C226	00256	00000	00000		TOTAL	0N4 02	TOTAL		VIII OMI 31A	TOTAL
55	11-C TOTAL		0-11			11-0 TOTAL	11-6	11-E TOTAL	00650 5-11	11-3 TOTAL					2.2			^			. 2		2	;			1111	VIII TOTAL

DATE 2

M1038	
FOR	
3	
(CLASS	
DOT	
MOUNT	

	20	1.5	505	34.		•	32.	10.		•		
	. ANE	Supp	foa									
	EXCESS LANFOR	CARRIED SUPPLIES	POUNDS			167.	32.	•		712.		
		******	POUNDS	1824.	1824.	•00•	.095	1250.	2210.	225.	225.	
		****** CAO.	CU FT	64. 32. 43. 1824.	<b>43.</b>	<u>:</u>	13.	200.	227.		00	
		****BRGN I	PACKAGES	32.			16.			:		
		*******				•00•	256.	25.		1200-		
ORGN	LOAD	RORMT	ROUNDS	57.		233.	224.	25.		488.		
	TOTAL	ROSMT	ROUNDS	•66		300.	238.	35.		984.		
RUUNDS	PFR	PACKAGE	ROUNDS	. 8		50.	16.	2.		300.		
			DESCRIPTION	CHG ASSEMBLY DEMD M		GREN HD RIOT CSI M2	GREN HD RIOT CONTRO	CHEM AGENT RIOT CUN		IGNITER TIME BLASTI 300.		
			S D001C	. VISINO 8-X	X-8 TUTAL		1-8 06963		I-B TOTAL	1-0 04766A	1-D TOTAL	
			ASS	×	*	-	-	-	1	1	1	

TOTAL

REPLENISHMENT RATE (BY DAYS) OF CLASSES I. II. IV. VI. VIIINDN SQUARF), VIII. IX AND X FOR MID38

															SO FT	÷		
POUNDS	7380.	4664.	1995.	.19	20101.	. 62.	•	290.	•	•	.36	.11.	5003.	•	25931.		11746.	10762.
CU FT	147.	143.	243.	ř	536.	;	:	23.	•	:	, ,	'n	95.	•	•699	13.	246.	246.
CATEGORY	CLASS I (A RATIONS)	CLASS I (B HATIONS)	CLASS I (MCI)	CLASS I (TRIOXANE)	TOTAL CLASS I	CLASS IIW	CLASS IV	CLASS VI (RAT SUPP)	CLASS VI (OTHER)	CLASS VII (NON-SQUARE)	CLASS VIII	CLASS IXW (UNIT)	CLASS IXW (SUPPORTING)	CLASS X	TOTAL	CLASS VIIW (SOUARE)	WATER(I GAL/MAN/DAY) 5 GAL CANS	WATER(1 GAL/MAN/DAY) 2.5 GAL CANS

\*\* THE REPLENISHMENT RATE IS FOR I DAYS

REPLENISHMENT RATE (PER DAY) OF CLASS III FOR MI038

CU FT POUNDS					•		119.	1119.
PACK							:	:
**084						•		
POUNDS	2579.	9359.	•	229.				259. 12166.
*******BULK******* CU FT POUNDS	.6.	205.	•	:				259.
POUNDS	2955.	10918.	•	262.	586.	•	•	14721.
****55 GAL DRUMS******* DRUMS CU FT POUNDS		318.	•		:	•	•	415.
*******55 GAL DRUMS******* DHUMS CU FT POUNDS		29.	•	:	:	•	•	38.
SALLONS	369.	1532.	•	33.	•89•	:	•	2002
CATEGURY	DIESEL	MOGAS	4	KEROSENE	CLASS IIIW LUBE	CLASS IIIA LUBE	CLASS IIIW (MARCORP)	TOTAL

THE REPLENISHMENT QUANTITIES HAVE BEEN EXPRESSED IN BOTH ORUMS AND BULK TO PROVIDE DATA FOR EITHER MODE OF TRANSPORTATION

\*

DATE

4.67 111.09 3.95 17.24 0.00 3.20 2.13 1.13 2.6.67 6.67 6.67 6.67 6.83 8.80 17.10 00000 79.20 28.80 205.20 145.50 200.00 4666-67 PER PACKAGE ROUNDS 5000.00 2.00 300.00 72.00 3.00 3.00 800.00 200.00 4000.00 4000.00 150.00 CTG 40MM HE M406 W/FZ PD CTG 40MM HE M406 W/FZ PD CTG 40MM HE M397 W/FZ PD ROCKET HEAT 3.5INCH M28A CAP BLASTING NUN-ELEC S FIRING DEVICE DEMU MI PU FUZE BLASTING TIME M700 CTG 60MM ILLUM M83A3 W/F CURD DETONATING REINF PL CTG 7.624M LINKED 4 BALL CHG ASSEMBLY DEMU M183 FIRING DEVICE DEMU MI FIRING DEVICE DEMO MS DESCRIPTION 1x-d x1-D 2 2 2 2 1 1111 CLASS 21000 A161M0 UM456A OMESEA 0M627A A0E 3MO ATSTMO 0M766A OM670A 08569 08600 08602 99590 0A131 08627

.31

162.49 7.13 88.33 58.30

360.00 437.73 721.60

188.80

CTG GOMM SMK WP M302 W/F CTG 60MM HE M49A2E1 W/FZ

0-11

CTG CAL .45 BALL M1911

8.22

-		CTG 5.56MM TRACER M196	1640.00	1876.00	1.14	1.88	76.73
-		CTG 5.50MM BALL MI93 10	1680.00	13132.00	7.82	13.13	563.36
-	>	RUCKET HEAT W/LCHR M72 S	15.00	9.88	99.	5.27	77.72
-		ADAPTER GREN PROJ MIAI W	48.00	10.	• 00	00.	10.
-		ADAPTER CHEM PROJ MZAI	20.00	1.28	.03	• 05	1.20
-	>	GREN HAND FRAG M67 W/SAF	30.00	•50	10.	• 02	.51
-	11-0	GREN HD ILLUM MK1 MOD-2	28.00	00.	00.	00.	10.
×	8-1x	GREN HD RIOT CSI M25A2	20.00	6.67	.13	.24	4.67
×	8-IX	GREN HD RIUT CUNTROL CS	16.00	6.40	04.	• 32	14.00
-	2	ROCKET HEAT W/LCHR M72 S	15.00	15.50	1.03	8.26	121.93
-	7-11	FLARE SURFACE TRIP M49	32.00	00.009	18.75	43.80	1087.50
×	8-1×	CHEM AGENT RIOT CONTROL	2.00	1.00	• 20	8.00	20.00
-	1	CTG BIMM ILLUM M301A3 W/	3.00	52.80	17.60	25.19	1056.00
-	^1	CTG BIMM HE M374 W/FZ PD	3.00	252.00	84.00	120.20	4460.40
-	0-11	CTG BIMM SMK WP M375 W/F	3.00	33.60	11.20	11.76	571.20
>	_	FUZE PROXIMITY. M532	16.00	50.40	3.15	3.33	138.60
-		CTG CAL.50 SPOTTER-TRACE	220.00	64.00	•29	•26	21.24
-	>	CTG 106MM HE. AT M344AI	2.00	16.00	8.00	21.68	00.890
-	>	CTG 106MM HEP-T. M346. W	2.00	38.40	19.20	49.73	2323.20
-	>	CTG 106MM APERS-T -BEEHI	2.00	09.6	4.80	16.32	643.20
-		ADAPTER GREN PROJ MIAL W	49.00	00.	00.	.00	00.
-		ADAPTER CHEM GREN PROJ M	16.00	00.	00.	00.	00.
-		ADAPTER CHEM GREN PROJ M	20.00	00.	00.	00.	00.
-		ADAPTER CHEM GREN PROJ M	20.00	00.	00.	00.	00.
-		ADAPTER CHEM GREN PROJ M	20.00	00.	00.	00.	00.
-	7-11	GREN HD INCENDIARY TH-3	16.00	00.	00.	00.	10.
-	11-E	GREN HD SMK HC AN-MB	16.00	2.80	.17	•11	7.17
-	0-11	GREN HD ANG RIFLE SMK WP	16.00	• 05	00.	90.	• 05

0G803A

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0690850

16650

36H06C 0G806E

90850

0G806F

96890 06963

06924 0H557

96470 0K768 0C226 00256 0C276 04574 05930

0N402

0H557A

06803

0A475

0A068

0A071

08990

08632

REPLENISHMENT SUSTAINING RATE (PER DAY) OF CLASS VW FOR MI038

		POUNDS	-05	•03	.05	000	00.	00.	000	00.	00.	• 02	00.	• 00	00.	30.36 16581.17
		CU FT	00.	00.	00.	• 00	00.	.00	.00	.00	00.	• 00	00.	00.	• 00	430.36
		PACKAGES	00.	00.	00.	000	00.	• 00	00.	00.	00.	00.	• 00	00.	00.	
		ROUNDS	10.	10.	.01	00.	00.	• • •	00.	000	00.	10.	.00.	000	••	
ROUNDS	PACKAGE	ROUNDS	16.00	16.00	16.00	80.00	80.00	80.00	36.00	36.00	36.00	36.00	36.00	36.00	36.00	
	93	CLASS DESCRIPTION	11-C GRENADE MAND SMUKE GREEN	GRENADE	11-C GRENADE HAND SMK RED MIS	SICNAL	SIGNAL	11-C SIGNAL ILLUM AZC DC GRE	SIGNAL	SIGNAL	SIGNAL	SIGNAL	11-C SIGNAL ILLUM GRD GREEN S	11-C SIGNAL SMK GRD RED PARAC	11-C SIGNAL SMK GRD GREEN PAR	
		21000	04690	06945	00000	01.225	01.226	01227	0L306	01307	01311	01312	01314	01.323	0L324	TOTAL

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21000	CLASS	DESCRIPTION	SCHOOL
OMIJIA	1111		180.
OM450A .		CORD DETUNATING HEINF PLIG-FILM WRAPPED	.0009
OMEZEA	-	FIRING DEVICE DEMO MI	36.
ONG27A		FIRING DEVICE DEMO MS	72.
OM6.30A	-	FIRING DEVICE DEMO MI PULL	36.
OMSTOA	-	FUZE BLASTING TIME M700	.0009
OM757A	1x-8	CHG ASSEMBLY DEMU MIB3	36.
OM766A	0-1×	IGNITER TIME BLASTING FZ M60	240.
08568	>1	CTG 40MM HF M406 W/FZ PD. M551	432.
08569	11.	PD.	432.
009Н0	2	RUCKET HEAT 3.5INCH M2BA2 ROCKET HEA	120.
04602	11-0	ROCKET SMK WP 3.5INCH M30	*0*
0A131		CTG 7.62MM LINKED 4 BALL M80-ITRACER M62	35000.
08627	2	CTG 60MM ILLUM M83A3 W/FZ TIMEM65A1	72.
01630	0-11	CTG 60MM SMK WP M302 W/FZ PD M52781	36.
08632	2	CTG GOMM HE M49A2E1 W/FZ PD M525	252.
04475		CTG CAL .45 BALL MI911	61111.
04068		CTG 5.56MM TRACER MI96 F/MARDIV.	9380.
04071	1.	CTG 5.56MM BALL MI93 10 RD F/MARDIV.	262640.
0H557A	^1	ROCKET HEAT W/LCHR M72 SERIES M72 SERIS	123.
06803	-	ADAPTER GREN PROJ MIAI W/LAUNCHING CLIPS	· a
0G806F	-	ADAPTER CHEM PROJ MZAI W/CLIPS	*0*
06881	2	GREN HAND FRAG M67 W/SAFETY CLIP	1200.
06895	11-0	GREN HD ILLUM MK1 MDD-2	1000
06924	X1-B	GREN HD RIOT CSI M25A2	2000
06963	x1-8	GREN HD RIDT CONTROL CS MIA3	192.
0H557	2	HOCKET HEAT W/LCHR M72 SERIES M72 SERIES	165.
01495	11-C	FLARE SURFACE TRIP M49	. 49
0K768	8-1×	CHEM AGENT RIOT CONTROL CS1	20.
002226	^1	CTG BIMM ILLUM M301A3 W/FZ TIME M84A1	24.
00256	2	CTG BIMM HE M374 W/FZ PD M524A5/M52	144.
00276	11-D	CTG 31 MM SMK WP M375 W/FZ PD M524A5/	24.
0N402	11	FUZE PROXIMITY, M532	. 49
0A574	-	CTG CAL.50 SPOTTER-TRACER. M48A1	192.
06650	2	CTG 106MM HE. AT M344A! W/FZ PI-BD M509	16.
00651	^1		24.
00000	2	CTG 106MM APERS-T -BEEHIVE- W/FZ MT XMS9	8.
06803A	-	GREN PROJ	26.
06806	1	GREN	*
06806C	-	CHEM GREN	10.
068060	-	ADAPTER CHEM GREN PROJ MZAI W/CLIPS	10.
0G806E	-		10.
00690	11-3	GREN HD INCENDIARY TH-3 AN-NIA	16.
06930	11-E	SMK	;
06937	11-0	AND A	128.
06940	11-0	HAND	48.
06945	11-0	GRENADE HAND SMK YELLOW MIS	48.

DESCRIPTION

C GRENADE HAND SMK RED MIR

C SIGNAL ILLUM A/C DS RED-RED AN-M37A2

C SIGNAL ILLUM A/C DS VELLOW-VELLOW AN-M39A

C SIGNAL ILLUM A/C DS GREEN-GREEN AN-M39A

C SIGNAL ILLUM GRD RED SC MIS9

C SIGNAL ILLUM GRD RED SC MIS9

C SIGNAL ILLUM GRD RED SC MI25

C SIGNAL ILLUM GRD RED SC MI25

C SIGNAL SMK GRD RED PARACHUTE MI29

-----

0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00

CLASS

DODIC

B-41

DATE

## MOUNT OUT (REPLENISHMENT) OF MAJOR EQUIPMENT FOR MI038

#### SQUARE LOADED EQUIPMENT

CATEGONY	CONTRUL NUMBER		2	DESCRIPTION	SESSESSENDONT OUT REQUIREMENTS SESSES QUANTITY SO FT CU FT POUNDS	T OUT RE	CU FT	9	DESN LA	LANKED SJOUTES
CLASS VIIW										
	A1900	02474A		RADIO SET. AN/MR		•	•	•		•
	A1910	02903A		RADIO SET. AN/MR	•	•	•	.0	•0	
	A1920	04600A		RADIO SET. ANIM		•0	•0	• 0	0.0	.0
	A2192	07272A		RADIO TERMINAL		•	•	•	•0	• 6
	00840	044698		TRAILER. AMPHIB		•	•	•0	0.0	.0
	01020	05939A		TRUCK, CARGO. 1	•0	•	•	•0	•	• 0
	01100	01118E		TRUCK. PLATFORM		•	•	•	• 0	.0
	01160	04751A		TRUCK. UTILITY.	•	••	.0	•	• 0	.0
	E1480	033288		RIFLE, 106MM. M		•	•	•	• 0	
CLASS VIIW (TYPE 3)										
TOTAL CLASS VITY						•	•	•		
Page LOAD						•	•	••		
LANFOR SUPPLIES						•	•	•		

MOUNT DUT (REPLENISHMENT) OF MAJOR EQUIPMENT FOR M1038

#### NON-SQUARE LOADED EQUIPMENT

		CONTROL NUMBER	α			DOM******	**************************************		OPGN LANFOR
### ### ##############################	CATEGORY	. OR FSN		<b>G</b>	DESCRIPTION	QUANTITY	SO FT CU FT	POUNDS	
### ### ### ### ######################	CLASS VIIW								
### ### ##############################	1341 34111	A1083	750750		NOISIV THEIN				•
ACCESSORY KIT,   ACCE		£1060	04706A		MORTAR. INFAN				
A MA328 06692A DETECTING SET 1. 1. 12. 12. 12. 14.94 METASCOPE, ASSE 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		A0005	04177A		ACCESSORY KIT		•		
A0490 04704B METECTING SET. 1. 12. A1082 034494 METASOPE, ASSE 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		A0328	06692A		CONVERTER FRE	•	•		
A MOGREZ  B MOGREZ  A MOGREZ  B MOGR		0640V	047048		DETECTING SET		•	-	
NICHT VISION SI 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		A0922	03449A		METASCOPE. AS		••		
A1927   07098A   NIGHT VISION ST   0.   0.   0.     A1420   05867A   RADIO SET. AN/P   0.   0.   0.     A2010   03815A   RADIO SET. AN/P   0.   0.   0.     A2010   03815A   RADIO SET. AN/P   0.   0.   0.     A2020   03815A   RADIO SET. AN/P   0.   0.     A2030   05916A   RADIO SET. AN/P   0.   0.     A2050   05916A   RADIO SET. AN/P   0.   0.     A2184   07277A   RADIO SET. AN/P   0.   0.     A2240   0566A   RECEIVING SET   0.   0.     A2250   05916A   RADIO TEMINAL   0.   0.     A2260   05916A   RADIO TEMINAL   0.   0.     A2260   05916A   RADIO TEMINAL   0.   0.     B1360   0593A   RADIO TEMINAL   0.   0.     E1090   05919A   000519A   000519A   00051A   0.     E1090   05919A   00051A   00051A   0.     E1090   02193A   DUBLIC ADDRESS   0.   0.     H2363   02243A   TELEPHONE SET,   0.   0.     A2450   06919A   00051A   00051A   0.     A2460   06919A   00051A   00051A   0.     A2460   06919A   00051A   00051A   0.     A2460   06919A   00051A   0.     A2460   00051A   0.		A1086			NIGHT VISION		•		
A1420 05867A RADAR SET ANYPP 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		A1087	07098A		VISION		•		
A1730   O4616A   RADIO SET.CONTR   O.		A1420	05867A				•		
## ## ## ## ## ## ## ## ## ## ## ## ##		A1730	04616A				•		
A2020 05817A RADIO SET AN/P 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		A2010	03816A				•		
### ### ### ### ### ### ### ### ### ##		A2020	03817A				•0		
### RADIO SET, AN/P 1. 1. 20.  ### A2150 06596A RADIO SET, AN/P 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		A2040	06828A				••		
## ## ## ## ## ## ## ## ## ## ## ## ##		A2050	05916A				•		
### 07277A RADIO TERMINAL 0. 0. 0. 0. 42240 05266A RECEIVING SET R 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	I	A2150	04622A		RADIO SET. AN	>	•0		
## RECEIVING SET R 0. 0. 0. 0. 0. 4240	3-	A2184	07277A		RADIO TERMINAL		•0		
A26480 00276A SWITCHBOARD, TE 0. 0. 0. 42660 00061A TELETYPE WRITER 0. 0. 0. 0. 0. 42660 00061A TERMINAL, TELEG 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	4:	A2240	05866A		RECEIVING SET	α	•0		
## ## ## ## ## ## ## ## ## ## ## ## ##	3	A2480	00276A		SWITCHBOARD.		•0		
## ## ## ## ## ## ## ## ## ## ## ## ##		A2660	0000 VI		TELETYPEWRITER		••		
### MOTOR GENERATOR 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		A2685	06963A		TERMINAL. TELE		•0		
E0180 00476A CIRCLE.AIMING.M 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		B1360	03965A		MOTOR GENERATO		•0		•
E1260 00519A MORTAR,INF,81MM 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		E0180	00476A		CIRCLE. AIMING		••		
E1260 02193A 00UADRANT, FIRE 0. 0. 0. 0. 1 E1900 00591A TELESCOPE, OBSE 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		E1090	00519A		MORTAR, INF. 81A		•		
E1900 00591A TELESCOPE, OBSE 0. 0. 0. 142357 04626A POWER SUPPLY, P 0. 0. 0. 0. 0. 142363 D2543A PUBLIC ADDRESS 0. 0. 0. 0. 142443 025336A TELEPHONE SET, 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		E1260 .	02193A		OUADRANT. FIRE		•		
H2367 04626A POWER SUPPLY, P 0. 0. 0. 12363 02543A PUBLIC ADDRESS 0. 0. 0. 0. 12443 02535A TELEPHONE SET. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		E1900	A16500		TELESCOPE, OB		•		
H2443 02543A PUBLIC ADDRESS 0. 0. 0. H2443 02336A TELEPHONE SET. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.		H2357	04626A		POWER SUPPLY.		•		
H2443 02336A TELEPHONE SET. 0. 0. 0.		H2363	02543A		PUBLIC ADDRES		•		
		H2443	02336A		TELEPHONE SET		•		
ř č	CLASS VIIW (TYPE 3)								
·	TOTAL CLASS VIIW						ř		
	ORGN LOAD						•		

ASSAULT ECHELON REPLENISHMENT CARGO

(CLASSES 1. 11. 1V. VI. VII NON-SQUARE. VIII AND IX)
CARRIED BY FOLLOW ON ECHELON FOR MID38

CATEGORY
I (B RATIONS)
CLASS ( (TRIOXANE)
CLASS VI (RAT SUPP)
CLASS VIIW (NON-SOUARE)
IXW (SUPPORTING)
CLASS VIIW (SQUARE)

ASSAULT ECHELON CLASS 111 CARRIED BY THE FOLLOW ON ECHELON FOR M1038

			OBINSER	******	*********	PRIN KARBS	******	SECTION OF THE PROPERTY IN THE PROPERTY OF THE	AGESA
900		GALLONS	DRUMS GALLONS CUFT POUNDS	POUNDS	GALLONS	CU FT POUNDS	POUNDS	CU FT POUNDS	POUNDS
•	. 0	•	•	•	16601.	2225.	116044.		
•		•	•	•	68926.	9236.	421141.		
•	.6 0.	:	•	•	•	•	0.		
•	.0	•	:	•	1507.	202.	10290.		
	61.	3294.	671.	28328.				•	•
	• 0 • 51	•	:	•				<u> </u>	
	• 0	:	:	•				176.	5367.
	.19	61. 3294.	671.	28328.	87034.	11663.	11663. 547474.	176.	5367.

PAGE

ASSAULT ECHELUN CLASS VW CARRIED BY THE FOLLOW ON ECHELON FOR M1038

286 23638. 23638. 20975. 303.	60130.	21600. 9204. 26724. 57528.	357.	2928. 89760. 339249. 3498.	48960. 210276. 43560. 104544. 28944.	6534.
CU FT 1. 252. 103. 722.	2628.	644. 192. 550.	: :	2592. 2592. 522. 807.	2238. 734.	157.
PACKAGES 0. 315. 63. 430.	1125.	400. 156. 524.	•	683. 1600. 601.	3960 3960 360 215	148.
ROUNDS P 2000. 252000. 722250 5370. 2880.	36000	1404.	139•	5994. 3978. 3726. 9612.	11880 720 1728 432	2376.
ROUNDS PFR PACKAGE RUUNDS 4000. 1640. 1640. 2000.	32.	m o m	•	22.69.32	ก็ตัดนั้นนั้	16.
CORD DETONATING REINF PLIO-FIL CTG 7.62MM LINKED A BALL M80-1 CTG 5.56MM TRCER M196 CTG 5.56MM WALL M193 10 RD CTG CAL .45 WALL M1911 CTG CAL .50 SPOTTER-TRACER.	FLARE SURFACE TRIP M49	ROCKET SMK WP 3.5INCH M30 CTG 60MM SMK WP M302 W/FZ PD CTG 81MM SMK WP M375 W/FZ	GREN HD SMK HC AN-MB	CTG 40MM HE M406 W/FZ PD. M551 CTG 40MM HE M397 W/FZ PD. M536 ROCKET HEAT 3.5INCH M28A2 CTG 60MM ILLUM M83A3 W/FZ TIME CTG 60MM HE M40A2E1 W/FZ PD ROCKET HEAT W/LUM M72 SERIES	CTG 81MM HE M374 W/FZ PD CTG 106MM HE, AT M344A1 W/FZ CTG 106MM HEP-T, M346, W/FZ CTG 106MM APERS-T -BEEHIVE-W/	FUZE PROXIMITY. M532
D001C 04456A 0A131 0A034 0A071 0A475	1 TOTAL 11-C 01495 11-C TOTAL	11-D 0H602 11-D 0B630 11-D 0C276 11-D T07AL	-	08568 08569 08627 08627 08532	00226 00256 00650 00651 00660	0N402
CLASS	1 21	11-0	3-11-E	222222	22222 2	5

ASSAULT ECHELON CLASS VW CARRIED BY THE FOLLOW ON ECHELON FOR MI038

CHG ASSEMBLY DEMO MIB3 2. 255. 127. 171. 7267.  GREN HD RIOT CSI M25A2 50. 200. 4. 7. 200.  GREN HD RIOT CONTROL CS MIA3 16. 288. 18. 14. 630.  CHEM AGENT RIOT CONTROL CS M. 5. 45. 9. 360. 2250.  IGNITER TIME BLASTING FZ M60 300. 1668. 6. 11. 313.		PER PACKAGE					
2. 255. 127. 171. 50. 200. 4. 7. 16. 288. 18. 14. 5. 45. 9. 360. 382. 300. 1668. 6. 11.	DESCRIPTION	ROUNDS	ROUNDS	PACKAGES	CU FT	POUNDS	
2. 255. 127. 171. 50. 200. 4. 7. 16. 288. 18. 14. 5. 45. 9. 360. 382. 300. 1668. 6. 11.					157.	6534.	
50. 200. 4. 7. 16. 288. 18. 14. 5. 45. 9. 360. 300. 1668. 6. 11.	CHG ASSEMBLY DEMO MIB3	5.	255.	127.	171.	7267.	
50. 200. 4. 7. 16. 288. 18. 14. 5. 45. 9. 360. 300. 1668. 6. 11.					1711.	7267.	
300. 1668. 6. 11.	GREN HD RIOT CSI M25A2	20.	200.		2	200-	
300. 1668. 6. 111.	CHEM AGENT RIOT CONTROL CSI		45.		360.	2250.	
300. 1668. 6. 111.	*				382.	3080.	
	IGNITER TIME BLASTING FZ M60	300	1668.	ċ	:	313.	
					:	313.	
					301.10		

ASSAULT ECHELON REPLENISHMENT CLASS VII(SQUARE LOADED) CARRIED BY THE FOLLOW ON ECHELON FOR MI038

	NUMBER					
CATEGORY	OR FSN	0	DESCRIPTION	SQ FT		CO FT POUNDS
CLASS VIII.						
	41900	02474A	RADIO SET. AN/MRG-83, TRK MTD	•	•0	.0
	A1910	02903A	RADIO SET.AN/MRC-87.TRK MTD	•	•	.0
	A1920	04660A	RADIO SET, AN/MRC-109, MTD IN	•	•	0
	A2182	07272A	RADIO TERMINAL SET. AN/MRC-134	•	••	.0
	00840	044698	TRAILER. AMPHIB CARGO, 1/4T. 2	• 0	.0	• 0
	01020	VORA50	TRUCK. CARGU. 1-1/41. 6X6. M56	0.0	.0	0.0
	01100	01118E	TRUCK. PLATFURM. UTILITY. 1/21	18.	42.	.600
	01160	04751A	TRUCK. UTILITY. 1/4T MISIAI-	.19	327.	2400.
	E1480	033288	RIFLE. 106MM, M40AIC, W/E -MT	45.	135.	450.
TOTAL CLASS VIIW				124.	504.	3720.

S I (MCI)  S II (INDIVIDUAL WEAPONS)  S II (CREW SERVED WEAPONS)  S II (ORGANIZATIONAL EQUIPMENT)  S VII (CREW SERVED WEAPONS)  S VII (CREW SERVED WEAPONS)  O  S VII (ORGANIZATIONAL EQUIPMENT)  O  S VII (ORGANIZATIONAL EQUIPMENT)  O	POUNDS	7995.	10083.	840.	25081.	•	•	
CATEGORY  S I (MCI)  S II (INDIVIDUAL WEAPONS)  S II (CREW SERVED WEAPONS)  S II (CREW SERVED WEAPONS)  S VII (CREW SERVED WEAPONS)  S VII (CREW SERVED WEAPONS)	CU F1	243.	579.	45.	1932.	:	•	-
CLAS CLAS CLAS CLAS	CATEGORY	CLASS 1 (MCI)	CLASS II (INDIVIDUAL WEAPONS)	CLASS II (CREW SERVED WEAPONS)	CLASS II (ORGANIZATIONAL EQUIPMENT)	CLASS VII (CREW SERVED WEAPONS)	CLASS VII (ORGANIZATIONAL EQUIPMENT)	TOTAL

 I TV ****		*0*	324.	•	•	•	:	•	•	•	•	26500.	•	•	•	:	9272.	•	•	•	•	•	36500.
****CAPACITY*****	3	•	•	•	•	•	•	:	•	•	•	1029.	•	•	•	•	552.	•	•	•	•	•	1587.
SONNOG	2000	8399.	36329.	•	•	•	:	•	•	:	•	26500.	•	:	•	•	11340.	•	•	•	:	•	82568.
Cu FT	3	255.	2576.	:	•	•	:	:	•	•	•	715.	•	•	•	•	1152.	:	•	:	•	•	4698.
50 61	3															•							•
SAL.	1			•	:	•	:	:	•	•													
CATEGORY				11 DIESEL	II MOGAS	ar 11	CLASS III KEROSENE	CLASS IIIW LUBE	CLASS IIIA LUBE	CLASS IIIW (MARCORP)	>	3	•	VZ		CLASS VII NML(SQ)	OTHER CLASS VII (NUN-SQUARE)		X	Y.	, xZ		
		CLASS I	CLASS 1	CLASS 111	CLASS 111	CLASS 111	CLASS 1	CLASS 1	CLASS 1	CLASS 1	CLASS IV	CLASS V	CL'ASS VA	CLASS V	CLASS VI	CLASS V	CNUN-S	CLASS VIII	CLASS IXW	CLASS 1XA	CLASS 1X2	CLASS X	TOTAL

POUNDS	****	82568.	7500.	1329236.
CU FT	1587.	4698.	•	66865.
	MOBILE LOAD CAPACITY	MUBILE LOADED CARGO	UNUSED CAPACITY	NON-MUBILE LOADED CARGO

GENERAL CARGO FOR M1038

CATEGORY	GAL	SO FT CU FT	F POUNDS
1 884 13			
		00.00	
CLASS 11		22462.	. 322038.
CLASS 111 DIESEL	5664.	. 416	42696.
CLASS III MOGAS	23035.	3880.	. 152288.
CLASS 111 JP	:	•	:
CLASS III KEROSENE	705.	131.	. 5325.
CLASS IIIW LUBE	1242.	253.	10681.
CLASS IIIA LUBE	•	•	:
CLASS IIIW (MARCORP)	•	-65	. 1789.
CLASS IV		15.	245.
CLASS VW		9766.	333442.
CLASS VA		•	•
CLASS VZ		•	•
CLASS VI		349.	8856.
CLASS VII NON-SQUARE		•696	. 8377.
CLASS VIII		333.	. 5412.
CLASS TXW		2931.	152223.
CLASS IXA		ò	•
CLASS 1XZ		•	•
CLASS X		•	•
TOTAL		45558.	1155822.
CLASS VII SQUARE		4717. 21307.	. 173414.

READ AN INPUT CARD. CARD IS...ASSAULT ECHELON COMPONENT = 1 M8937X 3PNAA

TOTAL FOR COMPONENT						OFFICER FNI ISTED
TOTAL FO						c
	NOT EXIST.	DUES NOT EXIST.	NOT EXIST.	NUT EXIST.	NOT EXIST.	PERSONNEL
UNIT NAME						
CONSISTING OF	SYSTEM NAME C6682	SYSTEM NAME C2330	SYSTEM NAME C3255	SYSTEM NAME C3340	SYSTEM NAME C3430	

M8937X

TYO DESIGNATOR

COMPONENT OF

NAME

61

DATE 2

TOTAL 237

188

MARCORP

241

161

20

GRAND TOTAL

B-53

### INITIAL ISSUE OF MAJOR EQUIPMENT FOR MA937X

#### SQUARE LUADED EQUIPMENT

;			6	2002	160	5000	. 00001	50000		000
•				7		2	101	2		20000
			.0	.0	.25	.0	.544.	. 404.		. 404
			CN	CN	CN	C.N	202			
CES NML			2680.	2650.	1140.	•60096	21840.	37910.		37910.
\$9 FT			76.	125.	92.	244.	495.	1033.		1033.
710			:		2.	*				
NO I			SET. ELEC	AILER. 3	PHIB CARG	1TY - 1/4T	ITY - 1-17			
DESCRIPTION			FLOODLIGHT SET. ELEC	CHASSIS, TRAILER, 3	TRAILER. AMPHIB CARG	TRUCK. UTILITY. 1/4T	TRUCK. UTILITY. 1-1/			
2										
			00903K	05945A	044698	C4751A	07064A			
CNTRUL NUMBER OR FSN										
CONTRUL NUMBER GR FSN			80630	00000	00840	0110	98110			
*	ASS VIII	• 111 · C						TOTAL	S VIIW	* 11 × S
CATEGORY	MEADONS(CLASS VIIM)	CINEW CLASS VIII						CLASS VIIN TOTAL	CTHER CLASS VIIW (TZE TYPE 3)	TOTAL CLASS VIIW

# INITIAL ISSUE PLUS MUUNT JUT (90 DAYS) OF MAJOH EQUIPMENT FOR ME937X

#### SOUARE LUADED EQUIPMENT

			ממשים המשפה המשפה						
	CONTHUL					***********	:	*****************	
CATEGORY	UR FSN	9	DESCRIPTION	017	SO FT	1 155 RML		00	
CVIOA AND VSTOL									
	3CH46Fx		CH46F	18.	12222.	262600.	2	15555.	100001
CIHER CLASS VIIA	•								
	MMF.CN1		MMF. COMNAV NO 1	:	160.	4500.	CN	0.0	•
	MMF . CN2		MMF.COMNAV NO 2	:	160.	4500.	ON	• 0	¢ .
	MMF.EL1		MMF.ELECTRICAL NO 1	:	160.	4500.	NG	.0	c
	MMF . EL2 .		MMF.ELECTRICAL NO 2	:	160.	4500.	CN	•	0
	17300750627		ADAPTER-FWD TRANSMIS	2.	48.	350.	NC		,
	17300750629		ADAPTER-VERTICAL SHA	:	27.	280.	00	•	c
	17301121024		ADAPTER-XMSN AND MIX	:	2A.	300.	CN	• 0	•
	17302949883		MAINTENANCE PLATFORM	3.	135.	2160.	ON	0.0	c
	43107280206		COMPRESSOR-AIR 100 P	8	118.	7600.	ON	• 0	0
	43107987641		COMPRESSOR-AIR PORTA	:	· S	273.	CN	• 0	•
В	49401642173		BLAST CLEANING MACHI	3.	21.	525.	CN	• 0 ·	c
-5	49407821630		CLEANING MACHINE-AIR	-	32.	1000	ON	• 0	c
5	61157826740		MOBILE ELECTRIC POWE	:	45.	.0099	ON	.0	<
	17400623100		TRAILEN-ENGINE TRANS	:	36.	800.	CN	• 0	•
	49401312518		CLEANER-STEAM PRESSU	-	13.	500.	NO.	• 0	•
	66355809892		PORTABLE MAGNETIC IN	:	8.	. 646	CN	• 0	c
LANE G CRAFT AND FLOATING EQUIPMENT	IND								
GTHEN CLASS VIIZ									
TOTAL					13378.	321940.	-	15552.	100800
TOTAL (-) A/C. L/C FLUATING ECUIPMENT	L/C AND				1156.	39340.		•	c

CATE

INITIAL ISSUE OF MAJOR EQUIPMENT FOR MAGGIX

#### NON-SQUARE LUADED EQUIPMENT

547		182.	210.
######################################		::	20
¥10		::	
DESCRIPTION		INTERCOMMUNICATION S SWITCHBOARD. TELEPHO	
9			
		00042A 00276A	
CONTRUL NUMBER UN FSN		A0870 A2480	
CATEGURY	ONGANIZATIONAL WPNS	OTHER CLASS VIIM	TUTAL NON-SQUARE

PAGE

61

INITIAL ISSUE PLUS MOUNT OUT (90 DAYS) OF MAJOR EQUIPMENT FOR M8937X

EQUIPMENT
EQU
LOADED
NON-SQUARE
ž

CU FT LAS	912.	2.	36.	. 58.	144.	-	148.	1629.	130.	+0+
CU FT	150.	2.	12.	.5	•	:	8.	22.	.6	3.
710	. 2	2.	2.	2.	. 2.	:	-	2.	1.	-
DESCRIPTION	CRANE-MAINTENANCE	ANALYZER-ATTITUDE	INSPECTION SET-PROPE	TEST DEVICE-DE-ICING	TEST SET RADIO	TEST TRAILER ASSY-	TEST SET RADAR ALTIM	TEST SET RADIO	RADAR TEST SET	TEST HARNESS-RADAR
2										
CONTROL NUMBER OR FSN	17307577232	49200978842	49201344689	49209563772	66250577453	49201653573	66250633271	66251337853	60252042249	66254848667
CATEGORY										

TUTAL NON-SQUARE

CLASS VIIZ

3081.

217.

INITIAL ISSUE OF SECUNDARY EQUIPMENT AND SUPPLIES FOR M8937X

POUNDS	52105.	52105.	•	52105.
Cu FT	3752.	3752.	•0	3752.
CATEGORY	CLASS IIW (TVPE 1)	TUTAL CLASS ITW	TUTAL CLASS IV	FUTAL INITIAL ISSUE

\* NUN-CONSUMABLES UNLY

SATE

CU FT POUNDS

CATEGORY

CLASS IIA CLASS 1XA TOTAL

38663. 1036104.

2490. 37500.

41153. 1073604.

B-59

CU FT	•
CORY	
CATEGORY	CLASS IXW
	7

POUNDS

. .

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TOTAL

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DATE

B-60

POUNDS	1488850.	26455.	1488850.
CU FT	234939.	1677.	233261.
CATEGORY	TOTAL INITIAL ALLOWANCE	NML INITIAL ALLOWANCE	TOTAL INITIAL ALLOWANCE - (NML) 233261.

CATEUDRY	OR FSN.	9	CLASS		DESCRIPTION	OUANTITY	
URGANIZATIUNAL MPNS SQUARE LUADED							
ONGANIZATIONAL MPNS NON-SOCARE LUADED							
INDIVIDUAL WEAPONS							
	E1180	00526A	בן ט	PISTOL. AUTO.	CAL 45. MI911AI		
	E1400	00538A	= 3	REVOLVER. CAL	CL 11 REVOLVER, CAL 38, S AND W. W/E	E 43.	
	E1440	05538A	11 75	RIFLE. 5.55MM	. MISAI. 4/E		

*****	**************	********	***	***LANFUR SUPPLIES***	PLIES	****	*****************	*******
SOO		CU FT HOUNDS	500	DOS CU FT POUNDS	POUNDS	Sua	CU F1	POUNDS
•	•	•	•	•	•	•	•	•
•	•	•0	0	•	•	c	•	•
S	238.	7832.	01	476.	15665.	15	714.	23497.
v	÷	•09	9	•	120.	15	•	181.
	241.	7893.		482.	15785.		723.	. 23678.
S	23.	578.	01	* 9	1157.		68.	1735.
	120.	2117.		2.	26.		122.	2143.
s		131.	10	15.	263.	15	23.	394.

MOUNT OUT (CLASS I. CLASS VI. AND CLASS VIII) FOR M8937X

GALLONS .065 CUNTAINER

TOTAL URGANIC CAPACITY

.590.

S GAL CANS

URGANIC WATER CANHYING CAPACITY FOR MB937X

67

CATE

B-64

GAL/MAN TOT GAL

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	•••••	URGN LOA	*******	****	NF OR SUF	PPL IES***	*****	*** TOTAL	*******
CATEGORY	soa	CU FT	POUNDS	500	CU FT	DOS CO ET POUNDS DOS CO ET POUNDS DOS CO ET POUNDS	500	CUFT	SOMOO
CLASS 11# .									
(1YPE 1)	v	•2	155.	10	13.	5 7. 122. 10 13. 244. 15	51	20. 360.	366.
TOTAL CLASS III		:	7. 122.		13.	13. 244.		20.	366.
CLASS 1XW	s	3.	3. 109.	01	13.	10 13. 655. 15	91	16. 763.	763.
10.TAL		10.	10. 231.		27.	27. 899.		36.	36. 1129.

MOUNT OUT (CLASS 111) FOR M8937X

•

#### ORGANIZATIONAL LOAD

	sno	CANS	DUS CANS GALLONS PUUNDS	Dd s		GALLONS POUNDS	POUNDS	DRUMS	GALLONS CU FT PUUNDS	GAL DRUMS	PUUNDS	CU FT POUNDS	KA 6F5 + +
DIESEL	0	•		••	•	•	•	26.	1378.	286.	11037.		
*36.45	v				•	•	•	15.	195.	165.	5667.		
9	۰					•	•	•	•	•	.0		
KEROSENE	v	•			•			:	53.	::	414.		
LUNE													
(11110)	S							2.	108.	22.	929.	•	.0
LUBE													
(11114)	S							:	54.	::	469.		
CLASS IIIW	2.0							•	•	•	•	*	105.
B-6		:		:	•	•	•		2388.	*66*	1881	ŕ	105.

DATE

MOUNT DUT (CLASS III) FOR MB937X

#### LANDING FURCE SUPPLIES

	•	*******	************** GAL DRUMS*********	WS****	*******	****	**************************************	ILK******		.0	******DRY PACKAGES****	*****5 3
CATEGORY	Sco	DRUMS	GALLUNS CU FT POUNDS	CU FT	POUNDS	500	DOS GALLUNS CU FT POUNDS	CU FT	POUNDS	500	DOS CUFT PUUNOS	SCNOOL
DIESEL	N	:	583.	121.	4609.	Ð	8 2072.	278.	14441			
MUGAS	N	•	318.	•99	2267.	Œ	1233.	165.	7532.			
4	N	248.	13144.	2724.	2724. 103164.	13	13 85336.	11435.	580283.			
KERUSENE	~	:	53.	፥	414.	60	•	• 0	•			
LUBE	•	:	216.	*	1858.					•	•	•
LUBE (111A)	01.	:	24.	Ė	469.							
CLASS IIIW (MAHCORP)	01	•	:	•	:					9		210.
TOTAL		271.	14368.	2981.	2981. 112845.		88640.	88640. 11878.	602296.		:	210.

DATE

19

MOUNT DUT (CLASS VW) FOR M8937X

TOTAL REGULREMENT = BASIC ALLOWANCE PLUS 15 DOA

## URGANIZATIONAL LUAD = BASIC ALLOWANCE PLUS 5 DOA

#### MOUNT OUT (CLASS VW) FUR M8937X

			ROUNDS	TOTAL	ORGN					0000		
			2		-					EXCESS LANFOR	LANE OF	
90			PACKAGE	RORMT		**************************************	**OBGN	LOAD****	*******	CAFRIED	CARRIED SUPPLIFS	
CLASS		DESCRIPTION	ROUNDS	ROUNDS	ROUNDS	ROUNDS PACKAGES	KAGES	CU FT	POUNDS	ROUNDS	POUNDS	
	0A475	CTG CAL .45 BALL MI	20002	1584.	1144.	2000-	-	•	113.	856.	•0	
	00400	CTG CAL .38 SPECIAL 2400.	2400.	1075.	645.	2400.	-	:	92.	1755.	.0	
	0A058A	CTG 5.56MM TRACER M	1640.	3080.	2053.	3280.	2.	2.	120.	1227.	.0	
	OAUTIA	CTG 5.56MM BALL M19	1680.	64680.	50307.	50400.	30.	36.	2400.	93.	14293.	
	06841	CTG RIFLE GRENADE 5 2080.	2080.	462.	359.	2080.	-	•0	56.	1721.	0.	
	05803A	ADAPTER GREN PROJ M	48.		7.	•8•	:	3.	*6*	41.		
	TOTAL							42.	2830.		•	
0-1	26650 Q-11 B-6	GREN HD AND RIFLE S	.91	32.	32.	4 8 •	E	2.	126.	• • • • • • • • • • • • • • • • • • • •	•	
0-1	11-0 TOTAL							\$	126.			
2	045578	RUCKET HEAT W/LCHR	15.	24.	• 91	30.	2.	<u>.</u>	236.	Ė	•	
^!	TOTAL							16.	236.			
TOTAL	,							•09	3192.			

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#### 10

### MOUNT OUT (CLASS VA) FOR M8937X

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ORGANIZATIONAL LOAD

### MOUNT OUT (CLASS VA) FUR M8937X

	EXCESS LANFOR	*** CAPRIED SUPPLIES	NOS ITEMS ITEMS	0. 0.	60. 0. 51250.	.00
		LOAD * * * * * * * * * * *	CU FT POUP	504.	0. 3060	504. 30600.
		**********	ITEMS PACKAGES	504. 504.	30600. 30600. 0. 30600.	
TOTAL	LUAD	RORMT	ITEMS	504.	30600.	
	TOTAL	RORMT	ITEMS	1512.	91800.	
ITEMS	PER	PACKAGE	ITEMS	:	:	
			DESCRIPTION	AVIATION ORDNANCE C	AVIATION GRONANCE W	
			21 003	SPEC AVORDCUCHA6F	SPEC AVORDMICHASE	TUTAL
		90	CLASS	SPEC	SPEC	SPEC TUTAL

TOTAL

504. 30600.

\*\* THE REPLENISHMENT RATE IS FOR 1 DAYS

CATEGÜRY	cu FT	POUNDS	
CLASS I (A MATIONS)	29.	1446.	
CLASS 1 (MCI)		1566.	
CLASS 1 (TRIUXANE)	:	12.	
TOTAL CLASS 1	105.	3938.	
CLASS IIW	:	15.	
CLASS IV	•	•	
CLASS VI (RAT SUPP)	ů	116.	
CLASS VI (QTHER)	•	•	
CLASS VII (NON-SQUARE)	•	:	
CLASS VIII	:	.61	
CLASS IXW (UNIT)	:	22.	
CLASS IXW (SUPPURTING)	•	29.	
CLASS X	•	•	
TOTAL	113.	+139.	SO FT
CLASS VIIW (SQUARE)	8	•	•
WATER(I GAL/MAN/DAY) S GAL CANS	•6•	2340.	
WATER (1 GAL/MAN/DAY) 2.5 GAL CANS	48.	2122.	

B-71

REPLENISHMENT RATE (UY DAYS) UF CLASSES I. II. IV. VI. VII(NUN SOUARE). VIII. IX AND X FOR MH937X

REPLENISHMENT RATE (PER DAY) OF CLASS 111 FUR MB937X

~

ORY PACKAGES*** CU FT POUNDS					•		21.	21.
**DRY PACKAGES*** CU FT POUNDS					•		•	:
PUUNDS	1856.	948.	44644.	13.				936. 47461.
CO FT PUUNDS	36.	21.	980.	•				936.
POUNDS	2126.	1105.	51532.	15.	148.	28.	•	1454. 54955.
****55 GAL DRUMS************************************	55.	32.	1363.	•	:	:	•	
####### GAL DRUMS####### DRUMS CU FT POUNDS	9.	3.	124.	•	•	•	•	132.
GALLUNS	265.	155.	6565.	2.	17.	3.	•	7008.
CATEGORY	DIESEL	MOGAS	a n	KEROSENE	CLASS IIIW LUBE	CLASS IIIA LUBE	CLASS IIIW (MARCURP)	TOTAL

THE REPLENISHMENT QUANTITIES HAVE BEEN EXPRESSED IN BOTH DRUMS AND BULK TO PROVIDE DATA FOR EITHER MODE OF TRANSPURTATION

REPLENISHMENT SUSTAINING HATE (PER DAY) OF CLASS VW FOR M8937X

			ROUNDS					
	. 50		PACKAGE					
21000	CLASS	DESCRIPTION	ROUNDS	ROUNDS	PACKAGES	CU FT	SOMOO	
0A475	-	CTG CAL .45 HALL MI911	2000.00	22.00	22.00	00.00	1.24	
04400	-	CTG CAL .38 SPECIAL BALL	2400.00	21.50	10.	16.	. 82	
DADEBA	-	CTG 5.50MM TRACER M196	1640.00	102.67	•00	90.	3.76	
0A071A	-	CTG 5.56MM BALL MI93 10-	1680.00	718.67	.43	15.	34.22	
14850	•	CTG RIFLE GRENADE 5.504M	2080.00	10.27	• 00	00.00	.28	
0H357H	2	HUCKET HEAT WALCHR M72 S	15.00	18.	• 05	.43	6.35	
0G803A	-	ADAPTER GREN PROJ MIAL W	48.00	00.	00.	• 00	.00	
06937	11-0	II-D GREN HD AND RIFLE SMK WP	16.00	.02	00.	• 00	•05	
TOTAL								

N

CATE

	RUINOS	. 476		F/0THER FO 1540.	F/0THER FO 43120.	1195 308,	HES MT2 SERIS	AUNCHING CLIPS	134
	DESCRIPTION	CTG CAL .45 HALL MIGIT	CTG CAL .38 SPECIAL HALL MAI	CTG 5.56MM TRACEP M196	CTG 5.56MM BALL M193 10-RD	CTG RIFLE GRENADE 5.55MM M195	RUCKET HEAT W/LCHR M72 SERIES M72 SERIS	ADAPTER GREN PROJ MIAI W/LAUNCHING CLIPS	TI-D GREN HE AND RIFLE SMK WP M34
90	CLASS	-	_	-	-		^1	-	11-D
	0000	04475	00400	040684	040714	05341	0H557B	063034	0.037

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	T POUNDS	20.16 0.00	1224.00	20.16 1224.00
	20	20.1	0.0	20.1
	PACKAGES	20.16 20.16	1224.00	
	TENS	20-16	1524.00	
(TEMS PER	PACKAGE	1.00	1.00	
	CG DESCRIPTION	DRUNANCE	DHUNANCE	
	DES	AVIATION	AVIATION	
	CLASS	SPEC	SPEC	
	DUDIC	AVORDCUCH46F	AVORDETCHASE	TOTAL

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DATE

#### SQUARE LUADED EQUIPMENT

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SJON TES					
202					
G05% 1 040/ 1040/17Y					
SONOOO	000		••	•	•
DRSN LANFORD JREMENTARRORM 1040' SJOOTIFS CU FT POUNDS QUANTITY CUANTITY	•••		•	•	:
GROW LAWFUD COUREMENTARTER 1040' SUPPLIFF COANTITY SO FT CO FT POUNDS QUANTITY COANTITY			•	•	•
**************************************	:::				
DUANT					
	SET.				
DESCRIPTION	FLOUDLIGHT SET. THAILER, AMPHIB TRUCK, UTILITY.				
DESCR	LOUDL AAILE RUCK.				
	242				
2					
	× 2 4				
	00903K 04459B 04751A				
E R					
RUL NUMB					
CONTRUC NUMBER CR FSN	82630 00840 01160				
3	600				
			V118		16.5
CATEGURY	<b>:</b> =	- 56	TOTAL CLASS VIIW	2	LANFUR SUPPLIES
, u	> 11	> w	J	0	-
3	(TYPE 1)	CLASS VIII	*	CHGN LOAD	FUB

9
DATE
-

MCUNT OUT (REPLENISHMENT) OF MAJOR EQUIPMENT FOR MA937X

PAGE 27

#### NUN-SQUARE LUADED EQUIPMENT

CATEGONY	CONTRCL NUMBER		2	DESCRIPTION	DESCRIPTION GUANTITY SO FT CU FT POUNDS QUANTITY GUANTITY	NT DUT PE	OUTREMENT	POUNDS	LOAD LOAD DUANTITY	COGN. LANFOR LOAD SUPPLIES ANTITY CUAUTITY	× × ×	
CLASS VIIW (TYPE 1+2)												
	A2480	00276A		SWITCHBOARD, TE	TE 0.		•	•		•		
CLASS VIIN (TYPE 3)												
TOTAL CLASS VIIN								ć				
CHGN LUAD	•											
							;	•				

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B-77

DATE

(CLASSES 1. 11. IV. VI. VII NON-SQUARE, VIII AND IX) CAHRIED BY FULLOW ON ECHELON FOR M8937X ASSAULT ECHELON REPLENISHMENT CARGO .

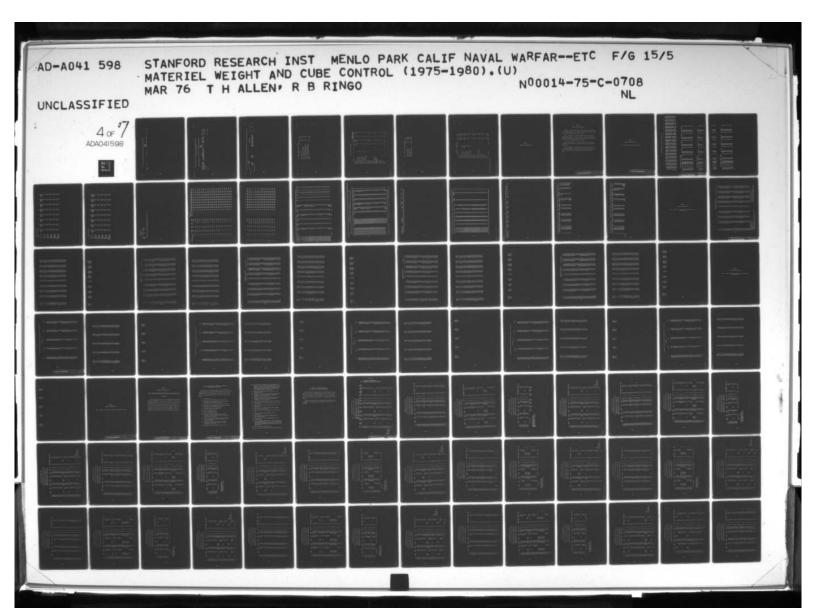
															S	
POUNDS	•	•	70492.	542.	71035.	815.	•	5206.	•	:	1069.	.776	1312.	:	80413.	:
CU FT	•	•	2142.	28.	2170.	20.	:	205.	•	•	•	27.	22.	:	2538.	:
sna	•	•	45	45		\$	45	\$	\$	45	•		*	45		•
CATEGORY	CLASS I (A RATIONS)	CLASS I (B RATIUNS)	CLASS I (MCI)	CLASS I (TRIUXANE)	TOTAL CLASS I	CLASS 11W	CLASS IV	CLASS VI (RAT SUPP)	CLASS VI (OTHER)	CLASS VITW (NON-SQUARE)	CLASS VIII	CLASS IXW (UNIT)	CLASS IXW (SUPPORTING)	CLASS X	TOTAL	CLASS VIIW (SOUARE)

ASSAULT ECHELON CLASS 111 CARRIED BY THE FOLLOW ON ECHELON FOR M8937X

CATEGORY	500	DRUMS	GALLONS	PROMS GALLONS CU FT POUNDS	POUNDS	GALLONS	*BULK****	POUNDS	********* GAL DRUMS######### ###########################
DIESEL	\$	•	•	•	•	11946.	1601.	1601. 83502.	
MOGAS	45	•	•	•	•	6978.	935.	426 38.	
4	<b>*</b>	•	•	•	•	295439.	39589.	39589. 2008988.	
KERUSENE	45	•	•	•	•	.68	12.	605.	
(1114)	•	15.	810.	165.	.9969		•		• 0
LUdE (111A)	\$	ě.	162.	33.	1406.				
CLASS IIIW	45	•	·	•	:				31. 946.
TOTAL		18.	972.	198.	8372.	314452.		42137. 2135732.	31. 946.

ASSAULT ECHELON CLASS VW CARRIED BY THE FOLLOW ON ECHELON FOR MUSSTX

			PER				
CLASS	DODIC	DESCRIPTION	ROUNDS		PACKAGES	CU FT	SONDO
-	04475	CTG CAL .45 BALL MI911	2000.		904.	0.	
-	0 400 64	CTG 5-SOMM TRACER MISS	1640.		3.	3.	162.
-	0A071A	CTG 5.56MM BALL MI93 10-RD	1680.		-92	31.	
	TOTAL					33.	2266.
2	0H557B	ROCKET HEAT W/LCHR M72 SERIES	15.	30.	2.	16.	240.
2	TOTAL			•		<u>.</u>	249.
TOTAL						•	2506.



ASSAULT ECHELON CLASS VZ CARRIED BY THE FOLLOW ON ECHELON FOR MB937X

ROUNDS PEH PACKAGE ROUNDS

DESCRIPTION

DIGCG

CLASS TOTAL

B-81

ROUNDS PACKAGES

CU FT

•

31

POUNDS

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DATE

# 10

ASSAULT ECHELON CLASS VA CARRIED BY THE FOLLOW ON ECHELUN FOR M8937X

# ASSAULT ECHELUN SORTIES

ASSALLT ECHELON CLASS VA CARRIED BY THE FOLLOW ON ECHELON FOR M8937X

		CU FT POUNDS	0.	0. 128520.	2117. 128520.
		CU FT	2117.		2117.
		CKAGES	2117.	128520.	
		ITEMS PACKAGES	2117.	128520. 13	
PER	PACKAGE	ITEMS	:	:	
	•	DESCRIPTION	TUN DRUNANCE CUBE FOR CHA	AVIATION ORDNANCE WEIGHT FOR C	
		21000 S	VORDCUCHASE	SPEC AVORDWTCHASE	DTAL
	93	CLASS	SPEC A	SPEC A	SPEC TOTAL

2117. 128520.

TOTAL

DATE

ASSAULT ECHELON REPLENISHMENT CLASS VII(SQUARE LOADED) CARRIED BY THE FOLLOW ON ECHELON FOR MA937X

S CNOOD S		.0			• 0
SO FT CUFT POUNTS		•	••	•	•
S0 FT		•		•	•
DESCRIPTION		FLOUDLIGHT SET. ELECTRIC. FSSE	TRAILER. AMPHIB CARGO. 1/4T. 2	TRUCK. UTILITY. 1/4T MISIAI-	
01					
		00903K	969000	04751A	
CUNTROL NUMBER CR FSN		90630	00840	01160	
CATEGORY	CLASS VIII				TOTAL CLASS VIIN

CATEGONY  I (MCI)  II (INDIVIDUAL WEAPONS)  II (CREW SERVED WEAPONS)  II (CREW SERVED WEAPONS)  VII (CREW SERVED WEAPONS)  VII (URGANIZATIONAL EQUIPMENT)	SONDO 1:	1566.	1573.	.0	. 5396.	.0	••	A536.
	CATEGORY CU FT	CLASS 1 (MC1) 48.	CLASS II (INDIVIDUAL WEAPONS) 87.		CLASS 11 (ORGANIZATIONAL EQUIPMENT) 392.			526.

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M8937X
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CARGO
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ED	POUNDS	:	790.	:	•	•	•	•	;	:	•	2000.	•	•	•	•	210.	•	•	•	.0	•	3000.
******	CU FT POUNDS	:	52.	•	•	•	•	•	•	•	•	•	•	•	•	:	• • •	•	•	•	•	•	62.
	POUNDS	1566.	7485.	;	:	•		•	•	:	:	2000-	•	:	•	•	210.	•	•	•	:	•	11261.
	CU FT	.8.	520.	•	•	•	•	•	•	•	•	37.	•	•	•	:		:	•	•	•	•	613.
	S0 FT															:							•
	SAL.			•	•	:	•	•	•	•													
	CATEGORY	CLASS 1	CLASS 11	CLASS 111 DIESEL	CLASS III MOGAS	CLASS 111 JP	CLASS III KEROSENE	CLASS III'N LUBE	CLASS IIIA LUBE	CLASS III'N (MARCORP)	CLASS IV	CLASS VW	CLASS VA	CLASS VZ	CLASS VI	CLASS VII NML(SQ)	OTHER CLASS VII (NON-SOUARE)	CLASS VIII	CLASS IXW	CLASS IXA	CLASS 1X2	CLASS X	TOTAL

POUNDS

CU FT

		,
MOUILE LUAD CAPACITY	• 29	10000
MOBILE LUADED CARGO	613.	11261.
UNUSED CAPACITY	•	7000
COOKS COOKS IN THE CONTROL	262723.	2342566

GENERAL CARGO FOR M8937X

POUNDS	22112.	1601901	30187.	15466.	683451.	829.	2786.	937.	315.	•0	1872.	91800.	•	1735.	3081.	2537.	763.	43753.	•	•	1982716.	359850.
CU FT	676.	41915.	695.	396.	14163.	22.	99	22.	10.	•	32.	1512.	•	68.	217.	145.	16.	2969.	•	•	62914.	189809.
S0 FT																						14411.
GAL.			4033.	2346.	98480.	106.	324.	108.	•													
CATEGORY		=	111 DIESEL	CLASS III MUGAS	CLASS 111 JP	CLASS III KEROSENE	CLASS IIIW LUBE	CLASS IIIA LUBE	CLASS IIIW (MARCURP)		* >	*	7.7	1,	CLASS VII NON-SOUARE	1111	H X I	IXA	1×2	×		CLASS VII SQUARE
	CLASS	CLASS	CLASS 111	CLASS	CLASS	CLASS	CLASS	CLASS	CLASS	CLASS IV	CLASS VW	CLASS VA	CLASS VZ	CLASS VI	CLASS	CLASS VIII	CLASS IXW	CLASS IXA	CLASS 1XZ	CLASS	TUTAL	CLASS

SAMPLES OF COMPUTER OUTPUTS

#### SAMPLES OF COMPUTER OUTPUTS

Appendix C contains sample output listings for the principal computer programs used in the study. The appendix is divided into four parts--each part presenting different sample output listings.

Parts 1 illustrates the output from the Transporation Feasibility Estimator Program (TFE). The output represents the results obtained from processing a notional MAU. Descriptions for reading the TFE Program output are found in the HQ FMFPAC TFE User's Manual.

Parts 2 and 3 illustrate the output listings from the Constrained Cargo Factoring Model (CFF) for factored cargo and constrained cube runs, respectively.

Part 4 illustrates the output from the Constrained T/E Embarkation Analysis Model (CONTEAM). The listings from ten representative FMF units, each constrained to 90, 85, and 75 percent of full T/E strength are shown.

SAMPLES OF COMPUTER OUTPUT

Part 1: Example of TFE Output: Notional MAU

	15	.66666	.56666	99999	.66666	.66666	66666	66666	.66666	66666	.66666	.66666	.66666	.66666	66666	0	. 50666
	2	.66666	66666	.66666	66666	66666	66666	66666	66666	.66666	66666	66666	.66666	.66666	•	66666	.66666
	13	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	0	.66666	66666	.66666
	12	66666	.66666	.66666	.66666	.65666	.66666	.66666	66666	.66666	.66666	.66666	•	.66666	.66666	.66666	.66666
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SEA LOWER	10	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	•	.66666	.66666	.66666	.66666	.66666	.66666
RIGHT	•	.66666	.66666	.66866	.66666	.66666	.66666	.65566	.65466	•	.66666	.66666	66666	.66666	.64466	.66666	.66466
AIR UPPER	•	99999.	.66666	99999	99999	.66666	66666	. 66666	.0	99999	.66666	99999	.66666	.66666	. 66666	.66666	.66666
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JISTANCE M	•	.66666	.66666	.46666	66666	.66666	•	.66666	.66666	66666	.66666	.66566	.66666	.66666	.66556	66666	.66666
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	6	.66666	.66666	.0	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666	.66666
	8	.66666	.0	*66666	.66666	.66656	.66066	.60066	.66066	.66666	.66066	.66665	.66666	.66666	.66666	.66666	.46664

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POD CONSTRAINTS (MEAS. TONS/DAY)

	DAY C	DAY CAPACITY	DAY CAPACITY		DAY CAPACITY	DAY	CAPACITY	DAY	CAPACITY	DAY	CAPACITY	
POD- 1	•	.666666		•			. 666	•	.660		.666	
2 -	0	****	.666	•		.0	.666		.666	0	.666	
6 -0	0	*666666	.666	0		.0	. 566	•	.666	•	.666	
4 -	0	.666666	. 666			•	.666	.0	.666	0	.666	
5 -(	0	*666666	. 666			.0	.666	0	.666	0	666	
4 -	.0	*665566	.666	0		.0	. 046	0.0	. 660	0	.606	
	.0	*6551.66	aye.	. 0	.666	.0	193.	.0	****	0	.666	
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FT/DAY)
CONSTRAINTS (SQUARE
POD CONS
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Ü	DAY CAPACITY	_		DAY CAPACITY	DAY	CAPACTTY	DAY	CAPACITY	DAY	CAPACITY	
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	.666666		•	.666	•	.666	•	.666		666	•
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	***		•	.666	•	.666	•0	.666		.666	0
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	*66666			.666	•	.666	•	.666		.656	0
	.666666		•	.666	•	.666	.0	.666		.666	0
	.666666		•	.666	•	.666	•	.660	•	.666	0
	.666666			.666	.0	.666	•	. 666		.666	0
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v	•	.664466	.664466	*****	.66.	•0	•	•	.664	•	•0	•	.664	•	•	•	*664	•	•0	•	.664	•	•	•
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	SHIP	SINGLE	SINGLE	SINGLE	SINGLE															
	AVAIL POE-8	666	556	666	666	666	566	666	666	666	666	666	666	666	666	666	666	666	666	666
	AVAIL PUE-7	665	666	665	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	665
	AVAIL POE-6	366	555	666	666	666	666	666	666	666	666	666	566	666	666	666	666	666	666	666
	AVAIL POE-5	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666
	AVAIL POE-4	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	665	666
	AVAIL POE-3	566	566	666	666	666	566	566	566	666	666	666	666	666	666	666	666	666	656	666
	AVAIL POE-2	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666
	AVATL POE-1	- 66	999	999	- 66	666	999	1 666	666	999	-666	999	999	-666	1666	999	1 666	999	1666	- 666
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SHIP IN	LOAD UNIT	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
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	CAA	226.	526.	226.	322.	1374.	1903.	1903.	947.	927.	658.	861.	875.	859.	333.	323.	316.	314.	337.	337.
	CARGO	2526.	2522.	2522.	1074.	*06*	3042.	3042.	1251.	1261.	950.	1130.	466	1152.	•	•	•	:	•	•
	SPEED	20.	50.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.	20.
	SHIP SHOUP NUMBER SPEED	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
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: :	666	666	665	**	665	666	665	666	666	666	666	666	666	666
7 7	666	666	565	***	555	566	666	666	666	666	666	666	666	666
166	666	666	666	***	666	666	666	666	666	666	666	666	666	666
: 5	666	666	555	5 5 5	164	565	766	666	666	666	666	666	666	666
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, 0	666	666	555	666	666	666	666	666	666	666	666	666	666	666
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	Į,	22	23	4	\$2	92	12	22	52	30	<b>∓</b> C-13	35	33	*

REGUIREMENT NAME	BLKCRGO	OUTSIZE	NON-AIR	PSSNGRS	-NISC-	SOFEET	POE	004	OAD	FAE	MODE	ROC
							:	•	:	:	:	:
CCVAAMOTOOUA	55.	•	•	75.	2.	1355.	-	~	-	10		14
PG- 1480101U4	•	•	•	::	-	321.	-	2	-	10	•	•
40105	•\$	•	•		•	214.	-	2	-	10	4	*
460110800000	35.	3	•	.94	:	680.	-	2	-	10	,	7.
2517741013 4	162.	•0	•	207.	:	•	-	2	-	10	•	7.
OS. SAMIOIS A	184.	•	•	207.	-	.0	-	~	-	10		1.
0	182.	•	•0	207	:	.0	-	~	-	10	•	**
0314441013 0	162.	.0	.0	207		0	-	7	1	10		*
0	570.	0	•0	402	.6	4780.	-	~	-	10	•	:
MOSSOMOSSON	1.		•		•			2	-	10		7.
IMMAMILLO3 A	.658		•	126.	.5	4842.		~		-	•	*
SHLESMOZOTUA	6	•	• 0	22.	0.	177.	•	2	-		•	
AULUS ON TAXA	21.		•0		: -	263		•			4	
AUCOCOMO SANA		0		•								
PHSACMOZONAL			. 0	36	: :	214		. ^			•	: :
MC 205MC 205M							• -		• •			::
WITTER STORES				•		• • • • • • • • • • • • • • • • • • • •	• •		••			::
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COSMANDED TON		•	•	.,,	•	104/		•	-	0		*
95NECMOZOBUA	• ;	•	•	2.	•	•0	-	2	-	10	•	7.
STY A BMO 209UA	52.	•	•	35.	•	3297.	-	~	-	10		*:
STWE BMD210UA		•	•	7.	•	•	-	2	-	10		14
MOSOMOSOUA	340.		•	13.	14.	10485.	-	2	-	10		*:
9CXAAM0301UA	1:	•	•	3,	•	•	-	~	-	10		*
MUSOSMOSOSUA	1.	••	•	7.	•	.0	-	2	-	10		14
GGDECMO3G3UA	:	•	••	7.	•	.0	-	2	-	-	•	*
PHSEAMCZD&UA	1:	•	•	2.	•	•	-	2	-	10		*
UJVAAMOBOSUA	12.		•0	35	0.0	0	-	2	-	10		*
25SAAM0207UA	1:	•	•0	. 80	•	•	_	2	1	10		*
FJUE BHO307UA	1.		•	3,	•		-	2	-	20		•
FTFEBM0308UA			•	3.	•			~	-	-	•	
9JLAAM1309UA	.00	•	.0	29.	•	0	1	~	-	-	•	-
94JECHO310UA		0	•	31.	•			•		-	•	
JJE EHMO311UA	33.	•	•	36.	•		-	~	-	-		
HJF EBM0312UA	3.		•	12.		0						
UJCEBMO313UA			•	•						-	•	
HVRL1M0314UA	•	•	•		•			•		-	•	
HVHL 2M0315UA	1.	•	•		:					-	•	
HVRL3M0316UA	:	•	•	*	•		-	~	-	2	•	*
JVJE1M0317UA	:	• 0	•	2.	•	.0	-	~	-	10	•	*
JVJEZMO318UA	:	••	•0	20.	•		-	~	-	10	•	:
JVJE3M1319UA	:	•	•	2.	•	•	-	~	-	10		*
JVJE4M0320UA	:		•	•	•	.0	-	~	-	10		*
9VCECM0321UA	2.	0.	.0	•	•	.0	-	~	-	10		*
MOGOGMOGOOUA	630.	• 0	•	372.	92.	. 4046	-	~	-	10		*
MOZOOMOZOOUA	2177.		•	402	139.	5349.	-	~	-	-		*
MOTOIMOTOIUA	872.		•	142.	•	40913.	-	~	-	10		
1												
TOTAL	. 6348.	:	•	2843	279.	84421.						

THERE WAS NO CHANGE FROM DAY. U THRU DAY- 11

•		•	•	•	•	•		•	•		•		•					•		•								•		•	•	•	•	•	• .	•	• •	•	•	•	•	•	•	•	•	•	•	•	
		PSSNORS	75.	11.		* * *	207.	207.	207.	207.	405.	•	126.	22.	43.	. 8	24.	3.	•	22.	5.	35.	7.	13.	3.	7.	7.	2.	35.	8.	÷	3.	29.	31.	36.	12.	•	.6	:		2.	20.	2.	:		372,	402.	142.	•
		NON-AIR	0.0	0.0									0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0		0.0					0.0	0.0	0.0	0.0	0.0	0.0	0.0	
		OUTSIZE	0.0	0.0	0.0		•	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				•	•	•				0.0	0.0	0.0	0.0	0.0	0.0	
	2	BLKCRGO	55.0	0.6	2.0	2	182.0	182.0	182.0	182.0	570.0	1.0	559.0	0.6	21.0	1.0	11.0	1.0	11.0	174.0	1.0	52.0	1.0	340.0	1.0	1.0	1.0	1.0	12.0	1.0	1.0	1.0		6	33.0		0.1	0.1	1.0	0:1	1.0	0.4	1.0	1.0	2.0	630.0	1002.0	0.0	
1		SOUAMEFT	1355.0	351.0	214.0	0.099	0.0	•••	0	0.	4780.0	0.0	4846.0	171.0	263.0	0.0	21.00	0.0	200.0	184/.0	0.0	329/.0	0.0	10485.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.						0.	0	•	0.	0.0	0.0		0.0	0.000	5347.0	38494.7	
Cadana iso	CARGO DELIVERED	MISCRGO		1.0	0.0	1.0	1.0	•••	•	1.0	•			0.0	1.0	0.0	0.0	0.0	0.0	3.0	0.0	8.0	0.0			0.0	0.0	0.0		•	0.0	0.0	•	•	•	0.0	•	•	•		•			•	0.0	95.0		0.0	
	ADDITIONAL.	REGUIREMENT NAME	CCVAAMO100UA	PGLAAMO101UA	M0102M0102UA	PUBECM01108A	DEVANHIO13 A	GVAAMIO13 B	DGVAAMIOI3 C	OGVAAMIOIS D	96UAAM1037 A	MOSOOMOSOOM	IHMAAM1103 A	9HLEBM0201UA	4HXAAM0203UA	HVECM0202UA	PHSAAMO204UA	MOZOSMOZOSUA	FJGEHM0206UA	SSAAMO207UA	SNE CM0208UA	ZTYAHM0209UA	9TWE BM0210UA	M0300M03000A	9CXAAM0301UA	M0302M0302UA	QUDECM0303UA	PHSAAM0204UA	UJVAAM0305UA	25SAAM0207UA	JAE HM0307UA	FTFEBM0308UA	9 JL AAMO 309UA	9JJECM0310UA	JULE HM 0311UA	HUPEHMUSICUA	UDCERMO313UA	HAHLIMUSIAUA	HVRL 2M0315UA	HVRL3M0316UA	JVJE1M0317UA	JVJE 2M0318UA	JVJE 3M0319UA	JVJE 4M0320UA	9VCECM0321UA	M0600M0600UA	MOSOGMOSOOM	M0701M0701UA	
1		REGUI	200	194	OM	PUE	190	190	190	190	196	0 N	ii.	H6	CH4	H4	PHG	NO.	F.30	552	956	21)	976	ON	606	OE	390	PH	5	<b>5</b> 2	F	FT	176	6	7	T.	200	2	> .	474	'n	*	`^	, Y	346	0 ×	01	2	
		CLOSUR	T CLO	1 CLOSE	T CLOSE	1 CLUSE	1 CLOSE	T CLOSE	CLOSE	1 CLOSE	CLOSE	T CLOSE	T CLOSE	T CLUSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE	CLOSE	CLOSE	CLOSE	T CLOSE	T CLOSE	I CLOSE	I CLOSE	T CLOSE	T CLOSE	T CLOSE	T CLOSE			
		POS	THIS	THIS	THI	THIS	S	THIS UN	THIS	IND SIHL	THIS	THIS UN	THIS	THIS	THI	-	IND SIHL	H		H	THI	THIS	THI	SIHI	THIS	HIS	THIS	THIS	THIS	THIS UN	THIS	THIS	THIS	THIS	ZO SIHL	THIS ON	NO SINI	NO SINI	THIS CN	THIS UN	THIS	THIS UN	HIS UN	THIS UN	-	THI	•	•	•

ALLONOOMO SAN	0.0	0.0	1175.0	9718100	2000	ATTENDED TOTAL TOTAL TOTAL STATE NOTICE NOTICE OF O O.O. O.O.O.O.O.O.O.O.O.O.O.O.O.O.O
M0701M0701UA	0.0	2451.2	872.0		0.0	

	 ******	PRIORITY GROUP		1 CLOSURES (DAY	(DAY) ****	*****		•
BLKCRGO	OUTSIZE	NON-AIR	PSSNGRS	-MISC-	SQ-FEET	FINAL	DESIRED DELIVERY	HODE
*	666	666	13	566	:	:	:	•
13	000	666	13	13	13	13	=	•
13	***	***	13	13	13	13	*1	•
13	665	666	13	666	. 13	13	**	•
13	666	466	13	13	13	13	=	•
13	666	666	13	13	666	13	*	•
13	666	666	13	13	666	13	*-	•
13	666	666	13	13	666	13	*	•
13	665	666	13	13	666	13	*	•
13	666	666	13	13	13	13	*	•
13	666	666	13	666	666	13	*	•
13	666	666	13	13	13	13	*	•
13	666	666	13	666	13	13	*1	•
13	666	666	13	13	13	13	*	•
13	666	666	13	666	666	13	*	
13	666	666	13	666	13	13	=	•
13	666	666	13	666	666	13	*	
13	666	666	13	666	13	13	*	•
13	666	666	13	13	13	13	*-	•
13	666	666	13	666	666	13	*	•
13	666	666	13	13	13	13	-	•
13	666	666	13	066	666	13	*	
13	665	566	13	13	13	13	*	•
13	666	666	13	666	666	13	*	•
•	000	000		-000	000		**	

13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	*:
666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	646	666	666	666	656	13	13
666	666	666	666	665	666	666	666	666	666	666	666	666	666	666	666	656	666	666	666	13	13
13	13	13	. 13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13
666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666	666
666	666	666	666	666	666	666	666	665	666	666	666	666	666	665	666	666	666	666	666	666	666
13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	13	1.
M030240302UA	GGDECM0303UA	PHSAAM0204UA	UJVAAMO305UA	25SAAM0207UA	FJRERM0307UA	FTFERM0308UA	9JLAAM0309UA	9JJECM0310UA	JJEEHM0311UA	HJFEHM0312UA	UJCERMO313UA	HVRLTM0314UA	HVHL2M0315UA	HVRL3M0316UA	JVJE1M0317UA	JVJEZMO318UA	JVJE3M0319UA	JVJE4M0320UA	9VCECM0321UA	MOGOMOGOOM	M0200M0200N

	800	::
•	MODE	:
****	FAE	:
	OAD	:
	004	:
•••••••	90e	:
	SOFEET	******
********** 2	-MISC-	
PRIORITY 2	PSSNGRS	******
d	NON-AIR	
********	BLKCRGO OUTSIZE	-
**********	BLKCRGO	
*********************************	REGULARENT NAME	

DESTINATION UNLOADING CUMPLETED MEAS. TONS PASSENGERSMISC- AREA	*****************************
Z DAY 13. 1147.2 386. Z79.0 Z DAY 13. 107.2 1582. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	PORT LOADED
Z DAY 13. 107.2 386. 279.0 Z DAY 13. 107.2 1582. 0.0 Z DAY 13. 1036.8 0.0 Z DAY 13. 0.0 0.0 Z DAY 14. 1251.2 0.0 0.0	119.50
Z DAY 13. 1147.2 1582. 0.0 Z DAY 13. 1036.8 0.0 Z DAY 13. 0.0 Z DAY 14. 1251.2 Z DAY 14. 306.8 0.0	PO€- 1
Z DAY 13. 1036.8 0.0 16. 0.0 2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	PO- 1
Z DAY 13. 1036.8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	POE- 1
Z DAY 13. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	POE- 1
2 DAY 13. 10.00 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	POE - 1
Z PAY 13. 1017.6 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	POE- 1
Z DAY 13. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	-
Z DAY 13. 0.0 0.0 0.0 0.0 2.0 DAY 13. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	-
2 DAY 13. 0.0 0.0 0.0 0.0 2 DAY 13. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	-
2 DAY 13. 0.0 0.0 0.0 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 0.0	-
2 DAY 13. 0.0 0.0 0.0 2.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 2 0.0 0.0	-
2 DAY 14. 490.4 0. 0.0 2 DAY 14. 1251.2 0. 0.0 2 DAY 14. 306.8 0. 0.0	-
2 DAY 14. 1251.2 0. 0.0	-
2 DAY 14. 306.8 0. 0.0	POE- 1
	PUE- 1

PARTIAL SHIP NUMBER	P NUMBER	PORT LOADED	DESTINATION	UNLOADING COMPLETED	COMPLETED	MEAS. TONS	PASSENGERS	-MISC-	AREA
NUMBER	2	POE- 1	P00- 2	DAY	13.	0.0	•0	8459.0	.0.0
NUMBER	3	POE- 1	5 -00d	DAT	13.	0.0	189.	6333.0	0.0
NUMBER	4	POE- 1	P00- 2	DAY	13.	0.0	317.	0.0	.0.0
NUMBER	2	POE- 1	P00- 2	DAY	13.	0.0	1764.	6333.0	0.0
NUMBER	ç	POE- 1	F00- 5	DAY	13.	0.0	323.	0.0	0.0
NUMBER	7	POE- 1	P00- 2	DAY	13.	0.0	316.	0.66	0.0
NUMBER		POE- 1	P00- 2	DAT	13.	0.0	1815.	6333.0	.0.0
NUMBER	•	P0E- 1	P00- 2	DAY	13.	0.0	314.	0.0	0.00
NUMBER	10	POE- 1	P00- 2	DAY	13.	0.0	337.	0.0	0.0
NUMBER	11	POE- 1	P00- 2	DAY	13.	0.0	337.	0.0	.0.0
NIJMBER	12	POE- 1	P00- 2	DAY	13.	0.0	337.	0.0	0.0
NUMBER	13	POE- 1	P00- 2	DAY	13.	0.0	337.	0.0	*0.0
NUMBER	14	POE- 1	P00- 2	DAT	14.	0.0	1374.	0.0	5319.00
NUMBER	15	POE- 1	P00- 2	DAY	14.	0.0	947.	0.0	9375.04
NUMBER	16	POE- 1	P00- 2	DAY	14.	954.0	927.	0.0	9975.0
						954.0			246.69 0

### SAMPLES OF COMPUTER OUTPUT

Part 2: Example of Constrained Cargo Factoring Model Output: Factored Cargo

17.1   17.1	18. TOT LON THE WO DIA CON IN THE CON IN THE CON THE CONTRIVE CO	## Color Total Color Total Color			·	,	CONSTRAIN		4	T 7	2
1757.7   1013.4   594.5   0.0   1672.0   3284.4     175.2   22.9   143.0   0.0   175.0   446.2.9     175.2   22.9   143.0   0.0   175.0   446.2.9     1101.4   55.0   426.0   0.0   0.0   175.0   446.2.9     1101.4   55.0   426.0   0.0   0.0   0.0     1101.4   55.0   426.0   0.0   0.0     1101.4   55.0   1.0     1101.4   55.0   1.0   0.	1757.7   1013.4   59.5   0.0   175     149.0   92.9   143.0   0.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0   175     160.1   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0     160.0   160.0     160.0   160.0     160.0   160.0     160.0     160.0   160.0	1757.7   1013.4   59.5   10.0   175.0   328.4     175.1   175.2   175.2   175.2   175.2   4062.2     175.2   175.2   175.2   4062.2     175.2   175.2   4062.2     175.3   42.5   42.5   42.5     175.4   42.5   42.5   42.5   42.5     175.4   42.5   42.5   42.5   42.5     175.4   42.5   42.5   42.5   42.5     175.4   42.5   42.5   42.5   42.5     175.4   42.5   42.5   42.5   42.5     175.4   42.5   42.5   42.5   42.5     175.4   42.5   42.5   42.5   42.5     175.4   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     175.5   42.5   42.5   42.5   42.5     17	מחרצ	TOT	CON TIE		UMA	×	1/8		200
140.0   92.9   813.0   0.0   175.0   4662.9     140.0   92.9   813.0   0.0   175.0   4662.9     1010.4   52.9   813.0   0.0   0.0   2662.9     1010.4   52.9   813.0   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     1010.4   52.9   426.6   0.0   2662.9     40.2   426.6	149.0   92.9   13.0   0.0   175     160.0   92.9   143.0   0.0   175     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1016.3   394.8   17.5   0.0   945     1016.3   394.8   17.5   0.0   945     1016.3   394.8   17.5   0.0   945     1016.3   394.8   17.5   0.0   945     1016.3   394.8   17.5   0.0   945     1016.3   394.8   17.5   0.0   945     1016.3   394.8   17.5   0.0   945     1016.3   394.8   17.5   0.0   945     1016.3   394.8   131.2   0.0   945     1016.3   394.8   131.2   0.0   945     1016.3   394.8   131.2   0.0   945     1016.3   394.8   131.2   0.0     1016.4   594.8   0.0   0.0     1016.4   594.8   0.0   0.0     1016.4   594.8   0.0   0.0     1016.4   594.8   0.0     1016.5   33.5   14.4   0.0     1016.5   33.5   21.4   0.0     1016.6   33.5   21.4   0	149.50   92.9   813.0   0.0   175.0   4662.9   175.0   175.0   4662.9   175.0   175.0   4662.9   175.0   4662.9   175.0   4662.9   175.0   4662.9   175.0   4662.9   175.0   4662.9   175.0   4662.9   175.0   4662.9   175.0   4662.9   4662.9   175.0   4662.9   466			1013.4	5.64	0.0	1672.0	328.4	312.0	4
165.0   02.9   143.0   0.0   175.0   4662.9   11014.4   559.1   426.6   0.0   0.0   175.0   4662.9   11014.4   559.1   426.6   0.0   0.0   0.0   0.0   426.8   11014.4   559.1   426.6   0.0   0.0   0.0   0.0   442.8   442.8   11014.4   559.1   426.6   0.0   0.0   0.0   0.0   442.8   442.8   11014.4   559.1   426.6   0.0   0.0   0.0   0.0   0.0   442.8   442.8   11014.4   559.1   426.6   0.0   0.0   0.0   0.0   0.0   442.8   442.8   11014.4   559.1   426.6   0.0   0.0   0.0   0.0   0.0   442.8   442.8   11014.4   559.1   426.6   0.0	165.0   92.4   143.0   0.0   175     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   345.8   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   17.5   0.0   945     1017.3   394.8   1312.3   0.0   945     1017.4   559.1   426.6   0.0   945     1017.4   559.1   426.6   0.0   945     1017.5   39.2   69.1   0.0   945     1017.5	165.0   02.9   13.0   0.0   175.0   4662.9   1101.4   1011.4   559.1   426.6   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0   0.0   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0   0.0   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0   0.0   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0   0.0   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0   0.0   0.0   0.0   0.0   4426.8   1101.4   559.1   426.6   0.0		0	42.9	83.0	0.0	175.0	4662.9	4196.6	4233.
1914.4   92.9   81.0   0.0   915.0   446.8   1014.4   559.1   426.6   0.0   915.0   446.8   446.8   1014.4   559.1   426.6   0.0   915.0   446.8   446.8   1014.4   559.1   426.6   0.0   915.0   446.8   446.8   1014.4   559.1   426.6   0.0   915.0   446.8   446.8   1014.4   559.1   426.6   0.0   915.0   446.8   446.8   1014.4   559.1   426.6   0.0   915.0   446.8   446.8   1014.4   559.1   426.6   0.0   915.0   446.8   446.8   1014.4   559.1   426.6   0.0   915.0   446.8	186.0 92.4 R1.0 0.0 0175  1014.4 559.1 426.6 0.0 945  1014.4 559.1 426.6 0.0 945  1014.4 559.1 426.6 0.0 945  1014.4 559.1 426.6 0.0 945  1014.4 559.1 426.6 0.0 945  1014.4 559.1 426.6 0.0 945  1014.4 559.1 426.6 0.0 945  1014.4 559.1 426.6 0.0 945  1014.4 559.1 426.6 0.0 945  437.3 348.3 1312.3 0.0 1660  437.3 392.1 345.8 0.0 941  437.3 394.8 17.5 0.0 416  437.3 394.8 17.5 0.0 416  437.3 394.8 17.5 0.0 64  110.3 39.2 69.1 0.0 68  43.4 0.0 68  43.4 0.0 0.0 945  110.3 39.2 69.1 0.0 108  110.3 39.2 69.1 0.0 108  110.3 39.2 69.1 0.0 108  110.3 39.2 69.1 0.0 108  231.5 66.6 33.6 0.0 13.9 0.0 13.9  110.3 39.2 69.1 0.0 108  231.5 66.6 33.5 69.1 0.0 108  231.5 7 18.0 13.9 0.0 18.0 18.0 13.9 0.0 13.9  35.0 18.0 13.9 0.0 0.0 88  58.6 33.5 21.4 0.0 0.0 54  58.6 33.5 21.4 0.0 0.0 54  58.6 33.5 21.4 0.0 0.0 54  58.6 33.5 21.4 0.0 0.0 54  58.6 33.5 21.4 0.0 0.0 54  58.6 33.5 21.4 0.0 0.0 54	1914.4   92.9   81.0   0.0   915.0   446.2		0	6.26	H3.0	0.0	175.0	4662.9	4196.6	4233.
1014.4   555.1   426.6   0.0   947.0   4426.8   1014.4   555.1   426.6   0.0   947.0   4426.8   1014.4   555.1   426.6   0.0   947.0   4426.8   1014.4   555.1   426.6   0.0   947.0   4426.8   1014.4   555.1   426.6   0.0   947.0   4426.8   1014.4   555.1   426.6   0.0   947.0   4426.8   1014.4   555.1   426.6   0.0   947.0   4426.8   1014.4   555.1   426.6   0.0   947.0   4426.8   4426.8   1014.4   555.1   426.6   0.0   947.0   4426.8   4426.8   1014.4   555.1   1312.3   0.0   1660.0   23015.7   4326.8   1312.3   345.8   0.0   1660.0   23015.7   4326.8   345.8   345.8   0.0   416.0   6531.0   6531.0   6531.0   6531.0   6531.0   6321	1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 1014.4 \$59.1 426.6 0.0 975 43.7 \$348.3 1312.3 0.0 167 43.7 \$348.3 1312.3 0.0 416 43.7 \$349.4 0.0 975 70.9 \$24.7 43.4 0.0 68 70.9 \$24.7 43.4 0.0 68 70.9 \$24.7 43.4 0.0 68 70.9 \$24.7 43.4 0.0 975 110.3 \$39.2 69.1 0.0 108 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 69.1 0.0 975 110.3 \$39.2 0.0 975 110.4 \$77.1 0.0 975 110.4 \$77	1014.4   555.1   545.6   0.0   947.0   4476.4   1014.4   555.1   545.6   0.0   947.0   4476.4   1014.4   555.1   542.6   0.0   947.0   4426.4   1014.4   559.1   542.6   0.0   947.0   4426.4   1014.4   559.1   542.6   0.0   947.0   4426.4   1014.4   559.1   542.6   0.0   947.0   4426.4   1014.4   559.1   542.6   0.0   947.0   4426.4   1014.4   559.1   542.6   0.0   947.0   4426.4   1014.4   559.1   542.6   0.0   947.0   4426.4   1014.4   559.1   542.6   0.0   947.0   5431.7   6431.7		0	65.6	0.19	0.0	175.0	4662.9	4136.6	4233.
1014.4   559.1   426.6   0.0   946.10   4426.8   1014.4   559.1   426.6   0.0   946.10   4426.8   4426.8   1014.4   559.1   426.6   0.0   946.10   4426.8   4426.8   1014.4   559.1   426.6   0.0   946.10   4426.8   4426.8   1014.4   559.1   426.6   0.0   946.10   4426.8   4426.8   1014.4   559.1   426.6   0.0   946.10   4426.8   4426.8   1014.4   559.1   426.6   0.0   946.10   4426.8   4426.8   1014.4   559.1   426.6   0.0   946.10   4426.8   4426.8   1014.4   559.1   426.6   0.0   946.10   53911.0   426.8   426	1014.4 559.1 426.6 0.0 947 10114.4 559.1 426.6 0.0 947 10114.4 559.1 426.6 0.0 948 10114.4 559.1 426.6 0.0 948 10114.4 559.1 426.6 0.0 948 10114.4 559.1 426.6 0.0 948 1014.4 559.1 426.6 0.0 948 1014.4 559.1 112.3 0.0 948 437.3 394.8 0.0 948 437.3 394.8 0.0 948 437.3 394.8 0.0 948 70.9 24.7 43.4 0.0 64 70.9 24.7 43.4 0.0 69 110.3 39.2 69.1 0.0 108 110.3 39.2 69.1 0.0 108 110.3 39.2 69.1 0.0 988 110.3 39.2 69.1 0.0 988 110.3 39.2 69.1 0.0 988 110.3 39.2 69.1 0.0 988 110.3 39.2 69.1 0.0 988 110.3 39.2 69.1 0.0 988 110.3 39.2 69.1 0.0 988 110.3 39.2 69.1 0.0 988 110.3 39.2 69.1 0.0 88 110.3 39.2 69.1 0.0 88 110.3 39.2 69.1 0.0 88 110.3 39.2 69.1 0.0 88 110.3 39.2 69.1 0.0 88 110.3 39.2 69.1 0.0 88 110.3 39.2 69.1 0.0 88 110.3 39.2 69.1 0.0 88 110.3 39.2 69.1 0.0 88 110.3 33.5 21.4 0.0 6.8 88 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 58 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 33.5 21.4 0.0 6.0 68 58.6 38.6 38.6 38.6 38.6 38.6 38.6 38.6 3	1014.4   559.1   476.6   0.0   946.10   4426.14   1014.4   559.1   426.6   0.0   946.10   4426.14   1014.4   559.1   426.6   0.0   946.10   4426.14   1014.4   559.1   426.6   0.0   946.10   4426.14   1014.4   559.1   426.6   0.0   946.10   4426.14   1014.4   559.1   426.6   0.0   946.10   4426.14   1014.4   559.1   426.6   0.0   946.10   4426.14   1014.4   559.1   426.6   0.0   946.10   4426.14   4426.14   426.1			259.1	456.6	0.0	945.0	4426.8	45024	4240.
1014.0   559.11   426.6   0.0   0.05.0   4426.4   1014.4   559.11   426.6   0.0   0.05.0   4426.4   4426.4   1014.4   559.11   426.6   0.0   0.05.0   4426.4   4426.4   1014.4   559.11   426.6   0.0   0.05.0   4426.4   4426.4   1014.4   559.11   426.6   0.0   0.0   0.05.0   4426.4   4426.4   1014.4   559.11   426.6   0.0   0.0   0.05.0   4426.4   4426	1014.4   559.1   426.6   0.0	1014.0   559.11   426.0   0.00   0.00   4426.0   1014.0   559.11   426.0   0.00   0.00   0.00   4426.0   1014.0   559.11   426.0   0.00   0.		•	559.1	456.6	0.0	0.00	4426.8	4.054	4240
1011.1 559.1 426.6 0.0 995.0 4426.8 1011.1 1011.1 426.6 0.0 995.0 4426.8 1011.1 426.6 0.0 995.0 4426.8 1011.1 426.6 0.0 995.0 4426.8 1011.1 426.6 0.0 995.0 4426.8 1011.1 426.6 0.0 995.0 4426.8 1011.1 12.3 0.0 1660.0 23015.7 102.1 346.8 11312.3 0.0 1660.0 23015.7 102.1 346.8 11312.3 0.0 1660.0 23015.7 102.1 346.8 11312.3 0.0 1660.0 23015.7 102.1 346.8 117.5 0.0 1670.0 6531.0 6531.0 102.1 346.8 117.5 0.0 1670.0 6531.0 102.1 102.1 346.8 117.5 0.0 1670.0 6531.0 102.1 102.1 346.8 117.5 0.0 1670.0 102.1 1	1014.4 559.1 426.6 0.0 985 1014.4 559.1 426.6 0.0 985 1014.4 559.1 426.6 0.0 985 1014.4 559.1 426.6 0.0 985 1014.4 559.1 426.6 0.0 985 1016.8 348.3 1312.3 0.0 1660 987 995.7 532.1 345.8 0.0 987 995.7 532.1 345.8 0.0 416 437.3 398.8 17.5 0.0 416 70.9 24.7 43.4 0.0 68 110.3 39.2 69.1 0.0 108 110.3 39.2 69.1 0.0 0.0 31 110.3 39.2 69.1 0.0 0.0 31 110.3 39.5 69.1 0.0 0.0 13.9 58.6 33.5 51.4 0.0 0.0 55 58.6 33.5 51.4 0.0 0.0 55 58.6 51.4 0.0 0.0 55 58.6 51.4 0.0 0.0 55 58.6 51.4 0.0 0.0 55 58.6 51.4 0.0 0.0 55 58.6 51.4 0.0 0.	1014.0   559.1   426.6   0.0   995.0   4426.4   1014.4   559.1   426.6   0.0   995.0   4426.4   1014.4   559.1   426.6   0.0   995.0   4426.4   1014.4   559.1   426.6   0.0   995.0   4426.4   1014.4   559.1   426.6   0.0   995.0   4426.4   4426.4   1024.4   559.1   426.6   0.0   995.0   4426.4   4			1.655	0.024	9.0	0.000	8.0744	4.0024	4740
1011.01   559.11   426.6   0.00   995.0   4426.8   1011.01   1011.01   426.6   0.00   995.0   4426.8   1011.01   1011.01   426.6   0.00   995.0   4426.8   1011.01   1012.3   0.00   1660.0   23015.7   4426.8   1011.01   2322.1   2352.1	1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1078.5   348.3   1312.3   0.0   1660     495.7   532.1   345.8   0.0   416     495.7   532.1   345.8   0.0   416     495.7   532.1   345.8   0.0   416     495.7   532.1   345.8   0.0   416     70.9   24.7   43.4   0.0   68     70.9   24.7   43.4   0.0   68     70.9   24.7   43.4   0.0   68     70.9   24.7   43.4   0.0   68     70.9   24.7   43.4   0.0   68     70.9   24.7   43.4   0.0   0.0     110.3   39.2   69.1   0.0   0.0     110.3   39.2   69.1   0.0   0.0     110.3   39.2   69.1   0.0   0.0     110.4   59.5   628.2   149.4   0.0   0.0     110.3   349.3   1312.3   0.0   0.0     110.3   349.3   1312.3   0.0   0.0     110.3   349.3   1312.3   0.0   0.0     110.3   349.2   69.1   0.0   0.0     110.3   349.2   69.1   0.0   0.0     110.3   349.2   69.1   0.0   0.0     110.3   349.2   69.1   0.0   0.0     110.3   349.3   1312.3   0.0   0.0     110.3   349.3   1312.3   0.0     110.3   349.3   1312.3   0.0     110.3   349.3   1312.3   0.0     110.3   349.3   1312.3   0.0     110.3   349.3   1312.3   0.0     110.3   349.3   1312.3   0.0     110.3   349.3   1312.3   0.0     110.3   349.3   1312.3   0.0     110.3   349.3   313.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.4   68.6   33.5   21.4   0.0     110.5   68.6   33.5   21.4   0.0     110.6   68.6   33.5   33.5   33.5     110.6   68.6   33.5   33.5     110.6   68.6   33.5   33.5     1	1011-11   559-11   426-6   0.00   995-0   4426-8   1011-11   1011-11   426-6   0.00   995-0   4426-8   1011-11   426-6   0.00   995-0   4426-8   1011-11   426-6   0.00   995-0   4426-8   1011-11   426-6   0.00   995-0   4426-8   4426-8   1011-11   426-8   0.00   965-0   4426-8   4426-8   1011-11   426-8   0.00   965-0   23015-7   436-8   0.00   965-0   23015-7   436-8   0.00   965-0   23015-7   436-8   0.00   967-0   6531-0   653		•	1.055	450.0	0.0	0.686	4420.8		4240.
1011.1 559.1 426.6 0.0 995.0 4422.8 1011.4 426.6 0.0 995.0 4422.8 1011.4 426.6 0.0 995.0 4422.8 1011.4 426.6 0.0 995.0 4422.8 1011.4 121.3 0.0 1660.0 23015.7 426.6 0.0 995.0 4422.8 1011.4 1312.3 0.0 1660.0 23015.7 905.7 532.1 345.8 0.0 877.0 6531.0 6531.0 905.7 532.1 345.8 0.0 877.0 6531.0 6531.0 905.7 532.1 345.8 0.0 416.0 6531.0 6531.0 1005.3 394.8 175.5 0.0 416.0 6531.0 1005.3 1006	1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.4   559.1   426.6   0.0   945     1014.5   348.3   1312.3   0.0   1660     405.7   532.1   345.8   0.0   416     417.3   394.8   17.5   0.0   416     417.3   394.8   17.5   0.0   416     417.3   394.8   17.5   0.0   416     410.3   39.2   69.1   0.0   69     410.3   39.2   69.1   0.0   69     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.3   39.2   69.1   0.0     410.4   69.1   0.0     410.5   69.1   0.0     410.	1011.4 559.1 426.6 0.0 995.0 4426.8 1011.4 1011.4 26.6 0.0 10.0 10.0 4426.8 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10		4 .	559.1	420.6	0.0	985.0	4420.8		4240
1014.4   555.1   426.6   0.0   0.05.0   4425.8   1078.5   346.3   1312.3   0.0   1660.0   23015.7   1078.5   346.3   1312.3   0.0   1660.0   23015.7   0.05.7   532.1   345.8   0.0   877.0   6531.0   0.0   477.0   6531.0   0.0   477.0   6531.0   0.0   415.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   415.0   0.0   0.0   415.0   0.0   0.0   417.0   0.0   0.0   417.0   0.0   0.0   415.0   0.0   0.0   415.0   0.0	1014.4 559.1 426.6 0.0 065.7 1074.4 559.1 1312.3 0.0 1660 1676.5 1676.5 1985.8 0.0 1676.9 167	1011.4 559.1 12.2 0.0 095.0 4926.4 107.5 1			1.600	4.50.0		0.686	9000		0000
1078-5   344.3   1312-3   0.0   1660.0   23015.7     1078-5   334.3   1312-3   0.0   1660.0   23015.7     205.7   532.1   345.8   0.0   677.0   65311.0     205.7   532.1   345.8   0.0   677.0   65311.0     205.7   532.1   345.8   0.0   677.0   65311.0     205.7   532.1   345.8   0.0   416.0   65311.0     205.7   532.1   345.8   0.0   416.0   65311.0     205.7   532.1   345.8   0.0   416.0   693.4     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   43.4   0.0   64.0   1006.3     70.9   24.7   24.1   26.1   26.1   26.1     70.0   312.0   26.2   21.4   0.0   22.0     70.0   312.0   26.2     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0     70.0   312.0	1678.5 348.3 1312.3 0.0 1660 1678.5 348.3 1312.3 0.0 1660 905.7 532.1 345.8 0.0 1670 905.7 532.1 345.8 0.0 175 437.3 394.8 17.5 0.0 416 70.9 24.7 43.4 0.0 64 70.9 24.7 43.4 0.0 64 110.3 394.2 65.1 0.0 108 110.3 395.2 65.1 0.0 108 110.3 395.2 65.1 0.0 108 110.3 395.1 16.7 215.5 0.0 108 110.3 345.1 16.7 215.5 0.0 108 110.3 345.1 16.7 215.5 0.0 1660 2313.5 628.2 149.4 0.0 2202 847.1 16.7 213.4 0.0 1660 2313.5 628.2 149.4 0.0 2202 847.1 628.2 149.4 0.0 1660 2313.5 18.0 13.9 0.0 187 110.3 35.0 18.0 13.9 0.0 188 110.3 35.0 18.0 13.9 0.0 188 110.3 35.0 18.0 13.9 0.0 188 110.3 35.0 18.0 13.9 0.0 188 110.3 35.0 18.0 13.9 0.0 188 110.3 35.0 18.0 0.0 13.9 0.0 188 110.3 33.5 21.4 0.0 55 58.6 32.6 32.6 32.6 32.6 32.6 32.6 32.6 32	1078.5 344.3 1312.3 0.0 1660.0 23015.7 005.7 532.1 345.8 0.0 0.0 6531.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		. 4	550.1	426.6	0.0	985.0	4426.8		4240
1678-5   348.3   1312-3   0.0   1660.0   23015.7     1678-5   348.3   1312-3   0.0   677.0   6531.0     1678-5   542.1   345.8   0.0   677.0   6531.0     1678-5   542.1   345.8   0.0   677.0   6531.0     1678-5   542.1   345.8   0.0   677.0   6531.0     1678-5   542.1   345.8   0.0   416.0   6531.0     1678-5   542.1   345.8   0.0   416.0   6531.0     1678-6   24.7   43.4   0.0   64.0   1096.3     1679-6   24.7   43.4   0.0   64.0   1096.3     1679-6   24.7   43.4   0.0   64.0   1096.3     1679-7   24.7   43.4   0.0   64.0   1096.3     1679-7   24.7   43.4   0.0   64.0   1096.3     1679-7   24.7   43.4   0.0   64.0   1096.3     1679-7   24.7   43.4   0.0   64.0   1096.3     1679-7   24.7   43.4   0.0   64.0   1096.3     1679-7   24.7   43.4   0.0   108.0   1520.2     1679-7   24.7   24.7   24.7   24.0     1679-7   119.3   1312-3   0.0   108.0   1320.0     1679-7   113.9   0.0   108.0   1320.0     1679-7   113.9   0.0   108.0   1096.3     1679-7   113.9   0.0   108.0   1096.3     1679-7   113.9   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.0     1679-7   113.0   0.0   108.	1678.5 348.3 1312.3 0.0 600 605.7 532.1 345.8 0.0 677 905.7 532.1 345.8 0.0 677 905.7 532.1 345.8 0.0 6416 416 417.5 0.0 416 416 417.3 390.8 17.5 0.0 416 416 417.3 390.8 17.5 0.0 416 416 417.3 390.8 17.5 0.0 6416 416 417.5 0.0 6416	1678-5 348.3 1312-3 0.0 1660.0 23015.7 0055.7 532.1 345.8 0.0 877.0 6531.0 0055.7 532.1 345.8 0.0 877.0 6531.0 0055.7 532.1 345.8 0.0 877.0 6531.0 0055.7 532.1 345.8 0.0 877.0 6531.0 0055.7 532.1 345.8 0.0 877.0 6531.0 0055.7 532.1 345.8 0.0 877.0 6531.0 0055.7 532.1 345.8 0.0 877.0 6531.0 0055.3 70.0 24.7 43.4 0.0 0.0 64.0 1006.3 70.0 24.7 43.4 0.0 0.0 64.0 1006.3 70.0 24.7 43.4 0.0 0.0 64.0 1006.3 70.0 24.7 43.4 0.0 0.0 64.0 1006.3 70.0 24.7 43.4 0.0 0.0 64.0 1006.3 70.0 24.7 43.4 0.0 0.0 64.0 1006.3 70.0 24.7 43.4 0.0 0.0 1006.0 152.0 2.0 1006.3 70.		ď	348.3	1 312.3		1660.0	23015.7		22048
905.7 512.1 345.8 0.0 677.0 6531.0 905.7 532.1 345.8 0.0 677.0 6531.0 905.7 532.1 345.8 0.0 677.0 6531.0 905.7 532.1 345.8 0.0 677.0 6531.0 905.7 532.1 345.8 0.0 677.0 6531.0 70.9 24.7 43.4 0.0 68.0 1006.3 70.9 24.7 43.4 0.0 68.0 1006.3 70.9 24.7 43.4 0.0 68.0 1006.3 70.9 24.7 43.4 0.0 68.0 1006.3 110.3 39.2 69.1 0.0 69.0 1006.3 110.3 39.2 69.1 0.0 108.0 15592.2 110.3 39.2 69.1 0.0 108.0 15592.2 110.4 34.4 0.0 108.0 15592.2 110.4 34.4 0.0 108.0 15592.2 110.3 39.2 69.1 0.0 108.0 15592.2 110.3 39.2 69.1 10.0 108.0 15592.2 110.4 49.3 1312.3 0.0 106.0 23315.7 23315.7 50.6 34.8 0.0 166.0 23315.7 23315.7 50.6 34.8 0.0 166.0 23315.7 23315.7 1002.7 113.9 0.0 166.0 156.0 166.0 1	905.7 532.1 345.8 0.0 677 905.7 532.1 345.8 0.0 677 905.7 532.1 345.8 0.0 677 905.7 532.1 345.8 0.0 677 905.7 532.1 345.8 0.0 670 915.3 373.3 398.8 17.5 0.0 416 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 0.0 108 110.3 39.2 69.1 0.0 0.0 108 110.3 39.2 69.1 0.0 0.0 332 345.8 110.3 39.2 69.1 0.0 0.0 332 345.8 110.3 345.8 0.0 0.0 108 13.7 69.1 106.2 113.9 0.0 0.0 108 13.9 0.0 0.0 31.9 35.0 18.0 13.9 0.0 0.0 31.9 35.0 18.0 13.9 0.0 0.0 31.5 21.4 0.0 0.0 54.8 58.6 33.5 21.4 0.0 0.0 54.8 58.6 58.6 33.5 21.4 0.0 0.0 54.8 58.6 58.6 33.5 21.4 0.0 0.0 54.8 58.6 58.6 33.5 21.4 0.0 0.0 54.8 58.6 58.6 33.5 21.4 0.0 0.0 54.8 58.6 58.6 33.5 21.4 0.0 0.0 54.8 58.6 58.6 33.5 21.4 0.0 0.0 54.8 58.6 58.6 33.5 21.4 0.0 0.0 55.6 58.6 58.6 58.6 33.5 21.4 0.0 0.0 55.6 58.6 58.6 58.6 58.6 58.6 58.6 58.6	905.7 512.1 345.8 0.0 877.0 6531.0 905.7 532.1 345.8 0.0 977.0 6531.0 905.7 532.1 345.8 0.0 977.0 6531.0 905.7 532.1 345.8 0.0 9.0 977.0 6531.0 905.7 532.1 345.8 0.0 9.0 977.0 6531.0 905.7 532.1 345.8 0.0 9.0 977.0 6531.0 905.7 7.0 9.0 916.		2	348.3	1312.3		660	23015.7		22048
905.7 5.32.1 345.8 0.0 677.0 6531.0 905.7 5.32.1 345.8 0.0 677.0 6531.0 417.3 590.8 17.5 0.0 416.0 693.4 437.3 590.8 17.5 0.0 416.0 693.4 70.9 24.7 43.4 0.0 69.0 1096.3 70.9 24.7 43.4 0.0 69.0 1096.3 70.9 24.7 43.4 0.0 69.0 1096.3 110.3 39.2 69.1 0.0 69.0 15592.2 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 135.1 116.7 215.5 0.0 133.0 16231.4 135.1 116.7 215.5 0.0 133.0 16231.4 135.1 116.7 133.9 0.0 2202.0 31214.4 101.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 110.3 39.2 69.1 0.0 108.0 1776.3 150.0 18.0 133.0 0.0 1776.3 150.0 18.0 133.0 0.0 1776.3 150.0 18.0 133.0 0.0 1776.3 150.0 18.0 173.0 0.0 1776.3 150.0 1700.9 150.0 1700.9 1700.9 150.	905.7 532.1 345.8 0.0 677 4 973.3 394.8 17.5 0.0 416 4 37.3 394.8 17.5 0.0 416 70.9 24.7 43.4 0.0 69 70.9 24.7 11.2 0.0 1.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	905.7 5.32.1 345.8 0.0 877.0 6531.0 905.7 5.32.1 345.8 0.0 877.0 6531.0 417.3 399.8 17.5 0.0 416.0 699.4 437.3 399.8 17.5 0.0 416.0 699.4 437.3 399.8 17.5 0.0 416.0 699.4 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 110.3 39.2 69.1 0.0 108.0 15592.2 110.3 39.2 69.1 0.0 108.0 15592.2 110.4 5.50.1 106.7 2.31.2 0.0 99.0 100.0 2335.1 106.7 21.4 0.0 2311.0 605.2 110.4 5.50.2 149.4 0.0 108.0 15592.2 110.4 5.50.1 106.2 113.9 0.0 108.0 15592.2 110.4 5.50.1 106.2 113.9 0.0 100.0 100.0 84.6 33.5 21.4 0.0 100.0 100.0 84.6 33.5 21.4 0.0 100.0 100.0 84.6 33.5 21.4 0.0 100.0 100.0 84.6 33.5 21.4 0.0 100.0 100.0 84.6 33.5 21.4 0.0 100.0 100.0 84.6 33.5 21.4 0.0 100.0 100.0 84.6 10.0 11 100.0 1			532.1	345.8	0.0	877	6531.0	6204.4	6256.
905.7 532.1 345.8 0.0 67.0 6531.0 437.3 394.8 17.5 0.0 66.0 437.3 394.8 17.5 0.0 66.0 416.0 69.4 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 93.0 15292.2 110.3 39.2 69.1 0.0 985.0 126.3 110.3 39.2 69.1 0.0 985.0 126.3 110.3 39.2 69.1 0.0 985.0 126.3 110.3 39.2 69.1 0.0 631.0 1733.7 2313.5 1062.7 1139.9 0.0 2202.0 13131.4 626.6 332.1 349.4 0.0 6292.0 1733.7 110.3 39.2 69.1 0.0 0.0 173.0 6522.2 35.0 18.0 13.9 0.0 109.0 15292.2 35.0 18.0 13.9 0.0 15292.2 35.0 18.0 13.9 0.0 15292.2 35.0 18.0 13.9 0.0 15292.2 35.0 18.0 13.9 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 13.9 0.0 15292.2 35.0 18.0 13.9 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 18.0 19.0 0.0 15292.2 35.0 19.0 0.0 15292.2 35.0 19.0 0.0 15292.2 35.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0 0.0 15292.2 35.0 19.0 0.0 19.0	417.3 345.8 0.0 047  417.5 0.0 416  417.3 3994.8 17.5 0.0 416  70.9 24.7 43.4 0.0 68  70.9 24.7 43.4 0.0 68  70.9 24.7 43.4 0.0 68  70.9 24.7 43.4 0.0 68  70.9 24.7 43.4 0.0 68  110.3 39.2 69.1 0.0 108  99.5 65.8 27.4 0.0 985  110.3 39.2 69.1 0.0 985  135.7 50.6 79.6 0.0 985  1678.5 346.8 36.8 0.0 1660  2313.5 166.7 139.9 0.0 1660  2313.5 166.8 345.8 0.0 108  110.3 39.2 69.1 0.0 108  2313.5 166.8 36.6 36.8 0.0 877  110.3 39.2 69.1 0.0 877  110.3 39.2 69.1 0.0 877  110.3 39.2 69.1 0.0 877  2313.5 166.8 33.5 21.4 0.0 5.8  24.1 Bulk (in MT)  25.5 56.6 33.5 21.4 0.0 5.8  25.5 56.6 32.6 5.8  26.6 56.6 32.6 5.8  27.7 60.0 3.1  27.7 60.0 3.1  27.7 60.0 3.1  27.7 60.0 3.1  27.7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	905.7 532.1 345.8 0.0 A77.0 6531.0 417.3 J994.8 17.5 0.0 416.0 69.4 437.3 J994.8 17.5 0.0 416.0 69.4 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 68.0 11096.3 70.9 24.7 43.4 0.0 108.0 15292.2 70.9 110.3 39.2 69.1 100.0 332.0 1201.4 70.0 201.9 13.9 0.0 108.0 15292.2 70.0 100.3 39.2 69.1 109.0 109.0 15292.2 70.0 100.3 39.2 69.1 109.0 109.0 15292.2 70.0 100.3 39.2 69.1 109.0 1		.7	532.1	345.8	0.0	877.0	6531.0	6204.4	6256.
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437.3 399.8 17.5 0.0 416.0 66.4  437.3 399.8 17.5 0.0 69.0 1096.3  70.9 24.7 43.4 0.0 69.0 1096.3  70.9 24.7 43.4 0.0 69.0 1096.3  70.9 24.7 43.4 0.0 69.0 1096.3  110.3 39.2 69.1 0.0 108.0 15292.2  110.3 39.2 69.1 0.0 108.0 15292.2  110.3 39.2 69.1 0.0 108.0 15292.2  135.1 116.3 39.2 69.1 0.0 108.0 15292.2  135.2 69.1 0.0 0.0 108.0 15292.2  135.3 1312.3 0.0 130.0 130.0 130.0 130.0  22313.5 1062.7 113.9 0.0 130.0 17353.7  40.0 100.0 112.4 0.0 183.0 0.0 131.0 6531.0  110.3 39.2 69.1 0.0 13.9 0.0 131.0 6531.0  110.3 39.2 149.4 0.0 131.0 6531.0  156.6 33.5 21.4 0.0 190.0  13.0 6295.9  13.0 18.0 13.9 0.0 109.0 15292.2  135.0 18.0 13.9 0.0 109.0 15292.2  135.0 18.0 13.9 0.0 109.0 15292.2  135.0 18.0 13.9 0.0 109.0 15292.2  135.0 18.0 13.9 0.0 109.0 15292.2  135.0 18.0 13.9 0.0 109.0 15292.2  135.0 18.0 13.9 0.0 109.0 15292.2  140.4 47.0 0.0 54.0 1900.9  56.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 65.0 1900.9  58.6 33.5 21.4 0.0 65.0 1900.9  58.6 100.0 1900.9  58.6 100.0 1900.9  58.6 100.0 1900.9  58.7 0 1900.9  58.8 10.0 MT)  Account (in MT)	437.3 399.8 17.5 0.0 416  437.3 399.8 17.5 0.0 416  70.9 24.7 43.4 0.0 68  70.9 24.7 43.4 0.0 68  70.9 24.7 43.4 0.0 68  70.9 24.7 43.4 0.0 68  110.3 39.2 69.1 0.0 108  110.3 39.2 69.1 0.0 108  135.7 50.6 79.6 0.0 985  145.8 345.1 116.7 215.5 0.0 180  1014.4 559.1 426.6 0.0 985  1014.4 559.1 149.4 0.0 2202  847.1 628.2 1139.9 0.0 187  135.0 18.0 13.9 0.0 88  135.0 18.0 13.9 0.0 88  258.6 33.5 21.4 0.0 0.0 84  58.6 33.5 21.4 0.0 5.6  58.6 32.6 32.6 32.6 32.6  58.6 32.6 32.6 32.6 32.6  58.6 32.6 32.6 32.6 32.6  58.6 32.6 32.6 32.6 32.6 32.6  58.6 32.6 32	## ## ## ## ## ## ## ## ## ## ## ## ##			3.88.8	17.5	0.0	416.0	4.69		65.
## 17.3 ## 17.5 ## 17.5 ## 16.0 ## 16.0 ## 16.0 ## 17.5 ## 17.	437.3 399.8 17.5 0.0 415 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 110.3 39.2 69.1 0.0 108 39.2 69.1 0.0 108 345.1 116.7 215.5 0.0 983 135.7 65.8 27.4 0.0 983 1678.5 348.3 1312.3 0.0 1669 469.0 546.6 13.9 0.0 2202 847.1 628.2 149.4 0.0 2202 847.1 628.2 149.4 0.0 108 35.0 18.0 13.9 0.0 887 110.3 39.2 69.1 0.0 887 110.3 39.2 69.1 0.0 888 23.3 18.0 13.9 0.0 888 25.6 41.4 47.0 0.0 888 25.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 33.5 21.4 0.0 55 25.6 58.6 58.6 59.6 33.5 21.4 0.0 55 25.6 58.6 59.6 33.5 21.4 0.0 55 25.6 58.6 59.6 33.5 21.4 0.0 55 25.6 58.6 59.6 33.5 21.4 0.0 55 25.6 58.6 59.6 59.6 59.6 59.6 59.6 59.6 59.6 59	437.3 394.8 17.5 0.0 64.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 110.3 39.2 69.1 0.0 108.0 1529.2 110.3 39.2 69.1 0.0 108.0 1529.2 110.3 39.2 69.1 0.0 108.0 1529.2 135.1 116.7 215.5 0.0 33.0 126.3 135.1 16.7 215.5 0.0 33.0 126.3 135.1 16.7 215.5 0.0 33.0 126.3 101.4 559.1 426.6 0.0 98.0 1763.7 291.5 53.0 119.7 39.1 0.0 120.0 1753.7 291.5 53.1 149.4 0.0 168.0 1753.7 291.6 53.2 149.4 0.0 168.0 1759.2 35.0 18.0 13.9 0.0 69.0 1759.2 35.0 18.0 13.9 0.0 69.0 1900.9 25.6 33.5 21.4 0.0 6.0 54.0 1900.9 25.6 33.5 21.4 0.0 5.0 554.0 1900.9 25.6 33.5 21.4 0.0 5.0 54.0 1900.9 25.6 33.5 21.4 0.0 5.0 54.0 1900.9 25.6 33.5 21.4 0.0 5.0 54.0 1900.9 25.6 33.5 21.4 0.0 5.0 554.0 1900.9 25.6 33.5 21.4 0.0 5.0 554.0 1900.9 25.6 34.0 1900.9 25.6 33.5 21.4 0.0 5.0 554.0 1900.9 25.6 34.0 1900.9 25.6 34.0 1900.9 25.7 11.4 0.0 11.4 0.0 5quare		.3	398.8	17.5	0.0	416.0	9.69	0.49	• ya
70.9 24.7 43.4 0.0 64.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 110.3 39.2 69.1 0.0 0.0 1529.2 39.5 6.5 69.1 0.0 0.0 1529.2 110.3 39.2 69.1 0.0 0.0 1529.2 110.4 559.1 42.4 0.0 945.0 128.3 110.4 559.1 1312.3 0.0 146.0 2312.4 110.3 39.2 149.4 0.0 166.0 2312.4 110.3 39.2 69.1 0.0 166.0 2312.4 110.3 39.2 69.1 0.0 166.0 2312.4 110.3 39.2 69.1 0.0 177.0 16832.0 110.3 39.2 69.1 0.0 177.0 16832.0 110.3 39.2 69.1 0.0 109.0 15292.2 110.3 39.2 69.1 0.0 109.0 15292.2 110.3 39.2 69.1 0.0 109.0 15292.2 110.3 39.5 12.4 0.0 190.0 1900.9 110.4 (In MT)  anizational Maintenance Activity (OMA) for 8 Total Constrained	70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 110.3 39.2 69.1 0.0 108 10.3 39.2 69.1 0.0 108 135.7 65.8 27.4 0.0 988 135.7 50.6 77.6 0.0 988 1678.5 348.3 1312.3 0.0 1860 2313.5 166.7 1139.9 0.0 2202 847.1 628.2 1149.4 0.0 2202 847.1 628.2 1149.4 0.0 108 15.0 18.0 13.9 0.0 817 10.3 39.2 69.1 0.0 818 15.0 18.0 13.9 0.0 818 15.0 18.0 13.9 0.0 818 15.0 18.0 13.9 0.0 818 15.0 18.0 13.9 0.0 818 15.0 18.0 13.9 0.0 818 15.0 18.0 173.9 0.0 88 15.	70.9 24.7 43.4 0.0 64.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 70.9 24.7 43.4 0.0 65.0 1096.3 110.3 39.2 69.1 0.0 0.0 1529.2 39.5 69.1 106.0 1529.2 213.5 50.6 77.6 0.0 133.0 126.1 213.5 50.6 77.6 0.0 332.0 126.1 213.5 106.2 7 149.4 0.0 332.0 126.3 213.5 106.2 7 149.4 0.0 34.0 177.0 16832.0 220.2 312.1 349.4 0.0 131.0 6232.0 35.0 18.0 13.9 0.0 131.0 6295.9 35.0 18.0 13.9 0.0 131.0 6295.9 35.0 18.0 13.9 0.0 1095.0 15292.2 35.0 18.0 13.9 0.0 1095.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 35.0 18.0 13.9 0.0 1096.9 33.5 21.4 0.0 0.0 54.0 1900.9 34.0 1900.9 34.0 10.0 10.0 1900.9 35.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 1		.3	398.8	17.5	0.0	415.0	4.69	64.0	. 66.
70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 70.9 24.7 43.4 0.0 68.0 1096.3 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 135.1 116.7 215.5 0.0 33.0 1361.4 135.7 50.6 72.6 0.0 33.0 1361.4 135.7 50.6 72.6 0.0 136.0 17361.7 60.0 52.0 110.3 1312.3 0.0 0.0 1760.0 17363.7 2213.5 1062.7 1139.9 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 0.0 177.0 16832.0 110.3 39.2 69.1 0.0 0.0 177.0 16832.0 110.3 39.2 69.1 0.0 0.0 108.0 15292.2 14.0 13.9 0.0 108.0 15292.2 15.0 18.0 13.9 0.0 108.0 15292.2 15.0 18.0 13.9 0.0 1090.9 13.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 56.0 54.0 1900.9 58.6 33.5 21.4 0.0 56.0 54.0 1900.9	70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 68 70.9 24.7 43.4 0.0 69 70.9 24.7 43.4 0.0 69 110.3 39.2 69.1 0.0 108 110.3 39.2 69.1 0.0 108 39.2 69.1 0.0 985 135.7 50.6 79.6 0.0 985 1014.4 559.1 10.3 348.3 1312.3 0.0 166 2313.5 106.2 7 113.9 0.0 108 2313.5 18.0 13.9 0.0 108 35.0 18.0 13.9 0.0 108 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 173.9 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 35.0 18.0 0.0 88 36.1 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 37.0 18.0 0.0 88 38.0 18.0 0.0 8	70.9 24.7 43.4 0.0 68.0 1096.3   70.9 24.7 43.4 0.0 68.0 1096.3   70.9 24.7 43.4 0.0 69.0 1096.3   70.9 24.7 43.4 0.0 69.0 1096.3   70.9 24.7 43.4 0.0 69.0 1096.3   70.9 24.7 43.4 0.0 0.0 1096.0 15292.2   110.3 39.2 69.1 0.0 0.0 15292.2   110.3 39.2 69.1 0.0 0.0 15292.2   135.7 21.5 0.0 0.0 33.2 0 156.14   79.6 0.0 33.2 0 126.1   101.4 550.6 76.6 0.0 33.2 0 126.1   79.6 0.0 33.2 0 126.1   79.6 0.0 33.2 0 126.1   79.6 0.0 33.2 0 126.1   79.6 0.0 33.2 0 126.1   79.6 0.0 33.2 0 126.1   70.6 0.0 33.2 0 126.1   70.6 0.0 33.2 0 126.1   70.6 0.0 0 126.1    70.6 0.0 0 1 70.6 0.0 0 1 70.6 0.0 0 1 70.6 0		0	24.7	43.4	0.0	68.0	1096.3	986.6	.506
70.9 24.7 43.4 0.0 69.0 1096.3 70.9 24.7 43.4 0.0 69.0 1096.3 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 39.5 65.8 27.4 0.0 133.0 15292.2 135.7 50.6 215.5 0.0 332.0 126.11.4 1014.4 559.1 426.6 0.0 596.0 23015.7 2313.5 1062.7 113.9 0.0 108.0 1753.7 2313.5 106.2 149.4 0.0 31.0 653.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 1095.8 35.0 18.0 13.9 0.0 1095.8 35.0 18.0 13.9 0.0 1095.8 35.0 18.0 13.9 0.0 1095.8 35.0 18.0 13.9 0.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9	70.9 24.7 43.4 0.0 69 70.9 24.7 43.4 0.0 69 110.3 39.2 69.1 0.0 108 110.3 39.2 69.1 0.0 108 345.1 116.7 215.5 0.0 332 1014.4 559.1 426.6 0.0 988 1678.3 345.8 0.0 988 2313.5 1062.7 1139.9 0.0 2202 847.1 628.2 149.4 0.0 2202 847.1 628.2 149.4 0.0 1877 110.3 39.2 69.1 0.0 1877 905.7 532.1 345.8 0.0 877 110.3 39.2 69.1 0.0 1877 110.3 39.2 69.1 0.0 1877 110.3 33.5 21.4 0.0 5.4 58.6 33.5 21.4 0.0 5.4 58.6 33.5 21.4 0.0 5.4 58.6 33.5 21.4 0.0 5.4 58.6 33.5 21.4 0.0 5.4 58.6 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 33.5 21.4 0.0 5.4 58.7 34.7 34.7 34.7 34.7 34.7 34.7 34.7 34	70.9 24.7 43.4 0.0 69.0 1096.3 70.9 24.7 43.4 0.0 109.0 1096.3 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 110.3 39.2 69.1 0.0 108.0 15292.2 345.1 116.7 215.5 0.0 932.0 15491.4 1014.4 559.1 426.6 0.0 945.0 23015.7 2313.5 1062.7 1139.9 0.0 1660.0 23115.7 628.2 149.4 0.0 177.0 16832.0 110.3 39.2 69.1 0.0 177.0 15832.0 110.3 39.2 69.1 0.0 177.0 15832.0 110.3 39.2 69.1 0.0 177.0 15832.0 110.3 39.2 69.1 0.0 177.0 15832.0 110.3 39.2 69.1 0.0 177.0 15832.0 110.3 39.2 69.1 0.0 177.0 15832.0 110.3 39.2 69.1 0.0 177.0 15932.0 110.3 39.5 21.4 0.0 190.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9		6	24.7	43.4	0.0	68.0	1096.3	9.96.6	.806
1000.3   1	110.3 39.2 69.1 0.0 108 110.3 39.2 69.1 0.0 108 110.3 39.2 69.1 0.0 108 110.3 39.2 69.1 0.0 108 345.1 116.7 215.5 0.0 133 135.7 50.6 79.6 0.0 988 1678.5 348.3 1312.3 0.0 1660 2313.5 1062.7 1139.9 0.0 2202 847.1 628.2 149.4 0.0 2202 847.1 628.2 149.4 0.0 2202 110.3 39.2 69.1 0.0 131 110.3 39.2 69.1 0.0 131 110.3 39.2 69.1 0.0 131 110.3 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 55 54 55.7 TATILITY THE T	100.3   39.2   69.1   108.0   15292.2     110.3   39.2   69.1   00.0   108.0   15292.2     110.3   39.2   69.1   00.0   108.0   15292.2     110.3   39.2   69.1   00.0   108.0   15292.2     110.3   39.2   69.1   00.0   108.0   15292.2     135.1   116.7   215.5   00.0   33.0   126.14     140.4   55.9   79.6   00.0   33.0   23312.4     1578.5   348.3   131.3   00.0   336.0   23312.4     1678.5   348.3   131.3   00.0   310.0   23312.4     1678.5   348.3   131.3   00.0   310.0   23312.4     1678.5   348.3   345.4   00.0   310.0   653.2     167.1   628.2   143.4   00.0   31.0   605.2     167.1   18.0   13.9   00.0   31.0   605.2     18.0   13.9   00.0   31.0     18.0   13.9   00.0   31.0     18.0   13.0   00.0   31.0     18.0   13.0   00.0   31.0     18.0   13.0   00.0   31.0     18.0   13.0   00.0   31.0     18.0   13.0   00.0   31.0     18.0   13.0   00.0   31.0     18.0   13.0   00.0   31.0     18.0   13.0   00.0   31.0     18.0   13.0   00.0     18.0   13.0   00.0     18.0   13.0   00.0     18.0   13.0		6	24.7	43.4	0.0	69.0	1096.3	9.986	.566
110.3   39.2   69.1   0.0   108.0   15292.2     110.3   39.2   69.1   0.0   108.0   15292.2     110.3   39.2   69.1   0.0   108.0   15292.2     110.3   39.2   69.1   0.0   108.0   15292.2     110.3   39.2   69.1   0.0   108.0   126.31.4     1345.1   116.7   215.5   0.0   33.0   126.31.4     135.7   50.6   79.6   0.0   945.0   426.8     1678.5   348.3   1332.3   0.0   136.0   23015.7     460.0   546.6   341.8   0.0   2202.0   31214.4     460.0   13.9   0.0   1736.3     110.3   39.2   69.1   0.0   1736.3     110.3   39.2   69.1   0.0   131.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   41.4   4.7   0.0   34.0   1900.9     58.6   33.5   21.4   0.0   54.0   1900.9     58.6   21.4   0.0   54.0   1900.9     58.6   21.4   0.0   54.0   1900.9     58.6   21.4   0.0   54.0   1900.9     58.6   21.4   0.0   54.0   1900.9     58.6   21.4   0.0   54.0   1900.9     58.6   21.4   0.0   54.0   1900.9     58.6   21.4   0.0   54.0   1900.9     58.6   2	110.3   39.2   69.1   0.0   108   110.3   110.3   39.2   69.1   0.0   109   110.3   110.3   39.2   69.1   0.0   109   109   109   345.1   116.7   215.5   0.0   332   345.1   116.7   215.5   0.0   332   345.1   116.7   215.5   0.0   346.	110.3   39.2   69.1   00.0   15292.2     110.3   39.2   69.1   00.0   15292.2     110.3   39.2   69.1   00.0   15292.2     110.3   39.2   69.1   00.0   15292.2     110.4   55.4   70.6   0.0   33.2   15292.2     101.4   55.4   70.6   0.0   33.2   15292.2     101.4   55.4   70.6   0.0   9.5   0.0   23312.4     101.4   55.4   131.2   0.0   1750.1     101.4   55.4   131.2   0.0   1750.1     101.4   55.4   131.2   0.0   1750.1     101.4   55.4   113.4   0.0   1770   16332.0     2311.5   106.7   113.4   0.0   1770   16332.0     100.3   39.2   140.4   0.0   1770   16332.0     100.3   39.2   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     39.6   33.5   21.4   0.0   54.0   1900.9     58.6   39.6   39.6   39.6   39.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6   30.6		•	24.7	43.4	0.0	68.0	1096.3	984.6	663.
110.3   39.2   69.1   0.0   108.0   15292.2     110.3   39.2   69.1   0.0   108.0   15292.2     110.3   39.2   69.1   0.0   108.0   15292.2     110.4   345.1   116.7   215.5   0.0   332.0   12431.4     1135.7   50.6   79.6   0.0   988.0   12431.4     1014.4   559.1   426.5   0.0   988.0   17363.7     2313.5   1062.7   1130.4   0.0   987.0   17363.7     407.1   628.2   149.4   0.0   177.0   15832.0     110.3   39.2   69.1   0.0   177.0   0531.0     110.3   39.2   69.1   0.0   177.0   0531.0     110.3   39.2   69.1   0.0   177.0   0531.0     110.3   39.2   69.1   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   33.5   21.4   0.0   54.0   1900.9     58.6   58.6   28.6   28.6   28.6   28.6   28.6     59.6   50.6   50.6   50.0   50.0   50.0   50.0     58.6   50.6   50.0   50.0   50.0   50.0   50.0   50.0   50.0   50.0   50.0   50.0   50.0   50.	110.3   39.2   69.1   0.0   108     110.3   39.2   69.1   0.0   108     345.1   116.7   215.5   0.0   332     135.7   50.6   79.6   0.0   332     1014.4   559.1   426.6   0.0   948     1014.4   559.1   426.6   0.0   948     1014.4   559.1   1312.3   0.0   968     2313.5   1062.7   1139.9   0.0   2202     47.1   628.2   149.4   0.0   2202     40.2   110.3   39.2   69.1   0.0   108     35.0   18.0   13.9   0.0   31     35.0   18.0   13.9   0.0   31     35.0   18.0   13.9   0.0   31     35.0   33.5   21.4   0.0   54     58.6   33.5   21.4   0.0   64     58.6   33.5   21.4   0.0   64     58.6   33.5   21.4   0.0   64     58.6   33.5   21.4   0.0   64     58.6   33.5   21.4   0.0   64     58.6   33.5   21.4   0.0   64     58.6   33.5   21.4   0.0   64     58.6   33.5   21.4   0.0     58.6   33.5   21.4   0.0     58.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.0     59.6   33.5   21.4   0.	1100.3   399.2   699.1   0.0   108.0   15292.2     1100.3   399.2   699.1   0.0   108.0   15292.2     199.5   65.8   27.4   0.0   93.0   106.1     135.7   559.1   470.6   0.0   985.0   4426.9     1678.5   348.3   1312.3   0.0   985.0   126.31.4     1678.5   348.3   1312.3   0.0   985.0   126.31.4     1678.5   348.3   1312.3   0.0   985.0   1273.1     1678.5   348.3   1312.3   0.0   985.0   1313.4     110.3   349.8   0.0   2202.0   1313.4     110.3   349.8   0.0   2202.0   1313.4     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   131.0   605.2     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   349.8   0.0   141.0     110.3   141.0   141.0     110.3   141.0   141.0     110.3   141.0   141.0     110.3   141.0   141.0     110.3   141.0   141.0     110.3   141.0   141.0     110.3   141.0     110.3   141.0   141.0     110.3   141.0		5	39.2	1.69	0.0	108.0	15292.2	14527.6	14649.
110.3 39.2 69.1 0.0 108.0 15292.2 345.1 165.6 27.4 0.0 932.0 126.31.4 135.7 50.6 79.6 0.0 932.0 126.31.4 135.7 50.6 79.6 0.0 945.0 126.31.4 1014.4 559.1 420.6 0.0 945.0 4426.9 1014.4 559.1 1139.9 0.0 1660.0 17363.7 2313.5 1062.7 1139.9 0.0 1660.0 17363.7 2313.5 1062.7 1139.9 0.0 1680.0 17363.2 905.7 532.1 345.8 0.0 877.0 16832.0 110.3 39.2 69.1 0.0 108.0 15292.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 1090.0 1900.9 55.6 41.4 47.0 0.0 54.0 1900.9 56.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.7 0.0 54.0 1900.9 58.8 59.8 59.8 59.0 1900.9 58.9 58.0 59.0 1900.9 58.0 59.0 54.0 1900.9 58.0 54.	110.3 39.2 69.1 0.0 108 349.5 65.8 27.4 0.0 933 135.7 50.6 79.6 0.0 985 1014.4 559.1 426.6 0.0 985 2313.5 1062.7 1139.9 0.0 2202 847.1 628.2 149.4 0.0 2202 847.1 628.2 149.4 0.0 277 110.3 39.2 69.1 0.0 108 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 88 39.8 41.4 47.0 0.0 88 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54	110.3   19.2   69.1   0.0   108.0   15292.2     135.7   215.5   0.0   332.0   12631.4     135.7   215.5   0.0   332.0   12631.4     135.7   20.6   20.0   23312.4     1014.4   559.1   420.6   0.0   968.0   23312.4     1014.4   559.1   420.6   0.0   968.0   17363.7     1678.5   348.3   1312.3   0.0   1660.0   23015.7     2313.5   1062.7   1139.9   0.0   2202.0   17363.7     2313.5   1062.7   1139.9   0.0   177.0   6531.0     110.3   39.2   69.1   0.0   31.0   6652.2     35.0   18.0   13.9   0.0   31.0   6652.2     35.0   18.0   13.9   0.0   31.0   6652.2     35.0   18.0   13.9   0.0   31.0   6652.2     35.0   18.0   13.9   0.0   31.0   6652.2     35.0   18.0   13.9   0.0   31.0   6652.2     35.0   33.5   21.4   0.0   54.0   1900.9     58.6   38.6			39.5	69.1	0.0	108.0	15292.2	14527.6	14649.
100   100	199.5 65.8 27.4 0.0 933 135.7 50.6 79.6 0.0 332 135.7 50.6 79.6 0.0 985 1678.5 148.3 1312.3 0.0 1660 2313.5 1062.7 1139.9 0.0 2202 847.1 628.2 149.4 0.0 2202 847.1 628.2 149.4 0.0 2202 110.3 39.2 69.1 0.0 108 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 88 35.0 18.0 13.9 0.0 88 398.1 201.9 173.9 0.0 88 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.7 10 MT)	99.5 65.8 27.4 0.0 33.20 1961.4  135.7 50.6 79.6 0.0 33.20 126.31.4  135.7 50.6 79.6 0.0 33.20 126.31.4  1014.4 559.1 426.6 0.0 965.0 4426.8  1678.5 348.3 1312.3 0.0 1660.0 23015.7  669.0 540.0 1312.3 0.0 1660.0 23015.7  62313.5 1062.7 1139.9 0.0 31214.4  647.1 628.2 149.4 0.0 168.0 15292.2  35.0 18.0 13.9 0.0 31.0 6.55.2  35.0 18.0 13.9 0.0 31.0 6.05.2  35.0 18.0 13.9 0.0 31.0 6.05.2  35.0 18.0 13.9 0.0 108.0 6295.9  39.1 201.9 173.9 0.0 1906.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 34.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 34.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.6 33.5 21.4 0.0 54.0 1900.9  58.7 3 3 3 5 21.4 0.0 1900.9  58.8 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		7	39.5	1.69	0.0	108.0	15292.2	14527.6	14649.
135.1   116.7   215.5   0.0   332.0   126.311.4     135.7   215.5   0.0   332.0   126.311.4     1014.4   559.1   426.6   0.0   945.0   23312.4     1678.5   348.3   1312.3   0.0   1660.0   23015.7     2313.5   546.6   361.8   0.0   2202.0   31214.4     847.1   628.2   149.4   0.0   2202.0   31214.4     905.7   532.1   345.8   0.0   877.0   6531.0     110.3   39.2   69.1   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   18.0   13.9   0.0   31.0   605.2     35.0   33.5   21.4   0.0   54.0   1900.9     58.6   33.5   21.4   0.0   21.0   21.0     58.6   28.6   28.6   28.6   28.6	135.7 50.6 3328  135.7 50.6 79.6 0.0 130  1014.4 559.1 426.6 0.0 983  1677. 213.3 0.0 1660  2313.5 1062.7 1139.9 0.0 2202  847.1 628.2 149.4 0.0 2202  1100.3 39.2 69.1 0.0 177  1100.3 39.2 69.1 0.0 177  1100.3 39.2 69.1 0.0 177  1100.3 39.2 69.1 0.0 108  135.0 18.0 13.9 0.0 31  25.0 18.0 13.9 0.0 31  25.6 41.4 47.0 0.0 37  58.6 33.5 21.4 0.0 54  58.6 33.5 21.4 0.0 54  58.6 33.5 21.4 0.0 54  58.6 33.5 21.4 0.0 54  58.6 33.5 21.4 0.0 54  58.7 33.5 21.4 0.0 54  58.7 33.5 21.4 0.0 54  58.7 33.5 21.4 0.0 54  58.7 33.5 21.4 0.0 55  58.7 33.5 21.4 0.0 55  58.7 33.5 21.4 0.0 55  58.7 33.5 21.4 0.0 55  58.7 33.5 21.4 0.0 55  58.7 33.5 21.4 0.0 55  58.7 34.7 34.7 34.7 34.7 34.7 34.7 34.7 34	135.1 116.7 215.5 0.0 332.0 126.31.4 135.1 116.7 215.5 0.0 332.0 126.31.4 1014.4 559.1 426.6 0.0 948.0 23312.4 1678.5 348.3 1312.3 0.0 1660.0 23015.7 2313.5 1062.7 1139.9 0.0 2202.0 1736.37 2313.5 1062.7 149.4 0.0 2202.0 1736.37 110.3 39.2 69.1 0.0 877.0 6531.0 110.3 39.2 69.1 0.0 877.0 6531.0 135.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 108.0 15292.2 35.0 18.0 13.9 0.0 15292.2 35.0 18.0 13.9 0.0 108.0 15292.2 35.0 18.0 13.9 0.0 15292.2 35.0 18.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19		۲.	65.8	27.4	0.0	93.0	1961.4	1765.2	1780.
135.7   50.6   79.6   9.0   130.9   23312.4     1014.4   559.1   426.6   9.0   965.0   4426.8     1678.5   348.3   1312.3   9.0   1660.0   17363.7     2313.5   1062.7   1139.9   9.0   17363.7     240.6   546.6   1139.9   9.0   17363.7     110.3   39.2   149.4   9.0   108.0   15292.2     150.0   18.0   13.9   9.0   31.0   605.2     35.0   18.0   13.9   9.0   31.0   605.2     35.0   18.0   13.9   9.0   31.0   605.2     35.0   18.0   13.9   9.0   31.0   605.2     35.0   18.0   13.9   9.0   31.0   605.2     35.0   33.5   21.4   9.0   54.0   1900.9     58.6   21.4   9.0   21.4   9.0     58.6   21.4   9	135.7 50.6 79.6 130 135.7 50.6 79.6 130 1014.4 559.1 426.6 0.0 988 1678.3 348.3 1312.3 0.0 1660 2313.5 1062.7 1139.9 0.0 2202 847.1 628.2 149.4 0.0 2202 847.1 628.2 149.4 0.0 2202 35.0 18.0 13.9 0.0 131 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 888 35.0 18.0 13.9 0.0 888 35.0 18.0 13.9 0.0 888 35.0 18.0 13.9 0.0 888 35.0 18.0 13.9 0.0 888 35.0 18.0 173.9 0.0 888 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.7 33.5 21.4 0.0 54 58.7 33.5 21.4 0.0 54 58.7 33.5 21.4 0.0 54 58.7 33.5 21.4 0.0 54 58.7 33.5 21.4 0.0 54 58.7 33.5 21.4 0.0 54	1014.4 559.1 79.6 0.0 130.0 23312.4 1014.4 559.1 426.6 0.0 986.0 4426.8 1678.5 348.3 1312.3 0.0 986.0 17363.7 2313.5 1062.7 1139.9 0.0 2202.0 31214.4 847.1 628.2 149.4 0.0 2202.0 31214.4 847.1 628.2 149.4 0.0 108.0 15292.2 35.0 18.0 13.9 0.0 108.0 15292.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 173.9 0.0 31.0 605.2 35.0 18.0 173.9 0.0 190.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 50.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9			116.7	215.5	0.0	332.0	12631.4	11368.3	11463.
1014.4 559.1 426.6 0.0 985.0 4426.8 496.6 0.0 1660.0 23015.7 960.0 1736.37 960.0 1736.37 960.0 1736.37 960.0 1736.37 960.0 1736.37 960.0 1736.37 960.0 1736.37 960.0 1736.37 960.0 1736.37 960.0 1736.37 960.0 177.0 16832.0 1100.3 39.2 69.1 0.0 0.0 877.0 6531.0 6531.0 160.0 150.0 177.0 16832.0 95.6 41.4 47.0 0.0 31.0 665.2 95.6 41.4 47.0 0.0 31.0 665.2 95.6 41.4 47.0 0.0 88.0 62.95.9 95.6 41.4 47.0 0.0 88.0 62.95.9 95.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 95.0 97.0 1700.9 95.0 97.0 97.0 97.0 97.0 97.0 97.0 97.0 97	1014.4 559.1 426.6 0.0 948 1678.5 348.3 1312.3 0.0 1660 2313.5 1062.7 1139.9 0.0 2202 847.1 628.2 149.4 0.0 2202 110.3 39.2 69.1 0.0 177 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 35.0 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.7 0 0.0 375 58.6 33.5 21.4 0.0 54 58.7 0 0.0 54 58.7 0 0.0 54 58.7 0 0.0 54 58.7 0 0.0 54 58.8 0 0.0 54 58.8 0 0.0 54 58.8 0 0.0 54	1014.4   559.1   426.6   0.0   945.0   4426.8			20.00	9.67	0.0	130.0	23312.4	20981.1	21166.
1678.5 348.3 1312.3 0.0 1660.0 23015.7 2313.5 140.4 0.0 0.0 0.0 0.0 17363.7 24313.5 1628.2 149.4 0.0 0.0 0.0 177.0 16832.0 1100.3 39.2 69.1 0.0 0.0 0.0 177.0 16832.0 1100.3 39.2 69.1 0.0 0.0 0.0 177.0 16832.0 168.0 13.9 0.0 0.0 177.0 16832.0 155.0 18.0 13.9 0.0 0.0 177.0 16832.0 18.0 13.9 0.0 0.0 177.0 1695.2 235.0 18.0 13.9 0.0 0.0 17.0 605.2 35.0 18.0 13.9 0.0 0.0 175.0 1095.2 21.4 0.0 0.0 175.0 1095.0 1090.0 256.6 33.5 21.4 0.0 0.0 54.0 1900.0 256.6 33.5 21.4 0.0 0.0 54.0 1900.0 256.6 33.5 21.4 0.0 0.0 54.0 1900.0 256.6 33.5 21.4 0.0 0.0 54.0 1900.0 256.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	1678.5 348.3 1312.3 0.0 1660 2313.5 166.5 361.8 0.0 908 2313.5 1662.7 1139.9 0.0 2202 847.1 628.2 149.4 0.0 777 905.7 532.1 345.8 0.0 877 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 88 398.1 201.9 173.9 0.0 88 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 58.7 38.8 33.5 21.4 0.0 54 58.7 38.8 33.5 21.4 0.0 54 58.8 33.5 21.4 0.0 54 58.8 33.5 21.4 0.0 54 58.8 33.5 21.4 0.0 54 58.8 33.5 21.4 0.0 54 58.8 33.5 21.4 0.0 54	1678.5 348.3 1312.3 0.0 1660.0 233115.7 2313.5 1062.7 1139.9 0.0 1777.0 16832.0 2905.7 532.1 345.8 0.0 2202.0 31214.4 110.3 39.2 69.1 0.0 877.0 6531.0 110.3 39.2 69.1 0.0 675.2 35.0 18.0 13.9 0.0 675.2 35.0 18.0 13.9 0.0 675.2 35.0 18.0 13.9 0.0 108.0 655.2 35.0 18.0 13.9 0.0 108.0 15292.2 35.0 18.0 13.9 0.0 108.0 15292.2 35.0 18.0 13.9 0.0 108.0 15292.2 35.0 18.0 13.9 0.0 108.0 1900.9 398.1 201.9 173.9 0.0 88.0 6295.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9		4	1.655	456.6	0.0	985.0	4426.8	45024	4240.
2313.5 1062.7 1139.9 0.0 2202.0 17353.7 1622.2 1139.9 0.0 2202.0 17353.7 1622.2 149.8 0.0 2202.0 1771.0 16832.0 1905.7 532.1 345.8 0.0 877.0 16832.0 1622.2 139.2 69.1 0.0 177.0 16832.0 15292.2 18.0 13.9 0.0 177.0 16832.0 15292.2 18.0 13.9 0.0 177.0 16832.0 15292.2 18.0 13.9 0.0 177.0 1695.2 18.0 13.9 0.0 177.0 1695.2 18.0 13.9 0.0 177.0 1695.2 177.0 1695.2 177.0 1695.2 177.0 1695.2 177.0 1695.2 177.0 1695.2 177.0 1695.2 177.0 1695.2 177.0 1695.3 177.0 1695.2 177.0 1695.2 177.0 1695.2 177.0 1695.3 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0 177.0	## 139.5   546.6   361.8   0.0   908    ## 2313.5   1062.7   1139.9   0.0   2202    ## 247.1   532.1   345.8   0.0   177    ## 25.0   18.0   13.9   0.0   31    ## 25.0   18.0   13.9   0.0   31    ## 25.0   18.0   13.9   0.0   31    ## 25.0   18.0   13.9   0.0   31    ## 25.0   41.4   47.0   0.0   88    ## 26.6   33.5   21.4   0.0   54    ## 26.6   33.5   21.4   0.0   54    ## 26.6   33.5   21.4   0.0   54    ## 26.6   33.5   21.4   0.0   54    ## 26.6   33.5   21.4   0.0   54    ## 26.6   33.5   21.4   0.0   54    ## 26.6   33.5   21.4   0.0    ## 26.6   33.5   21.4   0.0    ## 26.6   33.5   21.4   0.0    ## 26.6   33.5   21.4    ## 26.6   33.5   21.4    ## 26.6   33.5   21.4    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6   33.5    ## 26.6    ## 26.6   33.5    ## 26.6	2313.5 1062.7 1139.9 0.0 2502.0 17353.7 2513.6 0.0 2502.0 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.7 17353.0 173533.0 17353.0 17353.0 17353.0 17353.0 17353.0 17353.0 17353.0 173			348.3	1312.3	•	1660.0	23015.7	21864.9	22048.
2313.5 1062.7 1139.9 0.0 2202.0 31214.4 (628.2 149.4 0.0 777.0 16832.0 967.1 628.2 149.4 0.0 777.0 16832.0 110.3 39.2 69.1 0.0 0.0 877.0 16832.0 110.3 39.2 69.1 0.0 0.0 177.0 16832.0 15292.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 39.0 1 13.9 0.0 31.0 605.2 39.0 17.9 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.0 1000.9 54.0 1900.9 54.0	### 1995   1062.7   1139.9   0.0   2202   ### 1062.7   1139.9   0.0   2707   ### 100.3   39.2   69.1   0.0   1074   ### 100.3   39.2   69.1   0.0   1074   ### 13.9   0.0   31   ### 13.9   0.0   31   ### 13.9   0.0   31   ### 13.9   0.0   31   ### 13.9   0.0   31   ### 13.9   0.0   31   ### 13.9   0.0   31   ### 13.5   21.4   0.0   ### 13.5	## 1999		0	546.6	361.8		908.0	17363.7	15627.4	15765.
965.7 532.1 345.8 0.0 777.0 16832.0 110.3 345.8 0.0 0.0 65311.0 110.3 345.8 0.0 0.0 108.0 15292.2 110.3 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 173.9 0.0 31.0 605.2 35.0 173.9 0.0 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 54.0 1900.9 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9	## ## ## ## ## ## ## ## ## ## ## ## ##	### 1994   0.00   1777.0   16832.0   ### 1903   345.8   0.00   6777.0   16832.0   ### 1903   345.8   0.00   1777.0   16832.0   ### 1903   345.8   0.00   31.0   605.2   ### 1903   13.9   0.00   31.0   605.2   ### 1903   13.9   0.00   31.0   605.2   ### 1903   13.9   0.00   31.0   605.2   ### 1903   173.9   0.00   375.0   1900.9   ### 1903   173.9   0.00   54.0   1900.9   ### 1903   173.5   21.4   0.00   0.00   54.0   1900.9   ### 1903   173.5   21.4   0.00   0.00   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   ### 1903   173.5   21.4   0.00   0.00   ### 1903   173.5   21.4   0.00   ### 1903   173.5   21.4   0.00   ###		0.	1062.7	1139.9	•		31214.4	28093.0	28341.
110.3 39.2 69.1 0.0 877.0 0.531.0 100.3 39.2 69.1 0.0 0.0 100.0 15292.2 35.0 18.0 13.9 0.0 0.0 31.0 605.2 35.0 18.0 13.9 0.0 0.0 31.0 605.2 35.0 18.0 13.9 0.0 0.0 31.0 605.2 35.0 18.0 13.9 0.0 0.0 31.0 605.2 39.6 41.4 47.0 0.0 88.0 6295.9 39.1 201.9 173.9 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 54.0 1900.9 50.0 54.0 1900.9 50.	110.3 33.5.1 345.8 0.0 877 110.3 39.2 69.1 0.0 109 135.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 398.1 201.9 173.9 0.0 875 58.6 33.5 21.4 0.0 54 al Bulk (in MT)  strained T/E (in MT)  e 50.0 50.0 54 strained T/E (in MT)	110.3 39.2 54.8 0.0 877.0 0531.0 100.3 39.2 59.1 59.1 100.3 39.2 59.1 100.3 39.2 59.1 100.3 39.2 59.1 100.3 39.2 59.1 100.3 39.2 59.1 100.3 39.2 59.2 39.2 59.1 100.0 13.9 0.0 31.0 605.2 59.5 99.5 6 41.4 67.0 0.0 31.0 605.2 59.6 39.5 5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 54.0		- '	628.2	149.4	•	0.777	16832.0	15148.8	15282.
110.3	110.3	110.3			532.1	345.8		877.0	6531.0	6204.4	6256.
35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 19.0 375.0 10.0 62.9 5.0 19.0 9.0 375.0 10.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0	35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 35.0 18.0 173.9 0.0 88 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 al Bulk (in MT) strained T/E (in MT)	JS.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 173.9 0.0 88.0 6295.9 59.6 41.4 47.0 0.0 88.0 6295.9 59.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 54.0 190			39.5	1.69	•	108.0	15292.2	14527.6	14649.
35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 35.0 18.0 13.9 0.0 31.0 605.2 39.0 13.9 0.0 375.0 10956.8 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.0 1900.9	35.0 18.0 13.9 0.0 31 35.0 18.0 13.9 0.0 31 95.6 41.4 47.0 0.0 31 59.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 al Bulk (in MT) 5 strained T/E (in MT) 6	35.0 18.0 13.9 0.0 31.0 605.2 95.6 41.4 47.0 0.0 0.0 375.0 10956.9 396.1 201.9 173.9 0.0 375.0 10956.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 54.0 19		0 0	0.81	13.9	•	31.0	5.509	514.4	519.
395.6 41.4 47.0 0.0 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 62.95.9 51.0 6	al Bulk (in MT)  strained T/E (in MT)	95.6 41.4 47.0 0.0 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 675.2 51.0 670.2 51.			0.00	6.5.1	•	0.10	2000	4.4.4	
395.6 33.5 21.4 0.0 55.0 1905.6 3 58.6 58.6 33.5 21.4 0.0 5.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 1900.9 58.6 1900.9 58.0 1900.9	395.6 41.4 47.0 0.0 375 58.6 33.5 21.4 0.0 54 58.6 33.5 21.4 0.0 54 al Bulk (in MT) strained T/E (in MT) 66.6 57.5 57.5 57.5 57.5 57.5 57.5 57.5	395.6 33.5 21.4 0.0 375.0 1905.63 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 al Bulk (in MT) strained T/E (in MT)  at cont (in MT)  strained T/E (in MT)  at cont (in MT)  strained T/E (in MT)  at constrained T/E  at constrained Square sees IIA and VIIA non square			0.81	13.4	•	0.10	5.500	514.4	-615
## State	al Bulk (in MT)  strained T/E (in MT)	## 1 Park   1990	•		*****	0.7.	•	0.66	6.6620	5351.5	-1005
## 1900.9  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.6  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  1900.	al Bulk (in MT)  strained T/E (in MT)	58.6 53.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 58.6 33.5 21.4 0.0 54.0 1900.9 34.0 1900.9 34.0 1900.9 34.0 1900.9 34.0 1900.9 34.0 1900.9 34.0 1900.9 34.0 1900.9 34.0 1900.9 34.0 1900.9 35.0 1900.9 35.0 1900.9 35.0 1900.9 35.0 1900.9 34.0 1900	•		50102	6.671	•	0.000	8.90601	9861.1	9944.
## 1900.9  58.6  58.6  58.6  58.6  58.6  58.6  58.0  1900.9  21.4  0.0  58.0  1900.9  1900.9  21.4  0.0  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  58.0  1900.9  190	58.6 33.5 21.4 0.0 54  al Bulk (in MT)  strained T/E (in MT)  6 6	Sate		٥.	33.5	21.4	0.0	0.00	6.0061	1710.8	1725.
al Bulk (in MT)  strained T/E (in MT)  ntout (in MT)  anizational Maintenance Activity (OMA) for 8 Total Constrained Square  Strained T/E (in MT)  7 Constrained Square anizational Maintenance Activity (OMA) for 8 Total Constrained	al Bulk (in MT)  strained T/E (in MT)  strained T/E (in MT)	al Bulk (in MT)  strained T/E (in MT)  ntout (in MT)  sees IIA and VIIA non square		0 4	13 6	4.1.0		0.45		8.01/1	1725.
al Bulk (in MT)  strained T/E (in MT)  ntout (in MT)  7 Constrained Square anizational Maintenance Activity (OMA) for 8 Total Constrained	al Bulk (in MT)  strained T/E (in MT)  6	al Bulk (in MT)  strained T/E (in MT)  ntout (in MT)  7 Constrained Square anizational Maintenance Activity (OMA) for 8 Total Constrained sses IIA and VIIA non square		9	33.5	-		0.40	5.0061	8.0171	1725.
(in MT)  (in	(In MT) 6	(in MT)  (in MT)  6 Square Loaded T/E  7 Constrained Square Maintenance Activity (OMA) for  8 Total Constrained		,	2000	:	•	0.*50	6.0061	•	1,623.
(in MT) 6 Square Loaded T/E 7 Constrained Square Adintenance Activity (OMA) for 8 Total Constrained	(in MT) 6	(in MT) 6 Square Loaded T/E 7 Constrained Square 4 Adintenance Activity (OMA) for 8 Total Constrained VIIA non square	otal Bulk (in MT)						Constrain		0
7 Constrained Square Aaintenance Activity (OMA) for 8 Total Constrained		faintenance Activity (OMA) for 8 Total Constrained VIIA non square	onstrained T/E (i						T Loaded T		
faintenance Activity (OMA) for 8 Total Constrained		Maintenance Activity (OMA) for 8 Total Constrained VIIA non square	ountout (in MT)						mod Com	T bond T	/E Itome
(UMA) IOF 8 Total Constrained	י פסוופרומווופת פלתמוב	(UMA) IOF 8 Total Constrained	in the state of the state of			1000			nhe manita	מוב המשתבת ז	/ די דרבוווס
	(UMA) for 8 Total Constrained	A non square	rganizational Mai	nrenan	ce Activity	(OMA)			Constrain		aded Ite
A non a misto	A non a misto		Classes IIA and VI	A							
HOII W											

M1423	437.3	398.8	17.5	0.0	416.0	4.69	0.99	0.44
W1 427	115.2	1.69	38.6	0.0	107.0	6470.5	5823.4	5874-0
MESSSX	172.2	106.7	53.8	0.0	160.0	3640.0	3276.0	3304.0
×15.37	847.3	546.2	241.7	0.0	787.0	10485.5	9437.0	9520.0
*11.11	114.4	1.08	н.н.	0.0	1000	787.7	6.1.01	711.00
11 30 7X	153.7	2000	102.5	0.0	153.0	6561.7	5,406,5	6.75.7.0
41034	230.5	115.2	10501	0.0	220.0	11536.1	10959.3	11051.0
d5 0k3	19891	1126.3	682.7	0.0	1808.0	85992.3	773.93.0	78077.0
* 10.1.2.X	355.2	143.0	210.2	0.0	0.198	16520.4	14047.4	14179.0
X15.01.4	1007.4	250.3	717.4	0.0	976.0	13757.5	12391.7	12441.0
*BF40X	321.6	156.1	173.4	0.0	299.0	7934.8	6744.6	6407.0
44015X	19991	113.9	62.2	0.0	176.0	2870.1	24 39.6	2462.0
45.73 X	1216.3	949.5	212.3	0.4	1165.0	3163.8	1907.4	1932.0
M3937X	1216.8	949.5	212.3	0.4	1165.0	3163.8	1907.4	1932.0
XACOR.	1216.8	949.5	212.3	4.0	1165.0	3163.8	1907.4	1932.0
46937X	1216.8	944.5	212.3	4.0	1165.0	3163.8	1907.4	1932.0
M3937K	1216.8	949.5	212.3	4.0	1165.0	3163.8	1.707.4	1932.0
XE 468W	1200.6	954.8	272.8	34.8	1232.0	3896.0	2461.4	2492.0
N8943X	1290.6	954.8	272.8	34.8	1232.0	3896.0	2461.4	2492.0
M8943X	1290.6	954.8	272.8	34.8	12.32.0	3896.0	2461.4	2492.0
M8970X	1149.6	951.7	146.5	1.2	1099.0	2669.7	1484.6	1505.0
WHOSAX	1108.6	455.4	136.0	1.5	1059.0	2767.0	1955.1	1977.0
48964X	1108.6	952.4	136.0	٠٠٠	1059.0	2767.0	1955.1	1977.0
XF' Chr	1305.2	986.3	260.1	5.5	1251.0	3848.4	2592.9	2623.0
205850x	2000-6	952.6	1.966	5.1	1950.0	5420.8	2007.2	2050.0
M.851X	631.5	95.4	27.5	0.0	122.0	10956.8	9313.2	0.0000
MI 485X	65.0	55.6	31.9	0.0	57.0	12516.3	10638.9	10738.0
M4.112	99299	140.4	497.8	0.0	0.740	14468.8	13021.9	13137.0
M4103	416.7	107.6	297.3	0.0	404.0	10497.4	9447.7	9531.0
ZHEZIX	114.9	37.7	73.1	0.0	110.0	4830.5	4347.5	4385.0
M4 193	416.7	107.6	297.3	0.0	404.0	10497.4	0447.7	9531.0
102 64	9.99	35.8	27.1	0.0	62.0	2018.9	1817.0	1833.0
M4 225	677.2	539.3	78.2	0.0	617.0	8661.0	7794.9	7863.0
M3223X	571.1	393.1	120.6	0.0	503.0	11275.2	9583.9	9673.0
MJ243X	814.2	161.0	654.9	0.0	785.0	7131.2	6061.5	6118.0
M3255X	509.6	103.5	67.9	0.0	191.0	2741.2	2330.0	2351.0
43751X	2219.9	1749.3	162.4	0.0	1911.0	7846.5	66699	6732.0
M375.5X	R01.1	106.6	64229	0.0	782.0	8484.3	7551.6	7622.0
M3755X	801.1	106.6	675.9	0.0	782.0	8884.3	7551.6	7622.0

2214.0	2214.0	14788.0	14789.0	1870.0	1870.0
2176.7	2176.7	14651.2	14651.2	1853.5	1853.5
4900.8	4.0004	17236.7	17236.7	2180.6	2180.6
162.0	162.0	2795.0	2795.0	19.0	79.0
0.	0.	0.0	0.0	0.0	0.0
64.3	64.3	254.6	254.6	31.8	33.8
1.86	1.80	2540.8	2540.8	45.3	45.3
179.6	179.6	3238.2	3238.2	87.0	97.0

M8914X M8914X M8921 V4421

				FACTORED C	FACTORED CARGO CATEGORIES CONSTRAINT .00	IES	DOS ADJUSTMENT	0 12
LINO	פתרע בפנ	CON 17E	OM.	OMA	CON BULK	SQ T/E	CON 50 1/E	CON 00
,	1757.	15000	59.68	0.0	1656.0	128.4	5005	311.0
	143.0	8.00	9.3.1	0.0	173.0		4103.3	
	150.0	8.06	33.1	0.0	173.0	4662.9	410143	4145.00
27.73	185.3	8.00	83.1	0.0	173.0	4445.9	4103.3	4140.0
	1014.4	553.2	427.3	0.0	980.0	4425.8	4161.1	4196.0
01	10:00	553.2	427.3	0.0	0.006	6456.8	4161.1	4106.0
21,233	1010.4	553.2	421.3	0.0	0.026	6426.8	4161.1	4100.0
5571.	1014.4	503.2	427.3	0.0	0.000	4420.8	4:61.1	4100.0
41353	1014.4	553.2	427.3	0.0	0.056	4425.8	4161.1	4195.0
4103H	1014.4	553.2	427.3	0.0	0.066	4424.8	4151.1	4195.0
V:7.58	1014.4	553.2	. 427.3	0.0	0.086	4426.8	4161.1	4196.0
*1334	1014.4	553.2	427.3	0.0	0.086	4426.B	4:61.1	4196.0
*******	16/8.5	344.7	1312.8	0.0	1657.0	23015.7	21634.8	21818.0
*1123	1578.5	344.7	1312.8	0.0	1657.0	23015.7	21634.9	21818.0
41253	405.7	526.5	345.9	0.0	872.0	6531.0	6139.1	6191.0
×42.53	2.506	526.5	345.9	0.0	872.0	6531.0	5139.1	6191.0
. W4233	905.7	525.5	345.9	0.0	872.0	6531.0	6139.1	6191.0
311463	4.37.3	334.6	17.6	0.0	412.0	69.4	65.3	65.0
525 ix	437.3	394.6	17.6	0.0	412.0	69.4	65.3	65.0
K1423	437.3	394.6	17.6	0.0	412.0	69.4	65.3	65.0
W1 173X	20.9	24.2	43.5	0.0	67.0	1096.3	964.7	973.0
N1373X	6.07	20.2	43.5	0.0	67.0	1096.3	964.7	973.0
F137.3X	10.9	24.2	43.5	0.0	67.0	1095.3	964.7	973.0
XETEIN C	50.07	24.2	43.5	0.0	67.0	1096.3	964.7	973.0
1 24652	110.3	38.8	69.2	0.0	107.0	15292.2	14374.7	14496.0
255446	110.3	38.8	69.5	0.0	107.0	15292.2	14374.7	14406.0
MACTE	110.3	38.8	69.5	0.0	107.0	15292.2	14374.7	14405.0
Wie 3X	66.5	64.3	28.4	0.0	92.0	1961.4	1726.0	1741.0
M1 964X	345.1	114.1	215.6	0.0	329.0	12631.4	11115.6	11216.0
MIBECX	135.7	49.5	79.7	0.0	150.0	23312.4	20514.9	20,0000
W1019	1014.4	553.2	427.3	0.0	0.086	4426.8	4151.1	4196.0
F1123	1078.5	344.7	1312.8	0.0	1657.0	23015.7	21634.8	21918.0
×1106	0.006	534.5	362.0	0.0	896.0	17363.7	15230.1	15418.0
41.363X	2313.5	1039.1	1147.1	0.0	2186.0	31214.4	27468.7	27717.0
X4237	847.1	614.2	149.5	0.0	763.0	15632.0	14812.1	14946.0
86234	606.7	526.5	345.9	0.0	872.0	5531.0	6139.1	6191.0
25000		38.8	69.2	0.0	107.0	15292.2	14374.7	14496.0
84703		17.3	13.9	0.0	31.0	605.2	496.2	201.0
M4903		17.3	13.9	0.0	31.0	605.2	496.5	501.0
44903	35.0	17.3	13.9	0.0	31.0	603.2	2.966	201.0
10,22	95.5	40.0	47.:	0.0	87.0	65629	5152.6	5212.0
×3357X	393.1	197.4	174.0	0.0	371.0	10356.8	9641.9	0.6246
MARDIX	58.6	32.8	21.4	0.0	54.0	1000.0	1672.8	1687.0
M3853X	58.6	32.8	21.4	0.0	54.0			1687.0
M3853X	58.6	32.8	21.4	0.0	34.0	6.0061	1672.8	1537.0
M3853K	58.6	32.8	21.4	0.0	54.0	1900.9	1672.8	1687.0

65.0	5745.0	3232.0	9310.0	0.065	5826.9	10935.0	76357.0	13683.0	12216.0	6563.0	2376.0	1912.0	1912.0	1912.0	1912.0	1912.0	2466.0	2466.0	2465.0	1490.0	1955.0	1956.0	2596.0	2029.0	9071.0	10363.0	12947.0	9321.0	4289.0	9321.0	1792.0	7690.0	9335.0	5904.0	2269.0	6496.0	7355.0
65.3	5694.0	3203.2	9227.2	693.2	5774.3	10044.0	75673.2	13551.6	12105.6	6505.5	2353.5	1837.3	1887.3	1887.3	1997.3	1837.3	2435.5	2435.5	2435.5	1469.0	1934.5	1934.5	2565.6	19861	8984.5	10253.4	12732.5	9237.7	4250.9	9237.7	1776.7	7621.7	9245.7	5947.6	2247.8	6434.1	7285.1
59.4	6470.5	3640.0	10485.5	787.7	6561.7	11536,1	85992.3	16526.4	13757.5	7934.9	2870.1	3163.8	3163.8	3163.8	3163.8	3163.8	3895.0	3896.0	3896.0	2669.7	2767.0	2767.0	3848.4	5420.8	10956.8	12516.3	14468.9	10497.4	4830.5	10497.4	2018.9	8551.0	11275.2	7131.2	2741.2	7846.5	8884.3
412.0	106.0	158.0	777.0	107.0	152.0	219.0	1785.0	356.0	0.170	295.0	172.0	1160.0	1160.0	1160.0	1160.0	1160.0	1264.0	1264.0	1264.0	10000	1052.0	1052.0	1248.0	1942.0	119.0	26.0	644.0	402.0	109.0	402.0	62.0	605.0	490.0	789.0	187.0	1850.0	778.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	4.0	4.0	4.0	4.0	34.8	34.8	34.8	1.2	1.5	1.5	5.5	1.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
17.6	38.7	53.9	243.0	54.9	302.€	:05.3	9.869	218.4	717.5	173.5	65.3	212.5	212.5	212.5	212.5	212.5	273.0	273.0	273.0	146.7	136.1	136.1	260.2	8966	27.9	32.0	498.0	297.5	73.1	297.5	27.2	78.4	120.8	625.1	88.0	162.9	676.0
394.6	67.5	104.3	534.0	78.9	9.60	114.0	1101.3	138.0	253.5	121.6	109.9	944.4	944.4	944.4	4.446	944.4	6.956	6.956	956.9	943.1	914.5	914.5	982.6	944.4	92.1	24.7	146.1	105.2	36.8	105.2	35.0	527.3	369.6	155.4	6.66	1687.6	102.8
437.3	115.2	172.2	847.3	118.4	158.7	220.5	1932.1	396.2	1005.4	321.6	1.96.1	1216.8	1216.8	1216.8	1215.8	1216.6	1200.6	1290.6	1290.6	1149.6	1108.6	1108.6	1305.2	2000-6	631.5	62.0	663.6	416.7	114.9	410.7	9.99	677.2	571.1	814.2	509.6	5519.9	801.1
41423	MI 427	M8625X	M1983	X1 x1X	XI COLIN	* 50**	G5 (80	XZIONA	X15.724	Meses	XSTCEN	NG 137X	X2553X	MS-377	X2005X	x3558w	WGGG 3X	X8343X	MESSEN	767, 98	X 9 40 6 K	MSSSAX	WOOD NY	XSSERN	X1685.X	W1785X	M4112	M4143	MESSIX	N4145	M4201	M4226	M3223K	M3243X	*3253X	W3751K	M375,5X

				CONSTRAINT .85	•85		DOS AUJUSTMENT	6
TINO	BULK TOT	CON 1/E	Ç	AMO	CON BULK	SO 1/F	CON SO TVE	CON 20
M4623W	1757.1	1570.9	59.5	0.0	1630.0	328.4	303.8	306.0
41040	186.0	1.78	83.0	0.0	170.0	4662.9	3943.4	40000
ct:01.	136.0	87.7	83.0	0.0	170.0	4662.9	3963.4	40000
41030	196.0	87.7	93.0	0.0	170.0	4662.9	3963.4	400000
41038	1014.4	544.4	456.6	0.0	971.0	4426.9	4034.7	4129.0
41038	1014.4	5+4.4	456.6	0.0	971.0	4426.9	4.094.7	4129.0
55012	1014.4	544.4	456.6	0.0	0.176	4426.8	4094.7	4129.0
*1038	1014.4	544.4	456.6	0.0	0.176	4426.8	4004.7	4129.0
W1039	1014.4	544.4	454.6	0.0	0.176	4426.8	4094.7	4129.0
41038	1014.4	544.4	456.6	0.0	971.0	4426.8	4034.7	4129.0
W1039	1014.4	544.4	456.6	0.0	971.0	4426.8	4004.7	4129.0
41038	1014.4	544.4	426.6	0.0	0.176	4426.8	4094.7	4129.0
M1128	1678.5	339.2	1312.3	0.0	1651.0	23015.7	21289.5	21472.0
M1128	1678.5	339.2	1312.3	0.0	1651.0	23015.7	21289.5	21472.0
M4233	2.506	518.1	345.8	0.0	863.0	6531.0	6041.2	6093.0
44233	905.7	518.1	345.8	0.0	863.0	6531.0	6041.2	4093.0
MA233	405.1	518.1	345.8	0.0	863.0	6531.0	6041.2	6093.0
41423	437.3	388.3	17.5	0.0	405.0	4.60	64.2	0.49
41423	437.3	388.3	17.5	0.0	405.0	4.64	64.2	0.49
M1423	4 37.3	388.3	17.5	0.0	405.0	4.69	64.2	0.49
41.37.5X	10.9	23.4	43.4	0.0	0.99	1096.3	9.11.6	940.0
M1 37 3X	10.9	23.4	43.4	0.0	0.99	1096.3	931.8	0.000
41373X	40.07	23.4	43.4	0.0	0.99	1096.3	931.8	0.046
1 41.37.3X	50.02	23.4	43.4	0.0	0.99	1096.3	931.8	0.006
2507# 28	110.3	38.2	1.69	0.0	107.0	15292.2	14145.3	14267.0
M+652	110.3	38.2	69.1	0.0	107.0	15292.2	14145.3	14267.0
M4652	110.3	38.2	69.1	0.0	107.0	15292.2	14145.3	14267.0
M1 963X	66.5	42.2	27.4	0.0	0.68	1961.4	1647.2	1682.0
MIUSAX	345.1	110.2	215.5	0.0	325.0	12631.4	10736.7	10837.0
M: 462X	135.7	47.8	9.62	0.0	127.0	23312.4	19815.5	20001.0
MI 0.36	1014.4	544.4	426.6	0.0	971.0	4426.8	4004.7	4129.0
41128	1678.5	339.2	1312.3	0.0	1651.0	23015.7	21289.5	21472.0
961 IN	0.696	516.3	351.8	0.0	.878.0	17363.7	14759.2	14897.0
W1353X	2313.5	1003.7	1139.9	0.0	2143.0	31214.4	26532.3	26780.0
44237	1.748	593.3	149.4	0.0	742.0	16832.0	14307.2	14441.0
M4233	1.506	518.1	345.8	0.0	863.0	6531.0	6041.2	6093.0
44052	110.3	38.2	1.69	0.0	107.0	15292.2	14145.3	14267.0
M4903	35.0	16.4	13.9	0.0	30.0	605.2	469.0	473.0
MAJOS	35.0	16.4	13.9	0.0	30.0	605.2	469.0	473.0
70000	35.0	16.4	13.9	0.0	30.0	605.2	469.0	473.0
M4907	95.6	37.8	47.0	0.0	84.0	65629	4879.3	4929.0
M3857X	398.1	100.1	173.9	0.0	364.0	10956.8	9313.2	0.0046
M3853X	58.6	31.7	21.4	0.0	53.0	1900.9	1615.7	1630.0
M3853X	58.6	31.7	21.4	0.0	53.0	1900.9	1615.7	1630.0
#3853X	58.6	31.7	21.4	0.0	53.0	6.0061	1615.7	1630.0
M385.3X	58.6	31.7	21.4	0.0	53.0	6.0061	1615.7	1630.0

437.3	388.3	17.5	0.0	405.0	4.69	64.2	64.0
115.2	65.2	38.6	0.0	103.0	5470.5	5449.9	5551.0
172.2	100.8	53.8	0.0	154.0	3640.0	3094.0	3122.0
547.3	515.9	241.7	0.0	757.0	10485.5	8912.1	8996.0
113.4	10.3	8.HS	0.0	104.0	747.1	9.6.00	6.75.9
158.7	47.9	102.5	0.0	150.0	1.1959	5577.5	56.29.0
256.2	112.2	105.1	0.0	217.0	11536.1	10670.9	1971.2.0
123.21	106.3.7	642.7	0.0	1740.0	85942.3	73043.4	7.377H.0
34005	1.50.4	214.5	0.0	348.0	16526.4	12808.0	124574.0
1005.4	244.9	117.4	0.0	962.0	13757.5	11693.8	11803.0
341.6	114.9	173.4	0.0	298.0	7934.8	6149.5	6212.0
1.00.1	103.8	42.2	0.0	166.0	2470.1	2204.4	2241.0
1215.8	954.5	212.3	4.0	1140.0	3153.8	1857.2	1982.0
1216.8	924.5	212.3	4.0	1140.0	3153.8	1857.2	1882.0
1216.8	924.5	212.3	4.0	1140.0	3163.8	1857.2	1882.0
1210.8	924.5	212.3	0.4	1140.0	3163.8	1857.2	18H2.0
1216.8	954.5	212.3	0.4	1140.0	3163.8	1857.2	1982.0
1240.6	9006	272.8	34.8	1208.0	3896.0	2346.7	2427.0
1290.6	4000	272.8	34.8	1208.0	3896.0	2396.7	2427.0
1290.6	9000	272.8	34.8	1208.0	3896.0	2396.7	2427.0
1149.6	956.6	146.5	1.2	1074.0	2469.7	1445.5	1466.0
1108.6	1.868	136.0	1.5	1035.0	2767.0	1903.6	1925.0
1108.6	868.1	136.0	1.5	1035.0	2767.0	1903.6	1925.0
1305.2	6.096	260.1	5.5	1225.0	3848.4	2524.7	2555.0
50002	927.5	1.966	1.5	1925.0	5420.H	1954.4	1997.0
631.5	87.0	27.5	0.0	114.0	10956.8	8491.5	8578.0
62.0	23.4	31.9	0.0	55.0	12516.3	9700.2	0.0000
663.6	141.1	497.8	0.0	638.0	14468.8	12298.5	12413.0
416.7	101.6	297.3	0.0	398.0	10497.4	8922.8	9006
114.9	35.6	73.1	0.0	108.0	4830.5	4106.0	4144.0
416.7	101.6	297.3	0.0	398.0	10497.4	8922.8	9006
9.99	33.8	27.1	0.0	0.09	2018.9	1716.1	1732.0
617.2	509.3	78.2	0.0	587.0	8661.0	7361.9	7430.0
571.1	349.3	120.6	0.0	0.694	11275.2	8738.3	8928.0
814.2	146.8	654.9	0.0	771.0	7131.2	5526.7	5583.0
506.6	94.4	6.78	0.0	182.0	2741.2	2124.4	2146.0
5519.9	1594.9	162.4	0.0	1757.0	7846.5	1.1809	6143.0
801.1	97.2	6.229	0.0	773.0	8884.3	6845.3	6956.0
1.108	97.2	612.9	0.0	773.0	8484.3	6885.3	6956.0

2022.0	2022.0	13495.0	13495.0	1707.0	1707.0
1984.6	1984.6	13358.5	13358.5	1690.9	0.0691
4.0004	4800.8	17236.7	17236.7	2180.5	2190.6
153.0	153.0	2571.0	2571.0	75.0	75.0
0.	0.	0.0	0.0	0.0	0.0
64.3	64.3	254.6	254.6	33.8	33.8
89.4	4.68	2316.6	2316.6	41.3	41.3
179.6	179.6	3238.2	3234.2	06	67.0

C-30

				FACTURED C	FACTURED CARGO CATEGORIES CONSTRAINT .75	IES	DOS ADJUSTMENT	c
TIM	BULK TOT	CON 17E	Ç	OMA	CON BULK	SO 1/E	CON SO T/E	con so
W1523W	1757.7	1486.0	50.5	0.0	1545.0	328.4	287.3	289.0
07.017	190.0	77.4	83.0	0.0	160.0	4662.9	3497.2	3534.0
4101	196.0	77.4	83.0	0.0	160.0	4662.9	3497.2	3534.0
*10.00	186.0	77.4	83.0	0.0	160.0	4662.9	3497.2	3534.0
41038	1014.4	915.0	456.6	0.0	0.146	4426.8	3873.4	3908.0
*103%	1011.4	515.0	456.6	0.0	941.0	4426.3	3873.4	3908.0
41039	1014.4	515.0	426.6	0.0	0.146	4426.9	3873.4	3908.0
¥1034	1014.4	515.0	456.6	0.0	941.0	4426.8	3873.4	3908.0
W1038	1014.4	215.0	456.6	0.0	0.146	4426.8	3873.4	3408.0
41014	1014.4	215.0	456.6	0.0	0.146	4426.8	3873.4	3908.0
MIOSA	1014.4	515.0	426.6	0.0	0.146	4426.8	3473.4	3908.0
¥1033	1014.4	215.0	456.6	0.0	0.146	4426.8	3873.4	3908.0
M1128	1678.5	320.8	1312.3	0.0	1633.0	23015.7	20138.8	20322.0
M1128	1678.5	320.8	1312.3	0.0	1633.0	23015.7	20138.8	20322.0
M4233	2.506	1.064	345.8	0.0	835.0	6531.0	5714.6	5766.0
M4233	2.506	1.064	345.8	0.0	835.0	6531.0	5714.6	5766.0
N4233	405.7	405.1	345.8	0.0	835.0	6531.0	5714.6	5766.0
M1423	437.3	367.3	17.5	0.0	384.0	4.69	60.8	61.0
M1423	437.3	367.3	17.5	0.0	384.0	4.69	60.8	61.0
M1423	437.3	367.3	17.5	0.0	384.0	4.69	8.09	0.19
M1373X	6.07	50.6	43.4	0.0	64.0	1096.3	H22.2	A30.0
M1373X	6.07	50.6	43.4	0.0	64.0	1096.3	H22.2	830.0
O MISTAX	6.07	50.6	43.4	0.0	64.0	1096.3	822.2	830.0
	70.9	20.6	43.4	0.0	64.0	1096.3	822.2	830.0
2504 31	110.3	36.1	1.69	0.0	105.0	15292.2	13380.7	13502.0
M4652	110.3	36.1	1.69	0.0	105.0	15292.2	13340.7	13502.0
M4652	110.3	36.1	1.69	0.0	105.0	15292.2	13380.7	13502.0
M1863X	36.66	54.8	27.4	0.0	82.0	1961.4	1471.0	1486.0
M1864X	345.1	67.3	215.5	0.0	312.0	12631.4	9473.6	9574.0
W1802X	135.7	42.2	9.62	0.0	121.0	23312.4	17484.3	17669.0
41034	1014.4	515.0	456.6	0.0	0.146	4426.8	3873.4	3908.0
M1128	1678.5	320.8	1312.3	0.0	1633.0	23015.7	20138.8	20322.0
41196	0.696	455.5	361.8	0.0	817.0	17363.7	13022.8	13161.0
41 363X	2313.5	885.6	1139.9	0.0	2025.0	31214.4	23410.8	23659.0
M9237	847.1	523.5	143.4	0.0	672.0	16832.0	12624.0	12758.0
M1233	1.506	400.1	345.H	0.0	835.0	6531.0	5714.6	5766.0
M4652	110.3	36.1	69.1	0.0	105.0	15292.2	13380.7	13502.0
H4 903		13.2	13.9	0.0	27.0	605.2	378.2	383.0
44903	35.0	13.2	13.9	0.0	27.0	605.2	378.2	383.0
M4903	35.0	13.2	13.9	0.0	27.0	605.2	378.2	383.0
M4 907	9.56	30.5	47.0	0.0	77.0	65629	3934.9	3985.0
M3HS7X	398.1	168.3	173.9	0.0	342.0	10956.8	8217.6	8304.0
MSASJX	58.6	27.9	21.4	0.0	49.0	1.900.9	1425.6	1440.0
M3853X	58.8	27.9	21.4	0.0	49.0	1900.9	1425.6	1440.0
MJ855X	58.6	27.9	21.4	0.0	0.04	1900.9	1425.6	1440.0
MSBS3X	58.6	27.9	21.4	0.0	49.0	1900.9	1425.6	1440.0

M1423	437.3	367.3	17.5	0.0	384.0	4.64	6008	61.0
41427	115.2	57.5	30.6	0.0	0.96	6470.5	4852.9	4904.0
X4525X	172.2	98.9	53.8	0.0	142.0	3640.0	2730.0	2758.0
41443	847.3	1.55.	241.7	0.0	646.0	10485.5	7864.1	7947.0
*****	111.4	2.10	23.8	0.0	0.96	1.1.7	8.00%	597.0
X1 up:	158.7	42.2	102.5	0.0	144.0	1.1959	4921.3	4073.0
4.55.W	255.2	1001	10501	0.0	211.0	11536.1	10004.1	10195.0
G. C.F.)	1932.1	433.6	682.7	0.0	1621.0	85992.3	64434.2	65173.0
120105	330.4	105.2	214.2	0.0	323.0	16526.4	10329.0	10462.0
#36.51 X	1007.	216.1	717.4	0.0	933.0.	13757.5	10318.1	10427:0
X0496W	321.0	92.7	173.4	0.0	266.0	7934.8	4.959.3	5022.0
WHOL'SX	1.00.1	63.7	62.3	0.0	145.0	2470.1	17.95.8	1316.0
48437X	1216.8	974.6	212.3	4.0	1090.0	3163.8	1756.9	1782.0
*4695PX	1216.8	874.6	212.3	4.0	1090.0	3163.8	1756.9	1782.0
XASSEN	1216.8	974.6	212.3	4.0	1090.0	3163.8	1756.8	1782.0
XXXEnn	1210.8	874.6	212.3	0.4	100001	3163.8	1756.8	1782.0
XATOEN	1210.8	974.6	212.3	0.4	100001	3163.8	1756.8	1762.0
MESSEX	1290.6	851.8	272.8	34.8	1159.0	3896.0	2267.1	2298.0
MB943X	1290.6	851.8	272.8	34.8	1159.0	3896.0	2267.1	2298.0
118943X	1290.6	851.8	272.8	34.8	1159.0	3896.0	2267.1	2298.0
48970X	1149.6	876.5	146.5	1.2	1024.0	2669.7	1367.4	1384.0
*HOCHX	1103.6	849.6	136.0	1.5	0.786	2767.0	1800.7	1822.0
N9254X	1108.6	849.6	136.0	1.5	987.0	2767.0	1800.7	1922.0
XBGSGK	1305.2	♦08.4	260.1	5.5	1174.0	3848.4	2388.2	2418.0
WBS59X	9.0002	877.4	1.966	1.5	1875.0	5420.8	1848.7	1891.0
43851X	631.5	70.2	27.5	0.0	97.0	10956.8	6848.0	6935.0
M1 985X	62.0	18.8	31.9	0.0	20.0	12516.3	7822.7	7322.0
O 44112	663.6	124.5	497.8	0.0	622.0	14468.8	10851.6	10965.0
E 44133	416.7	89.7	297.3	0.0	380.0	10497.4	7873.1	1956.0
2 ME621X	114.9	31.4	73.1	0.0	104.0	4830.5	3622.9	3461.0
M4193	416.7	1.68	297.3	0.0	386.0	10497.4	7873-1	7956.0
M4201	9.99	29.8	27.1	0.0	26.0	2018.9	1514.2	1530.0
M4225	677.2	**6**	78.2	0.0	527.0	8661.0	6495.8	6564.0
W3223X	571.1	281.7	120.6	0.0	402.0	11275.2	7047.0	7136.0
W3243X	814.2	118.4	654.9	0.0	743.0	7131.2	4457.0	4513.0
M3253X	9.602	1.97	87.9	0.0	164.0	2741.2	1713.2	1735.0
W375!X	5519.9	1286.2	162.4	0.0	1448.0	7846.5	1.0064	4966.0
43753X	1.108	78.4	6.579	0.0	754.0	8884.3	5552.7	5623.0
M3753X	801.1	78.4	6.579	0.0	754.0	8884.3	5552.7	5623.0

1638.0	1639.0	10910.0	10917.0	1380.0	1360.0
1600.5	1600.5	10773.0	10773.0	1362.9	1362.9
4800.8	4800.8	17236.7	17236.7	2180.4	2180.6
136.0	136.0	2122.0	2122.0	67.0	67.0
•	0.	0.0	0.0	0.0	0.0
64.3	64.3	254.6	254.6	33.8	33.8
72.1	72.1	1868.3	1968.3	13.3	33.3
179.6	179.6	3238.2	3234.2	87.0	87.0

M8914X M8921 M8921 M8921 M8921

				FACTORED C	ARGO	les sai		
				CONSTRAINT	•10		DOS ADJUSTMENT	0
LINO	HULK TOT	CON 1/E	OW	DMA	CON BULK	SO 1/E	CON 50 T/E	CON SO
M4023W	1757.1	1443.6	565	0.0	1503.0	328.4	279.1	281.0
41030	186.0	72.2	83.0	0.0	155.0	4662.9	3264.0	3301.0
96018	186.0	72.2	83.0	0.0	155.0	4642.9	3264.0	3301.0
41000	196.0	72.2	83.0	0.0	155.0	4662.9	3264.0	3301.0
41034	1014.4	500.3	456.6	0.0	956.0	4426.8	3762.7	3797.0
41038	1014.4	500.3	456.6	0.0	926.0	4426.A	3762.7	3797.0
*1039	1014.4	50003	456.6	0.0	0.926	4426.8	3762.7	3797.0
41038	1014.4	50003	456.6	0.0	956.0	4426.9	3762.7	3797.0
*1039	1014.4	500.3	426.6	0.0	926.0	4426.8	3762.7	3797.0
M1038	1014.4	500.3	456.6	0.0	926.0	4426.8	3762.7	3797.0
*1039	1014.4	500.3	426.6	0.0	926.0	4426.8	37.62.7	3797.0
*103H	1014.4	50003	456.6	0.0	956.0	4426.8	3762.7	3797.0
W1128	1678.5	311.7	1312.3	0.0	1623.0	23015.7	19563.4	19746.0
M1128	1678.5	311.7	1312.3	0.0	1623.0	23015.7	19543.4	19746.0
M4233	905.7	476.1	345.8	0.0	821.0	6531.0	5551.3	5603.0
M4233	4.506	476.1	345.8	0.0	821.0	6531.0	5551.3	5603.0
M4233	4.506	476.1	345.8	0.0	821.0	6531.0	5551.3	5603.0
M1423	437.3	356.8	17.5	0.0	374.0	4.69	29.0	29.0
M1 423	4.37.3	356.8	17.5	0.0	374.0	**69	20.69	20.05
W1 423	4.37.3	356.8	17.5	0.0	374.0	4.69	20.0	20.0
M1 373X	6.07	19.2	43.4	0.0	62.0	1096.3	767.4	176.0
M137 1X	6.07	19.2	43.4	0.0	62.0	1096.3	767.4	176.0
M1 373X	6.07	19.5	43.4	0.0	62.0	1096.3	767.4	776.0
M1373X	10.9	19.5	43.4	0.0	62.0	1096.3	167.4	176.0
N#552	110.3	35.1	69.1	0.0	104.0	15292.2	12998.4	13120.0
W4652	110.3	15.1	1.69	0.0	104.0	15292.2	12998.4	13120.0
44 K52	110.3	35.1	1.69	0.0	104.0	15292.2	12908.4	13120.0
M1 46 3X	99.5	51.2	27.4	0.0	78.0	1961.4	1373.0	1398.0
MI 864X	345.1	90.06	215.5	0.0	306.0	12631.4	8842.0	H942.0
MI BOZX	135.7	39.4	19.6	0.0	118.0	23312.4	16318.7	16504.0
M1038	1014.4	500.3	456.6	0.0	956.0	4456.8	3762.7	3797.0
W1128	1678.5	311.7	1312.3	0.0	1623.0	23015.7	19563.4	19746.0
9611M	0.696	425.2	361.8	0.0	786.0	17363.7	12154.6	12292.0
MI 363X	2313.5	95928	1139.9	0.0	1966.0	31214.4	21850.1	22098.0
M4237	847.1	488.6	149.4	0.0	637.0	16832.0	11782.4	11916.0
M4233	405.7	476.1	345,8	0.0	821.0	6531.0	5551.3	5603.0
M4652	110.3	35.1	1.69	0.0	104.0	15292.2	12998.4	13120.0
M4903	35.0	11.6	13.9	0.0	25.0	605.2	332.8	337.0
M4903	35.0	9.11	13.9	0.0	25.0	605.2	332.8	337.0
M4903	35.0	9.11	13.9	0.0	25.0	605.2	332.8	337.0
M4 907	92.6	26.8	47.0	0.0	73.0	65629	3462.7	3512.0
M3857X	398.1	157.1	173.9	0.0	330.0	10956.8	1.6997	1756.0
M3853X	58.6	26.1	21.4	0.0	47.0	1900.9	1330.6	1345.0
M3853X	58.6	26.1	21.4	0.0	47.0	1900.9	1330.6	1345.0
M3853X	28.6	26.1	21.4	0.0	47.0	6.0061	1330.6	1345.0
M3853X	58.6	26.1	21.4	0.0	47.0	6.0061	1330.6	1345.0

C-34

W1423	437.3	356.8	17.5	0.0	3/4.0	0.7.4	29.0	0.60
11427	115.2	53.7	38.6	0.0	92.0	6470.5	4529.3	45.00.0
*8625X	172.2	83.0	53.8	0.0	136.0	3640.0	2548.0	2576.0
×11.48.1	847.3	4.4.8	241.7	0.0	6,000	10485.5	7.559.9	7423.0
1000	110.4	6.70	H. H.	0.0	0110	787.7	4.144	557.0
120514	158.7	10.4	102.5	0.0	141.0	6561.7	4593.2	4645.0
44654	226.2	107.1	105.1	0.0	208.0	11536.1	9805.7	0.1646
d. 0:3	1932.1	6.018	642.7	0.0	1558.0	8 - 76658	9. 86 100	60079.0
*****	330.4	6.20	218.2	0.0	310.0	16526.4	4.6800	9221.0
X 10 31 X	1005.4	201.7	717.4	0.0	910.0	13757.5	9630.2	0:6116
*CTOP!	321.6	91.6	173.4	0.0	255.0	7934.8	4364.1	4427.0
X-14PA	1.98.1	1.4.7	5.59	0.0	1.45.0	2870.1	15/8.6	1001.0
XYSEE	1216.8	949.6	212.3	4.0	1065.0	3163.8	1706.6	1731.0
MAGGER	1215.8	849.6	212.3	4.0	1065.0	3163.8	1706.6	1731.0
XXXXXX	1215.8	9.648	212.3	4.0	1065.0	3163.8	1706.6	1731.0
X35757X	1210.8	849.6	212.3	0.4	1065.0	3163.8	1706.6	1731.0
XASSEX	1216.8	849.6	212.3	0.4	1005.0	3163.8	1706.6	1731.0
XESSES	1290.6	827.5	272.8	34.8	1135.0	3896.0	2202.3	2233.0
MESESX	1290.6	827.5	272.8	34.8	1135.0	3896.0	2202.3	. 2233.0
MAYABX	1299.6	827.5	272.8	34.8	1135.0	3896.0	2202.3	2233.0
XBGTOX	1149.6	851.5	146.5	1.2	0.666	2669.7	1328.3	1349.0
NA964X	1108.6	825.3	136.0	1.5	962.0	2767.0	1749.3	1771.0
X B S C B N	1108.6	825.3	136.0	1.5	962.0	2767.0	1749.3	1771.0
MOSCHX	1305.2	882.5	260.1	5.5	1148.0	3848.4	2320.0	2350.0
MESSOX	50000	852.3	1.966	1.5	1849.0	5420.8	1795.9	1839.0
#3851X	631.5	61.7	27.5	0.0	0.68	10956.8	6026.2	6113.0
MISSSX	62.0	16.6	31.9	0.0	48.0	12516.3	6884.0	6983.0
O M4112	663.6	116.2	497.8	0.0	613.0	14468.8	10128.2	10243.0
I M4193	416.7	83.7	297.3	0.0	381.0	10497.4	7348.2	7431.0
×1294,	114.9	29.3	73.1	0.0	102.0	4830.5	3391.4	3419.0
241.23	416.7	83.7	297.3	0.0	381.0	10407.4	7348.2	7431.0
M4201	9.99	27.8	27.1	0.0	24.0	2018.5	1413.2	1429.0
M4226	677.2	419.4	78.2	0.0	497.0	8661.0	1.6062.7	6131.0
M3423X	571.1	247.9	120.6	0.0	368.0	11275.2	6201.4	6291.0
M3243X	914.2	104.2	654.9	0.0	129.0	7131.2	3922.2	3978.0
M3253X	209.6	67.0	6.78	0.0	154.0	2741.2	1507.6	1529.0
W3751X	2219.9	1131.9	162.4	0.0	1294.0	7846.5	4315.6	4378.0
M3753X	1.108	0.69	6.579	0.0	744.0	8884.3	4886.3	4957.0
W 175.4V		0 04	676.0		4 4 4 4	000	. 3004	

1446.0	1445.0	9617.0	9617.0	1216.0	1216.0
1408.4	1408.4	9480.2	9480.2	1109.3	1199.3
4800.B	4800.8	17236.7	17236.7	2180.6	2180.6
127.0	127.0	1898.0	1898.0	63.0	63.0
0.	0.	0.0	0.0	0.0	0.0
64.3	64.3	254.6	254.6	33.8	33.H
63.5	63.5	1644.1	1644.1	29.3	29.3
179.6	179.6	3238.2	3238.2	9.78	0.4.9
M8914X	X 9 1 6 B W	12684	12667	. 1.7.1	17664

C-36

### Appendix C

### SAMPLES OF COMPUTER OUTPUT

Part 3: Example of Constrained Cargo Factoring Model Output:
Constrained Cargo

CONSTRAINT= .90

SOUARE	328. 4663. 4663. 4663. 4663.	4427. 4427. 4427. 4427. 4427. 23016.	6531. 6531. 6531. 6531. 69.	1096. 1096. 1096. 1096.	15292. 15292. 1961. 12631. 23312. 4427. 23016. 17364.	6531. 15292. 605. 605. 605. 10957. 1901.
05 200	318 8233 8233 8233 8240 8240	2 4 4 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5	22048 4255 5256 5256 56 66	995	14649 14649 11468 21166 4240 22048 15765 15282	6256 14649 519 519 5401 9948 1725 1725
BULK	1698. 103. 103. 589.	589 5899 5899 5899 5699	367 560 560 560 520 520	2	41. 731. 586. 387. 181. 698.	2 2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
CON BULK	1613. 93. 93. 559.		**************************************	* * * * * * * * * * * * * * * * * * *	59. 39. 66. 117. 51. 559. 348. 547. 1063.	3.32. 3.99. 1.03. 5.02. 5.45. 6.45.
CNET	M M M M M M M M M M M M M M M M M M M	M M M M M M M M M M M M M M M M M M M	M 1128 M 4 4 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	M 1 3 7 3 X M 1 3 7 3 X M 1 3 7 3 X M 1 3 7 3 X M 1 3 7 3 X M 4 6 5 2 M 4 6	M4655 M1865X M1862X M1033 M1196 M1196 M1363X	M 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5

.69	6470.	36.40.	10446.	Trk.	6.675	11536.	85942.	165.26.	1,37.,7.	1435.	20145	3174.	3164.	3164.	3164.	3164.	389K.	3436.	3896.	2670.	2767.	2747.	3AAB.	5421.	10957.	12516.	14467.	10497.	4831.	10497.	2019.	. HAA1.	11275.	7131.	2741.	7847.	8884.	8884.
99 .	5874	3304	95.20	715	5957	11051	74077	14179	15491	5407	2462	1932	1932	2561	1912	1932	2642	2492	2465	1505	1977	17791	262.3	2050	9400	107.39	131.37	95.11	4385	1156	1933	7863	9673	6118	2351	6732	7622	7622
420.	77.	119.	607.	• 01.	-99	121.	1251.	168.	244.	140.	1.34.	.666	.666	.666	.666	•666	973.	973.	973.	1002.	971.	971.	10.38.	1003.	112.	30.	166.	120.	42.	120.	•0•	.665	451.	189.	122.	2058.	125.	125.
399.	•69	107.	546.	. H.	.1c	.115.	1120.	143.	259.	126.	114.	950•	950•	950.	950.	950•	925.	925.	925.	952.	922•	422.	986.	953.	95.	26.	149.	108.	38.	108.	36.	539.	383.	161.	104.	1749.	107.	107.
41423	M1427	44525X	W1953	MINITA	WI do IX	41014	cho cho	V-1612X	M30 :1X	MOTOR	Weblex	M89.57.X	MBG37X	X15957X	M8937X	M8937X	M8943X	XB46BX	M8943X	MB970X	MB964X	X496PM	MB968X	M4859X	MIRRIX	M1985X	M4112	F619W	W4621X	FOLOW	M4201	M4226	M3223X	M.324.3X	M3253X	M3751X	M3753X	M3753X

4801. 17237. 17237. 2151. 2151.

2214 2214 14788 14788 1870

2989. 2989. 533.

98. 98. 2541. 45.

M8914X M8914X M8921 M8621

CONSTRAINED CUBE FOR CLASS ITM AND VIEW NON SQUARE AND VIEW SQUARE TZE

SCUAFE 1991. CON SO 501 501 501 9729 1587 1587 1587 .88 BULK CONSTRAINT= CON BULK 43855X 4385.8X CNIT

M1423	395.	420.	69	49.
M1427	68.	77.	5745	6470-
43625x	104.	119.	3232	2640.
ero ix	534.	507.	0350	
X1251K	. 79.	•00	. 669	74.0
v1colv.	50.	56.	5426	
*****	114.	121.	10935	11636
CAD GD	1101.	1251.	76357	250.55
X21964	1.33.	148.	13663	10526.
748631X	. 254.	248.	12216	13757
Massax	122.	146.	6989	7935
VB615X	110.	134.	2370	2479.
XBB37X	0440	1005.	1912	3164.
XC600X	944.	1005.	1912	3164.
XCCC2X	944.	1025.	1912	3164.
×3037×	944.	1005.	1912	3164.
*CONT.	944.	1005.	1912	4:64.
WSSASX	957.	1019.	2446	3845
M8943X	957.	1019.	2466	3696.
MB943X	957.	1013.	2466	3835.
W3970X	943.	1003.	1490	2670.
X8964X	914.	973.	. 1956	2747.
W8964X	914.	973.	1956	2767.
×8968×	983.	1045.	2596	3848.
X8889X	944.	1005.	2029	5421.
MJ851X	92.	112.	9071	10957.
M1985X	25.	30.	10363	12516.
M4112	146.	155.	12847	14459.
M4193	105.	120.	0321	19497.
M8621X	37.	42.	6824	4831.
M4143	105.	120.	9321	10497.
M4201	35.	40.	1792	.6102
44560	527.	599.	1690	8661.
43223X	370.	151.	9335	11275.
M3243X	155.	199.	5904	7131.
M3253X	100.	122.	2269	2741.
. X1221	1688.	2058.	6496	7847.
M3753X	103.	125.	7355	ARRA.
43753X	103.	125.	7355	8884.

4801. 17237. 17237. 2181.

0

2138 2138 14271 14271 1805

2949.

95. 2451. 2401. 44.

M8914X M8914X M8921 W8421

CONSTRAINED CURE FOR CLASS IIM AND VIIW NON SQUARE AND VIIM SQUARE TE

CONSTRAINT= .85

SOUARE	326.	*663.	4663.	4663.	4427.		4427.		4427	4427	4427.	23016.	23016.	6531.	6531.	6531.	69.	•69	.69	1096.	.9601	.000	15292	15292	15292.	1961	12631.	23312.	4427.	23016.	17364.	16032	6531.	15292	605	605.	605.	6296.	10957.	1061	1001	1001	1001
CON SO	306	0000	0004	0000	4129	6211	6214	4 2 2 3	4129	4129	4129	21472	21472	6609	6093	6003	*9	• 0	*9	046	0 4 6	***	14267	14267	14267	1692	10837	20001	4129	21412	16041	14441	6093	14267	473	473	473	4929	9400	1530	1630	15.10	16.40
HULK	1698.	103.	.03	103.	. 284	580	589.	580.	589.	589.	549.	367.	367.	240.	560.		420.	420°	420.	27.	27.	27.	41.	41.	•1•	73.	130.	.000	265	607	1181-	698.	560.	41.	21.	21.	21.	•6•	224.	37.	37.	37.	
CON BULK	1571.	- 99	• 00 0	• 600	544.	544.	544.	544.	544.	544.	544.	339.	339.	518.	518.	518.	388.	388.	348.	23.	23.	23.	38.	38.	38.	62.	.011	• 0 • •	119.	516.	1000.	593.	518.	38.	16.	. 16.	16.	38.	191.	32.	• 27	• ::	••
UNIT	MINOS	40017	00 T	80.013	MIOUR	41038	M1038	M1038	M1038	M1038	M1038	M1128	W1128	446.53	44533	MICOS	2000	H1433	M1 42.3	MISTER	M1373X	M1373X	M4652	M4652	M4652	M1863X	X TO YOU THE	ALC:N	W. 1.28	M1196	M1363X	M4237	M4233	M4652	M4903	M4903	44903	M4 907	X / SR5W	M.585.5X	×3.8.5×	× 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	

M1 423	388.	420.	**	.69
M1427	65.	.11.	5551	6470.
48625X	101.	119.	3122	3640.
41014	516.	607.	9668	104A6.
7///	70.	.00.	473	71.1.
*1 coll	48.	50.	6,00%	
44054	112.	121.	10762	11536.
C.W. GD	1064.	1251.	73778	E3492.
MUSICA	130.	158.	124.19	16526.
440.11 X	245.	298.	11801	13757.
MADAGK	115.	148.	6212	7935.
MS615X	104.	134.	2247	2470.
MG937X	925.	•666	1442	3164.
MGGSTX	925.	. 6666	1842	3164.
M4937X	925.	•666	1882	3164.
Md937x	925.	•606	1882	3164.
M3937X	925.	•666	1882	3164.
Madesx	•006	97.3.	2454	38.16.
MBOA3X	.006	973.	24.27	3896.
XECCH	•006	973.	2427	3496.
MB970X	927.	1002.	. 1466	2470.
M8964X	898.	971.	1925	2767.
M8904X	898.	971.	1925	2747.
мврен	•096	1038.	2555	3848.
MARSOX	928.	1003.	1997	5421.
M3851X	87.	112.	8578	10057.
MIGHEX	23.	30.	9799	12516.
44112	141.	166.	12413	14469.
M4193	102.	120.	9006	10497.
MB621X	36.	42.	4144	4831.
H4193	102.	120.	9006	10497.
M4201	34.	•0•	1732	2019.
M4226	509.	-669	7430	.1998
MJ223X	349.	451.	4828	11275.
M3243X	147.	189.	5583	7131.
M3253X	94.	122.	2146	2741.
M3751X	1595.	2058.	6143	7847.
M3753X	97.	125.	6956	8884.
M3753X	97.	125.	9569	8884.

4801. 4801. 17237. 2181. 2181.

2022 2022 13495 1707

2989. 2989. 533.

89. 2317. 2317.

M8914X M8921 M8921 M4921 M4321

CONSTRAINED CUBE FOR CLASS ITM AND VITW NON SOUARE AND VITW SOUARE T/F

CONSTRAÍNT= .75

UNIT	CON BULK	BULK	CON 50	SOUARE
•				
44623M	1486.	1698.	289	328.
9001		103.	3534	4663.
M1036	77.	103.	3534	46.63.
97012	77.	103.	3534	4663.
M1038	515.	589.	3908	4427.
M1038	515.	589.	3908	4427.
M1038	515.	589.	3908	4427.
M1038	515.	589.	3908	4427.
M1038	515.	589.	3908	4427.
M1038	515.	589.	3908	4427.
M1038	515.	• 600	3908	4427.
2001	351.	367.	20122	2.1016
W1128	321.	367.	20322	23016
M4233	490.	560.	5766	6531.
M4233	*06*	560.	5766	6531.
M4233	• 06 •	260.	5766	6531.
M1423	367.	420.	19	.69
M1423	367.	420.	61	•69
M1423	367.	420.	61	. 69
M1373X	21.	27.	930	1096.
M1373X	21.	27.	830	1096.
M1373X	21.	27.	8.30	1096.
M1373X	21.	27.	830	.9601
2001	30.		13502	15202
M4652	36•	•1•	13502	15292.
41853X	55.	73.	1486	1961
MIB64X	97.	130.	9574	12631.
M1862X	42.	56.	17669	23312.
M1038	515.	589.	3908	4427.
M1128	321.	367.	20322	23016.
961190	456.		13161	17364.
M4237	523	498-	13759	11214.
M4235	490	560-	5766	
M4652	36.	41.	1.3502	15292.
M4903	13.	21.	183	605
M4903	13.	21.	383	605.
M4903	13.	21.	383	605.
M4907	30.	*6*	3985	6296.
M3857X	168.	224.	A304	10957.
M3853X	28.	37.	1440	1001
M 385 3X	28.	37.	1440	1001
MJRSSX	28.	37.	1440	1001
4.5H5.3X	.43	3/•	1440	1001

367.	420. 77. 119.	61 4904 2758	64.70. 3640.
.555.	• 607.	7967	10486.
42.	. 00	£454	6562.
100.	121.	10185	11536.
934.	1251.	65178	85992.
105.	168.	10460	16576.
210.	288.	10427	13757.
93.	148.	5022	7935.
84.	1.34.	1816	2870.
875.	.666	1782	3164.
875.	.666	1782	3164.
875.	•666	1782	3164.
A75.	.66.6	1782	3164.
875.	.616	1742	3164.
852.	973.	2298	3894.
852.	973.	2298	3896.
852.	973.	2298	3896.
877.	1002.	. 1388	2670.
850.	971.	1822	2767.
850.	971.	1822	2757.
908	1038.	2418	3848.
677.	1003.	1881	5421.
.02	112.	6935	10957.
1.3.	. 30.	1922	12516.
124.	166.	10965	14469.
•06	120.	7956	10497.
31.	42.	3661	4831.
•06	120.	7956	10497.
30.	*0*	1530	2019.
449.	599.	6564	8661.
282.	451.	7136	11275.
118.	149.	4513	7131.
76.	122.	1735	2741.
1286.	2058.	4966	7847.
78.	125.	5623	P.884.
78.	125.	5623	8894.

4801. 17237. 17237. 2181. 2191. 1638 1638 10910 1340 1380 115. 2989. 2989. 53. 72. 72. 1868. 33.

M8914X M8914X M8921 M3921

CONSTRAINED CURE FOR CLASS ITM AND VITW NON SQUARE AND VITW SQUARE TVE

CONSTRAINT# .70

SQUARE	328. 4663. 4663. 4663. 4427. 4427. 4427. 4427. 4427. 23016. 6531. 6531. 6531. 1096. 1096. 1096. 1196. 12631. 23312. 4427. 23016. 1661. 17364. 31214. 16832. 665. 665. 665.	1001
CON SO	281 3301 3301 3301 3301 3301 3301 3301 33	1345
BULK	1698 103 103 103 103 103 103 103 103 103 103	37.
CON BULK	72. 72. 72. 5000. 5000. 5000. 5000. 5000. 512. 476. 476. 476. 19. 19. 19. 19. 19. 19. 19. 19	26.
r v s	M M M M M M M M M M M M M M M M M M M	M3853X

M1423	357.	420.	59	•69
M1427	54.	.77.	4580	6470.
43625X	83.	119.	2576	3540.
WIO18	425.	607.	7423	10486.
W1377K	.1.0	.00	557	744.
WI SO7X	39.	.995	4645	6662.
M4654	103.	121.	4897	11536.
CND GP	876.	1251.	60819	65542.
1719174	43.	158.	4521	16.26.
M3631X	202.	288.	97.39	13757.
MA640X	H2.	148.	4427	7935.
X3196K	74.	1.34.	1001	ZH 70.
#3937X	H50.	•066	1731	3164.
M8937X	850.	.666	1731	3164.
M8937X	850.	.666	1731	3164.
X250FF	.058	•666	1731	3164.
XACTOR	850.	939.	1731	3104.
M3943X	827.	973.	2233	3896.
M8943X	827.	973.	2233	3896.
M8943X	827.	973.	22.33	3896.
MBG70X	852.	1002.	1349	26.70.
MR964X	825.	971.	1771	2767.
M8964X	A25.	971.	1771	2767.
мнубах	882.	1038.	2350	3848.
M8359X	852.	1003.	1839	5421.
M3R51X	.29	112.	6113	10957.
M1985X	17.	30.	6983	12516.
M4112	116.	166.	10243	14469.
M4193	84.	120.	7431	10497.
M3621X	29.	42.	3419	4831.
M4193	84.	120.	7431	10497.
M4201	28.	*0*	1429	2019.
M4226	419.	.665	6131	8661.
M3223X	248.	451.	6291	11275.
M3243X	104.	189.	3978	7131.
M3253X	67.	122.	1529	2741.
M3751X	1132.	2058.	4378	7847.
M375.3X	•69	125.	4957	8884.
M3753X	•69	125.	4957	8884.

4801. 17237. 17237. 2181. 2181.

1446 1446 9617 9517 1216 1216

2989. 2989. 2989. 53.

63. 1644. 1644. 29.

M8914X M8914X M8921 M8921 M8921

C-53

### Appendix C

### SAMPLES OF COMPUTER OUTPUT

Part 4: Example of Constrained T/E Embarkation Analysis Model Output

### Appendix C

### SAMPLES OF COMPUTER OUTPUT

### Part 4: Example of Constrained T/E Embarkation Analysis Model Output

### I INTRODUCTION

Part 4 of Appendix C is a series of constrained T/Es computed by the Constrained T/E Embarkation Analysis Model (CONTEAM) for a sample of ten representative FMF units. For each unit, three tentative constrained T/Es are included--one for each constraint (90%, 85%, and 75%) applied to the unit's fully authorized T/E. Each constraint is applied equally to both square and cube items in the listings; however, CONTEAM is capable of calculating a constrained T/E for a unit with different constraints for square and cube even though such a case isn't presented in the tables.

### II DETAILED EXPLANATION OF CONSTRAINED T/E EMBARKATION ANALYSIS MODEL OUTPUT LISTING

Explanations for the headings, columns, and totals found in the sample output listing from the Constrained T/E Embarkation Analysis Model (CONTEAM), Table C-1, are given below. The number of each explanation relates to the same number superimposed on the output listing of unit M1038.

- (1) Unit description.
- (2) Total cube of all cube loaded items in unit's T/E.
- (3) Percentage of total cube this unit is to be constrained.

  Total cubic feet of unit when constrained.
- (4) Total square of all square loaded items in unit's T/E.
- (5) Percentage of total square this unit is to be constrained. Total square feet of unit when constrained.
- (6) TAM number from unit's authorized T/E.
- (7) Square of individual TAM item.
- (8) Cube of individual TAM item.
- (9) Weight of individual TAM item.
- (10) Item square (column 7) multiplied by T/E quantity (column 13). Total square feet in unit's T/E occupied by all units of a TAM item.
- (11) Item cube (column 8) multiplied by T/E quantity (column 13). Total cube feet in unit's T/E occupied by all units of a TAM item.
- (12) Item weight (column 9) multiplied by T/E quantity (column 13). Total weight in unit's T/E occupied by all units of a TAM item
- (13) Quantity of each TAM item authorized in unit's T/E.

- (14) Item criticality. Relevance of item to supporting unit's mission. The 8 criticality items support the unit's primary mission(s); the 4 criticality items support the unit's secondary mission(s); the 2 criticality items support the unit's tertiary mission(s); and the 1 criticality items are the remaining items of the unit's T/E.
- (15) Quantity of each TAM item in unit's reduced T/E after applying constraint.
- (16) Item square (column 7) multiplied by reduced T/E quantity (column 15). Total square in unit's constrained T/E occupied by all units of a TAM item.
- (17) Item cube (column 8) multiplied by reduced T/E quantity (column 15). Total cube in unit's constrained T/E occupied by all units of a TAM item.
- (18) Item deficiency in constrained T/E (column 13- column 15).
- (19) Total square feet of all square loaded TAM items in unit's authorized T/E.
- (20) Total cubic feet of all cube loaded TAM items in unit's authorized T/E.
- (21) Total weight of all (cube loaded and square loaded) TAM items in unit's authorized T/E.
- (22) Total of all units of all TAM items in unit's authorized T/E.
- (23) Total of all unit's of all TAM item's in unit's constrained T/E.
- (24) Total square feet of all square loaded TAM items in unit's constrained T/E.
- (25) Total cubic feet of all cube loaded TAM items in unit's constrained T/E.
- (26) Operational Readiness Index relating to unit's constrained T/E square loaded items. This index relates the criticalityweighted square loaded items in the unit's constrained T/E to the criticality-weighted square loaded items in the unit's authorized T/E.
- (27) Same as 26 but for cube loaded items.
- (28) Same as 26 but for both square loaded and cube loaded items.

### III SAMPLE OF FMF T/Es CONSTRAINED TO 95%, 85% AND 75% OF AUTHORIZED ALLOWANCES

Table C-1 contains constrained T/Es for ten representative FMF units. Applied to each unit is a weighted constraint of 90, 85, and 75 percent of the unit's authorized T/E cube and square. Section VI explained how each unit was assigned a weight according to its importance in the assault echelon.

These ten units were chosen as a sample of FMF units since publishing a compendium of all MAF units was too voluminous to include in this appendix.

Table C-1

SAMPLE FMF T/Es CONSTRAINED TO 90%, 85%, AND 75% OF AUTHORIZED T/E ALLOWANCES

					<b>e</b>	SENCY :																																			
					0	CURF	5.0	39.0	0.0	0.0	25.0	C - 1	15.0	0.:	0.3	2.0	1.0	15.0	7.0		2002	0.0	24.0	6.04	0.0		0.4	2.0	53.0	3.0	0.0		2.0	2.0	3.0	;	0.00	2.0	56.0	346.0	
					9	SOUARE														140.0	122.0					120.0									;	24.0			-		
					<b>@</b>	0TY	:	13.			25.	•	15.	:	:	٠,	• -	15.		2.	5 6	: :	3.	5.	5 x.		٥' :		1.	ř.	•	:		:	<u>.</u>	:	: :		7.	٠.	:
		TEMS	tt		3	CRIT	60	•	<b>6</b> 0 <b>6</b> 0	. 60	c	4 4	* œ	•		•	4 4	60	6	80	<b>6</b> 0 <b>6</b>	. 60	80	8	en en	8	<b>c</b> c	n no	•	or .	<b>2</b> 3		4	4	4	٠.	e (,	. 0.	~	63 1	
38	NOIS	TAM ITEM	55	200	0	977	-	13		4	52		. 2	-		~ ~	<b>-</b>	15	1	8	~ ~		•	ın ı	5.8	~	ο :	נו	-		- 4		~	-	m .	- :		~	2	· ·	-
UNIT M1038	WARINE DIVISION	-	15556.65 R 15824.00	S 4431.00	0	T/E.	159.0	6111.0	240.0	36.0	300.0	42.0	45.0	26.0	252.0	20.0	45.0	330.0	392.0	8380.0	5070.0	0.0	303.0	695.0	1150.0	6740.0	110.0	100.0	145.0	201.0	0.00	20.0	80.0	30.0	45.0	2041.0	225.0	0.000	210.0	1920.0	
O 1/E FOR	BATTALION. WA	CLASS VII. CLASS I	S.0 PCT OR	_	9	T/E CUBE	5.0	39.0	12.0	0.4	25.0	0.0	15.0	1.0	8.0	22.0	1.0	15.0	7.0		7002	0.0	24.0	40.0	58.0		•	5.0	53.0	3.0	0.0	1.0	2.0	5.0	3.0	(	6.1	2.0	56.0	0.68.0	
CONSTRAINED	INFANTRY BATT		COUSE OF PUBLISHED T/E	CONSTRAINED TO 95.0 9CT	9	SQUARE														140.0	122.0					150.0	_								4	34.0					
	INF	CURTATE T/E FOR	CONSTR/	SQUARE CONSTRI	<b>9</b>	ITEM WEIGHT	159.0	47.0	20.0	0.6	12.0	0 4 5 0	3.0	26.0	252.0	0.01	45.0	22.0	26.0	4190.0	2575.0	0.0	101.0	130.0	20.0	3370.0	55.0	28.0	145.0	97.0	0.0	20.0	25.0	30.0	15.0	212	225.0	116.0	355.0	0.000	7
	Θ		<b>@</b> @	<b>©</b> @		LTEN	5.0	•	0.0	0.1	0.1		1.0	1.0	9.0	0.1	•	1.0	1.0		350.0	0.0	8.0	8.0			2.0		53.0	0.1	000	1.0	1.0	2.0	1.0	0	8.1	1.0	13.0	173.0	
			Į		0	SOUARE														20-0	0.10					90.0										0.00					
					0	144	Aunas	A003c	AG320	40.128	06404	40.400	A03: 2	41143	A1240	41 41 41 41 41 41 41 41 41 41 41 41 41 4	A1 × 7.9	A1 7.30	41800	21900	A1940	41950	A2010	APCRO	A2950	A2182	42134	A2430	A2510	A2580	42635	A2700	A2710	A2960	A3230	20405	80500	81540	05918	91,590	2000
																																			M1038	int =	706	!			

### CONSTRAINED TZE FOR UNIT MI038

# INFANTRY BATTALION. MARINE DIVISION

CUNTATE THE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE IS 16655.65 CU FT CONSTRAINED TO 95.0 PCT OR 15024.00 CU FT

SQUARE OF PUBLISHED TZE IS 4431.00 SO FT CONSTRAINED TO 95.0 PCT OP 4209.00 SO FT

1.00   25   1   25   1   12   13   13   13   13   13   13	TEN CUBE
150.0   25   1   25.   12.0     150.0   25   1   25.   13.5     150.0   25   1   25.   18.7     160.0   10   1   10.   19.0     160.0   10   1   10.   19.0     160.0   10   1   10.   19.0     160.0   12   1   12.   12.0     160.0   12   1   12.   12.0     160.0   12   1   11.   12.0     160.0   12   1   11.   12.0     160.0   12   1   11.   12.0     160.0   12   1   11.   12.0     160.0   10   11   11.   11.     160.0   12   1   11.   12.0     160.0   10   11   11.   12.0     160.0   11   11.   12.0     160.0   12   1   12.0     160.0   12   1   12.0     160.0   13   1   13.0     160.0   13   1   13.0     160.0   13   1   13.0     160.0   13   1   13.0     160.0   13   1   13.0     160.0   13   1   13.0     160.0   13   1   13.0     160.0   13   1   14.0     160.0   13   1   14.0     160.0   1   14.0     160.0   1   14.0     160.0   1   14.0     160.0   14.0   15.0     160.0   160.0     160.0	0.4
150.0 50 1 50. 13.5  150.0 25 1 25. 18.7  500.0 10 1 10. 19.0  500.0 25 1 25. 19.0  500.0 25 1 25. 17.0  19984.0 1249 1 1249. 1274.5  500.0 12 1 1 1 1. 2.0  500.0 12 1 1 1 1. 2.0  600.0 6 1 6 1 6. 10.6  600.0 6 1 1 1 1 1. 2.0  1550.0 390 1 390. 370. 33.9  600.0 6 1 1 1 1 1. 2.0  600.0 6 1 1 1 1. 10. 10.6  600.0 6 1 1 1 1. 10. 10.6  600.0 6 1 1 1 1. 10. 10.6  600.0 6 1 1 1 1. 10. 10.6  600.0 70.0 1 1 1 1. 10. 10.6  600.0 70.0 1 1 1 1. 10. 10.6  600.0 70.0 1 1 1 1. 10. 10.6  600.0 70.0 1 1 1 1. 10. 10.6  600.0 1 1 1 1 1. 10.6  600.0 1 1 1 1	0.9
175.0   25   1   25.   18.7   18.7   175.0   25   1   25.   18.7   18.7   18.0   18.	3.0
600.0 10 10 10.0 18.5 50.0 50 1 50.0 3.5 50.0 25 1 25.0 17.0 50.0 12 1 12.0 18.0 60.0 12 1 1 1 1 1.0 60.0 6 1 60.0 18.0 60.0 6 1 60.0 18.0 60.0 1 1 1 1.0 60.0 1 1 1 1 1.0 60.0 1 1 1 1 1.0 60.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.0
18.0	0.09
50.0       50.       3.5         50.0       25       1         50.0       25       1         50.0       25       1         50.0       25       1         50.0       12       1         50.0       1       1         27.0       1       1         50.0       1       1         50.0       1       1         50.0       6       1         60.0       6       1         60.0       6       1         60.0       6       1         60.0       6       1         60.0       6       1         60.0       6       1         60.0       6       1         60.0       6       1         60.0       1       1         70.0       30.0       3.0         30.0       30.0       3.0         30.0       3.0       3.0         40.0       1       1       1         40.0       2       1       2         60.0       1       1       1         40.0       2       1	3.0
50.0 25 1 25.  50.0 25 1 25.  50.0 1249 1 1249.  50.0 1 1 1 1 1.  27.0 1 1 1 1 1.  27.0 1 1 1 1 1.  27.0 1 1 1 1 1.  27.0 1 1 1 1 1.  27.0 48 1 68.  60.0 6 1 69.  53.0 1 1 1 1 1.  30.0 1 30.  30.0 1 1 1 1 1.  40.0 1 1 1 1 1.  27.0 20. 1 1 1 1.  40.0 0 1 1 1 1.  40.0 0 1 1 1 1.  40.0 0 1 1 1 1.  27.0 20.0 8 83.0 22 1 22.  285.0 0 35 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22 1 22.  883.0 22.  88	1.0
50.0 25 1 25. 3.8   50.0 25 1 25. 17.0   50.0 12 1 12. 75.6   50.0 12 1 12. 75.6   50.0 1 1 1 1. 1.   27.0 1 1 1 1. 1.   60.0 6 1 66. 19.6   60.0 6 1 66. 19.6   53.0 1 1 1 1.   320.0 5 1 50. 9350.1   350.0 350 1 390. 33.0   60.0 1 1 1 1.   7.7   7.7   7.7   7.8	1.0
50.0       25       17.0         19984.0       1249       1 1249       1 234.5         50.0       1       1       1       2.0         27.0       1       1       1       2.0         27.0       1       1       1       6       1       6         240.0       6       1       6       1       6       1       6       1       6       1       6       1       6       1       6       1       6       1       6       1       6       1       6       6       1       6       6       1       6       6       1       6       6       1       6       6       1       6       6       1       6       6       1	2.0
19984.0 1249 1 1249. 1235.5 960.0 12 1 12. 75.6 27.0 1 1 1 1. 1. 2.0 27.0 1 1 1 1. 1. 2.0 280.0 8 1 86. 51.8 60.0 6 1 66. 51.8 53.0 7 1 1 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	2.0
960.0 12 1 12.  50.0 1 1 1 1.  50.0 1 1 1 1.  5240.0 6 1 6.  5240.0 6 1 6.  50.0 6 1 6.  50.0 1 1 1 1.  50.0 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1 1.  50.0 1 1 1 1 1.  50.0 1 1 1 1 1 1.  50.0 1 1 1 1 1 1.  50.0 1 1 1 1 1 1 1.	16.0
50.0       1       1       1.3         40.0       6       1       1.3         240.0       6       1       6.0       10.3         50.0       48       1       48.0       10.0       5.0         60.0       6       1       5.0       5.0       5.0       5.0         50.0       0       1       1       1.0       5.0       <	80.0
27.0 1 1 1 1.3 40.0 8 1 8	20.0
40.0       8       1       6.       19.6         540.0       6.       1       6.       119.6         480.0       6.       1       6.       93.0         53.0       1       1       1.       4.2         50.0       30.0       1       1.       7.7         320.0       5       1       1.       7.7         320.0       30.0       1       1.       7.7         320.0       30.0       1       1.       1.       7.7         204.0       1       1       1.       1.       1.       1.         204.0       1       1       1.       1.       1.       1.       1.       1.       1.       1.       1.       1.       1.       44.6       44.6       44.6       44.6       44.6       44.6       44.6       44.6       45.0       2.       2.0       2.0       2.       2.0 <td>27.0</td>	27.0
240.0 6 1 66 119.6 660.0 661.8 660.0 661.1 66.0 15.8 65.0 65.0 1 65.0 65.0 65.0 65.0 65.0 65.0 65.0 65.0	2.0
480.0 48 1 48. 51.8 60.0 6 1 5. 7.9 530.0 5 1 1 1 6.0 320.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	40.0
165600   6   1   5   5   5   5   5   5   5   5   5	10.0
155600.0 920   1   1   1   1   1   1   1   1   1	10.0
155600.0 920   1 850.   9350.1   320.0   320.0   55.0	53.0
320.0 5 1 5.  390.0 390 1 10.  204.0 1 1 1 10.  440.0 1 1 1 10.  240.0 1 1 1 10.  5250.0 7 1 17.  5250.0 35 1 32.  565.0 35 1 22.  5754.0 17 1 17.  2850.0 2 2 1 22.  3750.0 2 1 10.  5250.0 35 1 32.  3750.0 2 1 10.  5250.0 35 1 32.  5750.0 2 1 10.  5750.0 2 1 20.  5750.0 2 1 10.  5750.0 2 1 20.  5750.0 2 1 10.  5750.0 2 10.  5750	180.0
50.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	64.0
390.0 390 390.  200.0 1 1 1 1 1.  240.0 1 1 1 1 1.  240.0 2 1 2.  240.0 39 1 18.  5250.0 35 1 32.  502.0 22 1 22.  502.0 29 1 1 1.  5250.0 35 1 32.  5250.0 35 1 32.  5250.0 35 1 32.  5250.0 2 1 2.  5250.0 2 1 1 1 1.  5250.0 35 1 32.	20.0
204.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.4
595.0 11 1 1.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	234.0
240.0 2 1 2. 240.0 6 1 6. 595.0 7 1 7. 472.0 59 1 56. 24.0 2 1 26. 5250.0 35 1 32. 504.0 35 1 32. 504.0 35 1 32. 504.0 17 1 17. 2850.0 17 1 17. 2850.0 22 1 22. 2620.0 22 1 22. 2754.0 17 1 17.	0.9
240.0 6 1 6. 440.0 11 1 11. 525.0 7 1 7. 24.0 59 1 55. 60.0 1 1 2. 5250.0 35 1 32. 504.0 35 1 32. 504.0 36 1 34. 83.0 22 1 22. 2754.0 17 1 17. 2850.0 22 1 22. 2752.0 22 1 22. 2752.0 22 1 22.	5.0
440.0 III I II. 595.0 7 1 7. 472.0 59 1 55. 24.0 2 1 2. 504.0 35 1 32. 504.0 36 1 22. 83.0 22 1 22. 2754.0 17 1 17. 2850.0 2 1 22.	40.0
595.0 7 1 7.  472.0 59 1 55.  524.0 2 1 1 2.  5250.0 35 1 32.  392.0 2 1 22.  504.0 36 1 34.  2754.0 17 1 17.  262.0 2 1 22.	40.0
24.0 59 1 56	85.0
24.0 2 1 2. 5250.0 35 1 32. 392.0 2 1 2. 504.0 36 1 34. 83.0 22 1 22. 2754.0 17 1 17. 2850.0 19 1 19. 262.0 2 1 2.	8.0
5250.0 1 1 1 32. 5250.0 35 1 32. 504.0 35 1 34. 83.0 22 1 22. 2754.0 17 1 17. 2850.0 19 1 19. 842.0 2 1 2.	12.0
5250.0 35 1 32. 392.0 2 1 2. 504.0 35 1 34. 83.0 22 1 22. 2754.0 17 1 17. 262.0 2 1 22. 262.0 2 1 22.	0.09
392.0 2 1 2. 504.0 36 1 34. 83.0 22 1 22. 2754.0 17 1 17. 2850.0 19 1 19. 8422.0 2 1 2.	150.0
504.0 36 1 34. 2754.0 17 1 17. 2850.0 19 1 19. 262.0 2 1 2.	106.0
2754.0 17 1 17. 2850.0 19 1 19. 262.0 2 1 2.	14.0
2850.0 17 1 17. 2850.0 19 1 19. 262.0 2 1 2. 845.0 24 1 24.	0.4
2850.0 19 1 19. 262.0 2 1 2. 8472.0 24 1 24.	162.0
262.0 2 1 2. 3472.0 24 1 24.	150.0
222.0 24 1 24.	131.0
22.1.0 6. 1	353.0
	34.0

### CONSTRAINED THE FOR UNIT MID39

## INFANTKY BATTALION. MARINE DIVISION

# CURTATE TIE FOR CLASS VII. CLASS II TAM TTEMS

CONSTRAINED TO 95.0 PCT OR 15824.00 CU FT SOUARE OF PURLISHED T/E IS 4431.00 SO FT CONSTRAINED TO 95.0 PCT OR 4209.00 SO FT

101	ITEM	I TEM	TYEN WF CONT	1/E	1/E	TVE WETCHT	1/E	CPIT	*****	******EDUCED T	T/E****	DEFIC-
									•			
C\$430		2.8	100.0		22.1	800.0	œ		9.		22.1	
06053		1.5	31.0		1.5	31.0	-	-	.1.		1.5	
01090		5.0	200.0		2.0	50000	-	-	-1		5.0	
C6140		٠,	7.0		1.3	0.04		-	.7.		1.3	
61243		0.9	84.0		6.0	84.0	-	1	:		6.0	
66220		5.	7.0		6.0	84.0	12	1	12.		6.0	
09290		11.0	2.0		11.0	2.0	-	-			11.0	
C6.370		6.3	107.0		50.4	856.0	œ	-	α •		50.4	
C6383		6.5	140.0		58.7	1400.0	10	1	10.		48.7	
C6390		7.2	257.0		86.2	3084.0	12	-	12.		86.2	
C6410		18.0	330.0		144.0	2640.0	6	-	. 8		144.0	
C6490		1.5	62.0		10.5	434.0	1	-	7.		10.5	
00590		1.0	12.0		5.0	0.09	r	-	5.		5.0	
. 01593		6.9	0.06		34.3	450.0	S.	-	٠,		34.3	
06990		3.2	30.0		3.2	30.0	-	-	1.		3.2	
C66.70		6.	18.0		0.	18.0	-	-	-1		6.	
C6684		0.	1.0			1111.0	111	1	1111.		1.1	
06000	38.0		1054.0	38.0		1054.0	-	•	:	38.0		
00100		20.0	163.0		20.0	163.0	-	2	:		50.0	
06800		1.4	21.0		4.1	21.0	-	2	1:		1.4	
00100		5.	16.0		• 5	16.0	1	2	:		v.	
01.00		9.	16.0		9.	16.0		2	:		9.	
07500		۳.	10.0		•3	10.0	-	2	:		E.	
00725		125.0	1832.0		125.0	1832.0	-	2	1:		125.0	
90100		••	1.0		0.	1.0	-	2	:		0.	
00110		2.06	1890.0		2.06	1890.0	-	2	:		2.00	
00840	0.94		570.0	828.0		10260.0	13	80	17.	7.55.7		:
00800	71.0		2780.0	71.0		2780.0	-	4	:	71.0		
07010	134.0		7370.0	938.0		21590.0	1	<b>c</b>	7.	938.0		
00110	18.0		0.000	540.0		27000.0	30	8	27.	4.00.4		3.
01160	61.0		2400.0	1220.0		48000.0	50	60	18.	1100.5		
EDUBO		•	3.0		4.3	108.0	36	-	36.		4.3	
E0000		*	7.0		1.6	28.0	*	-	. 4		1.6	
E0189		1.0	10.0		0.1	10.0	-	œ	:		0.1	
E0210		0.	1.0		:	2.0	c	-	٠,		:	
E0230		4.0	68.0		0.0	68.0	-	œ	:-		4.0	
E0200		••	7.0		4.8	84.0	15	4	12.		4.8	
E0320		8.9	108.0		17.9	216.0	2	8	2.		17.9	
E0892		0.0	0.0		0.0	0.0	110	80	110.		0.0	
60000		3.0	27.0		36.0	324.0	15	80	12.		36.0	
50050		2.5	15.0		68.3	480.0	35	æ	32.		5.P.R	
06603		1.3	24.0		4.5.5	840.0	5	æ	35.		8.50	
61060		12.0	5.0.0		144.7	6.006		r	15.		144.0	

CONSTRAINED TZE FOR UNIT M1038

## INFANTRY DATTALION. MARINE DIVISION

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE IS 16656.65 CU FT CONSTRAINED TO 95.0 PCT OR 15824.00 CU FT

SQUARE OF PUBLISHED TZE 15 4431.00 SQ FT CONSTRAINED TO 95.0 PCT OR 4209.00 SQ FT

	LTEN	ITEM	ITEM	1/E	1/E	1/E	1/E	CRIT	****	*****REDUCED T/E***	T/E****	DEFIC-
1.34	SOUARE	CUBE	WEIGHT	SOUARE	CUBE	WEIGHT	017		410	SOUARE	CUBE	IFNCY
06013		62.0	120.0		496.0		ď	60	8		496.0	
E1155		0.0	0.0		0.0		36	80	36.		0.0	
1156		0.0	0.0		0.0			•	•		0.0	
151		0.0	0.0		0.0			80	•		0.0	
180		0.	2.0		1.1	72.0	36	. 60	36.		::	
240		••	1.0		y.			60	20.		9.	
260		1.0	3.0		2.0	0.9		-	2.		2.0	
480	45.0		420.0	360.0		3360.0	60	60	8.	360.0		
530		4.2	68.0		4.2	68.0	-	80	:		4.2	
160		.3	8.0		1.3	32.0	•	60	.4		1.3	
006		1.0	5.0		2.0	10.0	8	•	2.		2.0	
096			2.0		•	2.0	-	~	:		-	
52030		::	39.0		3.4	117.0	m	~	3.		3.4	
	GRAND TO	OTALS		4431.0	16656.6	412462.0 405	4051		3968.	4209.0	4209.015824.0	
				9	8	8	8		8	8	(8)	
0000	TODAYS DATE 03/03/76 OR INDEX(SQUARE) = 93.46 OR INDEX(CUBE) = 98.99 OR INDEX(TOTAL T/E) = 98	03/03/76 ARE) = 93.46 E) = 98.99 AL T/E) = 98.51	3.46 19 198.51									

### CONSTRAINED TZE FOR UNIT MID38

# INFANTRY BATTALION. MARINE DIVISION

# CURTATE T/E FUR CLASS VII. CLASS II TAM ITEMS

CU FT	1 00	SO FT	SO FT
16656.65	00-10-51	4431.00 SO FT	4099-00
CUBE OF PUBLISHED T/E IS 16656.65 CU FT	CONSTRAINED TO 92.5 PCT OR 15407.00 CO FT	SQUARE OF PUBLISHED TYE IS	CONSTRATINED TO 92-5 PCT OR 4099-00 SO FT

																																							000	138	: = 85%	11
DEFIC-	IF NCY																																				NOTE.		T	Unic = MIU38	Constraint	Constrain
T/F****	CUAE	5.0	39.0	0.0	12.0	4.0	25.0	1.0	5.0	15.0	1.0	8.0	2.0	55.0	1.0	15.0	7.0			700.0	0.0	24.0	0.00	3.0	58.0		0.4	10.0	5.0	53.0	3.0	5.0	4.0	1.0	2.0	2.0	3.0		29.0	8	2.0	26.00
	SOUARE																	140.0	122.0							120.0												54.0				
****	017	:	13.	:	12.	•	. 52.	:-	1:	15.	:-	1.	2.	2.		15.		2.	2.	2.	:	3.	5.	.3.	58.	2.	2.	10.	5.	1.	3.		. 4	:	2.	:	3.	:	:	1.	5.	٠ ،
CRIT		<b>6</b>	8	80	8	8	8	4	4	8	4	4	4	4	4	80	8	8	60	80	60	60	80	8	80	60	80	80	8	4	80	8	80	4	4	4	4	2	4	~	2	2 0
1/E	OTY	-	13	-	12	4	25	-	-	15	-	-	8	2	-	15	1	2	2	2	-	٣	S	3	28	2	2	10	S	-	3	-	4	-	67	-	6	-	-	-	2	n n
1/6	WE IGHT	159.0	6111.0	0.0	240.0	36.0	300.0	42.0	0.46	45.0	26.0	252.0	20.0	186.0	45.0	330.0	392.0	8380.0	5070.0	2150.0	0.0	303.0	695.0	69.0	1160.0	6740.0	110.0	20.0	140.0	145.0	291.0	0.06	40.0	20.0	20.0	30.0	45.0	2641.0	312.0	225.0	232.0	7:0.0
T/E	CUBE	5.0	39.0	0.0	12.0	4.0	25.0	1.0	5.0	15.0	1.0	8.0	2.0	22.0	1.0	15.0	7.0			700.0	0.0	24.0	40.0	3.0	58.0		4.0	10.0	2.0	53.0	3.0	5.0	4.0	1.0	2.0	2.0	3.0		29.0	8.1	2.0	25.0
1/E	SQUARE																	140.0	122.0							120.0												54.0				
	WEIGHT	159.0	47.0	0.0	20.0	0.6	12.0	42.0	94.0	3.0	26.0	252.0	10.0	93.0	45.0	22.0	26.0	4190.0	2535.0	2575.0	0.0	101.0	139.0	23.0	20.0	3370.0	25.0	2.0	28.0	145.0	97.0	0.06	10.0	20.0	25.0	30.0	15.0	2641.0	312.0	225.0	 116.0	355.0
ITEM	CUBE	5.0	3.0	0.0	1.0	1.0	1.0	1.0	5.0	1.0	1.0	8.0	1.0	11.0	1.0	1.0	1.0			350.0	0.0	8.0	8.0	1.0	1.0		2.0	1.0	1.0	53.0	1.0	2.0	1.0	1.0	1.0	2.0	1.0		29.0	8.1	1.0	13.0
ITEM	SOUARE																	10.0	61.0							0.09												54.0				
	TAM	2000	A0090	A0265	A0320	A0328	A0490	A0710	40800	43922	A1180	A1240	A:250	A1420	A1573	A: 730	A1800	41900	A1920	A1940	A1950	A2010	A2020	A2040	A2950	A2132	A2184	A2390	42480	A2510	A2580	0992V	42685	A2700	42710	A2900	A3280	30465	06408	60500	 91240	91540

### CONSTRAINED T/E FOR UNIT MI038

# INFANTRY BATTALION, MARINE DIVISION

CURTATE T/E FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE IS 16656-65 CU FT CONSTRAINED TO 92-5 HCT OF 15407-00 CU FT

SQUARE OF PUBLISHED T/E IS 4431.00 SQ FT CONSTRAINED TO 92.5 PCT OR 4099.00 SQ FT

	TTEM	I TEM WEIGHT	SQUARE	T/E CUBE	1/E WEIGHT	1/E 017	CRIT	014	*REDUCED SQJARE	CUBE	DFF1C-
7		0.4		7.8	100.0	25	-	25.		7.8	
s.		0.9		12.0	150.0	52	-	25.		12.0	
		3.0		13.5	150.0	20	-	20.		13.5	
8.		7.0		18.7	175.0	25	-	25.		18.7	
••		1.0			9.0	S	-	2.		:	
1.9		0.09		18.5	0.009	01	-	10.		18.5	
.2		3.0		1.0	18.0	9	-	•		1.0	
:		1.0		3.5	50.0	20	-	20.		3.5	
0.		1.0		:	2.0	S	-	5.	•	-	
.2		2.0		3.8	20.0	52	-	25.		3.8	
		2.0		17.0	50.0	25	-	24.		17.0	
1.0		16.0		1236.5	19984.0	1249	-	1247.		1236.5	
6.3		90.0		75.6	0.096	12	-	12.		75.6	
2.0		50.0		2.0	80.0	-	-	1:		2.0	
1.3		27.0		1.3	27.0	-	1	-		1.3	
7.		5.0		4.	40.0	•	7	8.		9.	
3.3		40.0		19.6	240.0	9	-	•		10.6	
1:1		10.0		51.8	480.0	84	-	48.		51.8	
• 5		10.0		2.9	0.09	•	-	•		5.9	
4.2		53.0		4.2	53.0	-	-	-		4.2	
11.0		180.0		10120.0	165600.0	920	-	815.		8964.5	105.
11.0		64.0		25.0	320.0	S	-	5.		55.0	
7.7		0.09		7.7	0.09	-	_	-1		7.7	
••		1.0		3.9	390.0	390	-	390.		3.9	
3.0		85.0		3.0	85.0	-	-	:		3.0	
12.0		204.0		12.0	204.0	-	-	-		12.0	
1.4		0.9		1.4	0.9	-	-	:		1.4	
.2		2.0		4.	4.0	8	-	5.		4.	
5.0		40.0		11.7	240.0	9	-	•		11.7	
7.7		40.0		84.6	440.0	=	-	-11		84.6	
6.4		85.0		44.6	295.0	1	-	٠.		44.6	
3.6		8.0		210.0	472.0	29	-	55.		196.2	4
4.		12.0			24.0	~	-	2.		1.	
1.0		0.09		1.0	0.09	-	-	1:		1.0	
14.0		150.0		490.0	5250.0	35	-	31.		430.3	
. 0.4		196.0		8.1	392.0	2	-	2.		8.1	
2.7		14.0		95.8	504.0	35	-	34.		4.68	2.
3.8		0.4		83.2	88.0	22	-	22.		83.2	
8.2		162.0		138.7	2754.0	17	-	17.		138.7	
7.0		150.0		132.2	2850.0	61	-	19.		132.2	
0.6		131.0		18.0	262.0	2	-	2:-		18.0	
25.0		353.0		60000	8472.0	54	-	23.		585.7	:
4.3		38.0		25.1	228.0	9	-	٠,		25.7	

### CONSTRAINED TZE FOR UNIT M1038

## INFANTRY BATTALION, MARINE DIVISION

CURTATE TZE FUR CLASS VII. CLASS II TAM ITEMS

CUNSTRAINED TO 92.5 PCT OR 15407.00 CU FT CUNSTRAINED TO 92.5 PCT OR 15407.00 CU FT SQUARE OF PUBLISHED T/E IS 4431.00 SQ FT CONSTRAINED TO 92.5 PCT OR 4099.00 SQ FT

;	ITEM	ITEN	ITEM	T/E	3/1	1/E	1/E	CRIT	****	*REDJCFD T/	T/E***	DEFIC-
	30000	300	11011	and one	300		;		;	2000	2000	
C5930		2.8	100.0		22.1	0.008	œ	-	8.		22.1	
06650		1.5	31.0		1.5	31.0	-	-	-		1.5	
01090		2.0	200.0		2.0	200.0	-	-	:		2.0	
C6140		.2	7.0		1.3	49.0	1		7.		1.3	
C6215		0.9	84.0		0.9	84.0	-	-	-		6.0	
C6220		••	7.0		0.9	84.0	12	-	12.		0.9	
09793		11.0	5.0		11.0	5.0	-		-		11.0	
C6370		6.3	107.0		50.4	856.0	80	-	œ		50.4	
C5388		5.9	140.0		58.7	1400.0	10	1	10.		58.7	
Co390		7.2	257.0		86.2	3084.0	12	-	12.		86.2	
01493		18.0	330.0		144.0	2640.0	60		8		144.0	
C6490		1.5	62.0		10.5	434.0	^		7.		10.5	
00593		1.0	12.0		5.0	0.09	S	-	5.		0.4	
C6510		6.9	0.00		34.3	450.0	S	-	'n		34.3	
09993		3.2	30.0		3.2	30.0	-		-		3.2	
C6670		6.	18.0		6.	18.0	-	1	1.		0.	
C6684		••	1.0		1:1	1111.0	111	-	111.		1:1	
06000	38.0		1054.0	38.0		1054.0	-	4	:	38.0		
00100		20.0	163.0		20.0	163.0	-	8	1.		20.0	
00390		1.4	21.0		1.4	21.0	-	8	-		1.4	
00400		.5	16.0		• 5	16.0	-	. ~	-		٠.	
01400		9.	16.0		9.	16.0	-	8	-		9.	
00530		•3	10.0		.3	10.0	-	8	:			
00725		125.0	1832.0		125.0	1832.0	-	N	:		125.0	
99100		•	1.0		с.	1.0	1	8	1:		0.	
00110		2.06	1890.0		2.06	1890.0	-	2	:		4006	
00840	46.0		570.0	828.0		10260.0	18	60	16.	738.1		2.
06800	71.0		2780.0	71.0		2780.0	-	4	:	71.0		
01020	134.0		7370.0	938.0		21290.0	^	80	7.	928.6		
00110	18.0		0.006	540.0		27000.0	30	80	56.	464.1		•
01110	61.0		2400.0	1220.0		48000.0	20	80	18.	1068.7		2.
E0080		7.	3.0		4.3	108.0	36		36.		4.3	
E0090		4.	7.0		1.6	28.0	4		4.		1.6	
E0180		1.0	10.0		1.0	10.0	-	80	:		1.0	
E0210		•	1.0		•	5.0	S	-	5.		:	
E0230		4.0	0.89		4.0	68.0	-	8	:		0.4	
E0290		4.	7.0		4.8	84.0	12	4	12.		4.8	
E0320		8.9	108.0		17.9	216.0	8	80	5.		17.0	
E0892		0.0	0.0		0.0	0.0	110	60	110.		0.0	
E0900		3.0	27.0		36.0	324.0	12	8	12.		36.0	
E0420		2.2	15.0		68.3	480.0	32	8	32.		68.89	
E0490		1.3	24.0		45.5	840.0	35	8	35.		45.5	
09013		15.0	6.05		144.0	0.009	12	8	12.		144.0	

CONSTRAINED T/E FOR UNIT MI038

## INFANTRY BATTALION, MARINE DIVISION

CURTATE THE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED T/E IS 16656.65 CU FT CONSTRAINED TO 92.5 PCT OR 15407.00 CU FT

SQUARE OF PUBLISHED T/E IS 4431.00 SQ FT CONSTRAINED TO 92.5 PCT OR 4099.00 SQ FT

TAM	SQUARE	LTEN	I TEM WE I GHT	SQUARE	T/E CUBE	T/E WEIGHT	T/E CRIT	CRIT	****	*****REDJCED	TVETT	DEFIC-
060		62.0	120.0		496.0	960.0		60			436.0	
155		0.0	0.0		0.0	0.0	36	80	36.		0.0	
E1156		0.0	0.0		0.0	0.0		80	4.		0.0	
157		0.0	0.0		0.0	0.0		80	. 4		0.0	
180		0.	2.0		1.1	72.0		8	36.		1:1	
240		0.	1.0		9.	20.0		8	20.		••	
260		1.0	3.0		2.0	0.9			2.		2.0	
480	45.0	. /	420.0	360.0		3360.0		80	8.	354.5		
530		4.2	68.0		4.2	68.0		60	:			
160		3	8.0		1.3	32.0	*	8	•		1.3	
006		0.1	2.0		2.0	10.0		4	2.		2.0	
096		1.	2.0		-	2.0	-	2	:		:	
030		:	39.0		3.4	117.0		~	3.		3.4	
	GRAND TOT	OTALS		4431.0	16656.6	412462.0 4051	4051		3926.	4099.0	4099-015407-0	

TODAYS DATE 03/02/76
OR INDEX(SQUBE) = 90.20
OR INDEX(CUBE) = 98.48
OR INDEX(TOTAL T/E) = 97.76

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### CONSTRAINED TZE FOR UNIT MI039 INFANTRY BATTALION. MARINE DIVISION

# CURTATE T/E FOR CLASS VII. CLASS II TAM !TEMS

CUBE OF PUBLISHED IZE IS 16656.65 CU FT CONSTRAINED TO 67.5 PCT OR 14575.00 CU FT

SQUARE OF PUBLISHED TZE IS 4431.00 SO FT CONSTRAINED TO 87.5 PCT OR 3877.00 SO FT

DEFIC-	FENCY																																				NOTE:		Unit = M1038	Constraint - 75%				
	CURE TE	0.0	39.0	0.0	12.0	4.0	55.0	1.0	5.0	15.0	1.0	8.0	2.0	22.0	1.0	15.0	7.0			700.0	0.0	24.0	0.04	3.0	58.0		0.4	10.0	8.0	53.0	3.0	5.0	0.4	1.0	2.0		3.0 NO		29.0 Un			24.0	344.0	4.2
*****REDUCED T/E***	SOUARE									•								140.0	122.0							120.0												40.4						
****	410	-	13.	1.	12.	•	25.	-	-	15.	-	:	2.	2.	-	15.	7.	2.	2.	2.	-	3.	2.	3.	58.	2.	2.	10.	·	-	3.	-		-	2	-	3.	-	-	-		2	· ·	:
CRIT		60	60	0	80	. 60	60	•	4	60	•	•	4	4	•	8	80	89	60	80	60	60	8	60	80	8	80	80	80	•	20	8	8	4	4	4	4	~	4	2	~	~	2	2
1/E	410	-	13	-	12	4	52	-	-	15	-	-	2	2	-	15	1	~	8	8	-	3	2	n	58	8	8	10	c	-	•	-	4	-	2	-	m	-	-	~	~	۲.	2	-
T/E	WEIGHT	159.0	6111.0	0.0	240.0	36.0	300.0	42.0	0.46	45.0	26.0	252.0	20.0	186.0	45.0	330.0	392.0	8380.0	2070.0	5150.0	0.0	303.0	695.0	0.69	1160.0	6740.0	110.0	20.0	140.0	145.0	291.0	0.06	0.04	20.0	20.0	30.0	45.0	2641.0	312.0	225.0	232.0	710.0	1920.0	140.0
1/E	CUBE	5.0	39.0	0.0	12.0	4.0	25.0	1.0	5.0	15.0	1.0	8.0	2.0	22.0	1.0	15.0	7.0			700.0	0.0	24.0	40.0	3.0	58.0		0.4	10.0	2.0	53.0	3.0	2.0	4.0	1.0	5.0	5.0	3.0		29.0	8.1	2.0	56.0	346.0	4.2
1/E	SOUARE																	140.0	122.0							120.0												54.0						
	WEIGHT	159.0	47.0	0.0	20.0	0.6	12.0	45.0	0.46	3.0	26.0	252.0	10.0	93.0	45.0	22.0	26.0	4190.0	2535.0	2575.0	0.0	101.0	139.0	23.0	20.0	3370.0	55.0	2.0	28.0	145.0	97.0	0.06	10.0	20.0	25.0	30.0	15.0	2541.0	312.0	225.0	116.0	355.0	0.005	140.0
ITEM	CUBE	5.0	3.0	0.0	1.0	1.0	1.0	1.0	5.0	1.0	1.0	8.0	1.0	11.0	1.0	1.0	1.0			350.0	0.0	8.0	8.0	1.0	1.0		2.0	1.0	1.0	53.0	1.0	2.0	1.0	1.0	1.0	2.0	1.0		29.0	8.1	1.0	13.0	173.0	4.2
ITEM	SQUARE																	10.0	61.0							0.09												24.0						
	TAM	AOOOS	Angeo	A0265	A0320	A0328	A0490	0110V	A0800	A0922	A1180	41240	A1250	A1420	41570	A1730	A1500	41900	A1920	41040	0561V	A2910	42020	A2046	A2050	42192	A2184	A2330	AZAFO	A2510	42580	A2660	A2635	A2700	A2710	A2900	43280	80465	B0430	80500	91540	8:650	131540	32220

### INFANTRY BATTALION. MARINE DIVISION

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED T/E IS 16556.65 CU FT CONSTRAINED TO 87.5 PCT OR 14575.00 CU FT

SQUARE OF PUBLISHED TZE IS 4431.00 SO FT CONSTRAINED TO 87.5 PCT OR 3977.00 SO FT

DEFIC- TENCY												.40						•			164.											7.			7.		4					2.	
T/E****	7.8	12.0	13.5	18.7	:	18.5	1.0	3.5		3.8	17.0	1143.3	75.5	2.0	1.3	٧.	19.6	6.74	2.0	4.2	8320.3	55.0	7.7	3.0	3.0	12.0	1.4	4.	11.7	84.6	9.44	193.6			30705	F. 9	84.0	83.2	130.7	132.2	10.0	545.1	2.50
*****PEDUCED																																											
****	25.	25.	20.	25.	٠,	10.	. 9	50.	5.	25.	25.	1155.	12.	:	-	8	• 9	44.		:	756.	5.	-	390.	:	:	-	2.	• 9	::	7.	52.	2.	:	28.	2.	32.	22.	17.	10.	2.	55.	•
CRIT	-		-	-	. 1	-	-	-	-	-	1	-	-	-	-	-	1	1	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-
17E	25	25	20	25	S	10	9	20	S	25	52	1249	12	-	-	8	ç	48	9	1	920	c	-	390	-	-	-	2	9	=	1	29	2	-	35	2	36	22	17	13	~	24	٤.
T/E WEIGHT	100.0	150.0	150.0	175.0	3.0	0.009	18.0	20.0	5.0	20.0	20.0	19984.0	0.096	20.0	27.0	40.0	240.0	480.0	0.09	53.0	165600.0	320.0	60.0	390.0	95.0	204.0	0.9	4.0	240.0	440.0	205.0	472.0	24.0	60.0	5250.0	392.0	504.0	84.0	2754.0	2850.0	252.0	8472.0	203.0
T/E CUBE	7.8	12.0	13.5	18.7	•	18.5	1.0	3.5	•	3.8	17.0	1236.5	75.6	2.0	1.3	9.	19.6	51.8	2.9	4.2	10120.0	55.0	7.7	3.9	3.0	12.0	1.4	4.	11.7	84.6	44.6	210.0		1.0	490.0	8.1	0.5.8	83.2	138.7	132.2	18.0	6.00.0	25.7
TZE																																											
ITEM WEIGHT	0.4	0.9	3.0	7.0	1.0	0.09	3.0	1.0	1.0	2.0	2.0	16.0	80.0	20.0	27.0	2.0	40.0	10.0	10.0	53.0	180.0	64.0	0.09	1.0	85.0	204.0	0.9	2.0	40.0	40.0	85.0	8.0	12.0	0.09	150.0	196.0	14.0	4.0	162.0	150.0	131.0	353.0	14.0
1 TEM CUBE	r.	• 5	£.	8.	••	1.9	• 5	••	0.	• 5		1.0	6.3	2.0	1.3	••	3.3	1:1	•5	4.2	11.0	11.0	7.7	0.	3.0	12.0	1.4	• 5	2.0	7.7	6.4	3.6	4.	1.0	14.0	4.0	2.1	3.8	8.2	7.0	0.0	25.0	4.3
SQUARE																																											
TAM	62010	C2030	52040	C2050	62060	C2070	22100	22160	C2230	C2223	C2310	C3020	C4000	C4010	C4015	C4020	C4040	C4110	C4140	C4250	04240	C4340	C4.390	C4436	C4650	C4650	54670	C4680	06943	C4 790	C4870	C4 H80	C4930	04430	08640	C5090	C5110	C5200	C5320	C5400	C5410	65.920	C/83/0

### INFANTRY BATTALION, MAYINE DIVISION

CURTATE THE FOR CLASS VII. CLASS II TAM ITTING

COBE OF PUBLISHED TZE IS 16656-65 CU FT CONSTRAINED TO 87-5 PCT 08 14575-00 CU FT

SQUARE OF PUBLISHED TZF IS 4431.00 SO FT CONSTRAINED TO 87.5 PCT OR 3677.00 SO FT

	1164	LTEM	ITEM	1/6	TZE	1/1	1/E	CRIT	****		1/E***	Deerc-
144	SGUARE	CUBE	WEIGHT	SOUARE	CUBE	WEIGHT	710		410	SOUAPE	-CuBE	1 F NCV
02553		2.8	100.0		22.1	800.0	a.	-	e:		22.1	
06653		1.5	31.0		1.5	31.0	1				2.	
02010		5.0	200.0		5.0	200.0	-	-	-:		5.0	
C6140		• •	7.0		1.3	49.0	1	-	. 7 .		1.3	
C6215		0.9	84.0		0.0	84.0	-	. 1			6.0	
C6223		5.	7.0		0.9	84.0	12	-	12.		6.0	
09293		11.0	5.0		11.0	2.0	-	-	1.		11.0	
021.63		6.3	107.0		50.4	855.0	œ	-	œ		50.4	
C6388		8.9	140.0		58.7	1400.0	01	1	10.		56.7	
C6.390		7.2	257.0		86.2	3084.0	12	-	12.		86.8	
C6410		18.0	330.0		144.0	2640.0	60		8.		144.0	
C6490		1.5	62.0		10.5	434.0	1	-	7.		10.5	
00573		1.0	12.0		5.0	0.09	r	-	5.		5.0	
01593		6.9	0.06		34.3	450.0	S	-	5.		34.3	
09990		3.2	30.0		3.2	30.0	-	-	:		3.2	
C6670		6.	18.0		0.	18.0	-	-			c.	
COURS		0.	1.0		1:1	111.0	111	-	111.		1.1	
06000	38.0		1054.0	38.0		1054.0	-	4	-	38.0		
00100		20.0	163.0		20.0	163.0	-	2	:		20.0	
00300		1.4	21.0		1.4	21.0	-	2	:		1.4	
00400		• 5	16.0		.5	16.0	-	2			6.	
01400		9.	16.0		٠٠	16.0	-	2	-		9.	
00530		.3	10.0		.3	10.0	-	2			F:	
00725		125.0	1832.0		125.0	1832.0	-	2	-		125.0	
59100		•	1.0		0.	1.0	-	8	1:		0.	
00110		2.06	1890.0		2.06	1890.0	-	2	:		40.06	
00840	46.0		0.076	828.0		10260.0	18	80	15.	596.2		en.
06.600	71.0		2780.0	71.0		2780.0	-	•	••	70.3		
01020	134.0		7370.0	938.0		51590.0	7	œ	• 9	850.9		:
00110	18.0		0.006	540.0		27000-0	30	60	25.	441.7		5.
01110	61.0		2400.0	1220.0		48000.0	50	80	17.	1005.8		3.
E0080		:	3.0		4.3	108.0	35	-	36.		4.3	
Ecoso		4.	7.0		1.5	28.0	4	-			1.6	
E0130		0.1	10.0		1.0	10.0	-	8	:		0.1	
E0210		•	1.0		-	٥٠٤	r	-	·		:	
E0230		0.4	68.0		4.0	68.0	-	8	:		4.0	
E0200		4.	7.0		4.8	84.0	15	4	12.		4.6	
E0320		8.9	108.0		17.9	216.0	2	æ	2.		17.0	
E0492		0.0	0.0		0.0	0.0	110	œ	110.		0.0	
E0100		3.0	57.0		36.0	324.0	12	60	12.		36.0	
20020		2.2	15.0		68.3	480.0	35	8	32.		58.A	
06663		1.3	24.0		45.5	0.018	35	c	35.		45.5	
6.100.0		12.0	0.00		140.0	20000	1.5	9	17.		144.0	

CONSTRAINED THE FOR UNIT MI039

### INFANTRY BATTALION. MARINE DIVISION

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED T/E IS 16656-65 CU FT CONSTRAINED TO B7-5 PCT OP 14575-00 CU FT

SOUARE OF PUBLISHED T/E IS 4431.00 SQ FT CONSTRAINED TO 87.5 PCT OR 3877.00 SQ FT

	LTEM	I TEM	ITEM	1/E	1/E	1/5	1/6	CRIT	****	********	1/5***	DEFIC-
TAN	SOUARE	CUBE	WEIGHT	SOUARE	CUBE	WE IGHT	710		710	SOJARE	CUBE	TENCY
E1090		62.0	120.0		496.0	963.0	60	80			494.0	
51155		0.0	0.0		0.0	0.0	36	<b>6</b> 0;	36.		0.0	
E1136		0.0	0.0		0.0	0.0	4	80	. 4		0.0	
E1157		0.0	0.0		0.0	0.0	4	60	4.		0.0	
E1130		••	2.0		1:1	72.0	36	60	36.		1.1	
E1240		••	1.0		ç.	20.0	50	8	20.			
E1260		1.0	3.0		2.0	6.0	2	1	2.		2.0	
E1480	45.0		420.0	360.0		3360.0	60	60		331.7		-
E1530		4.2	68.0		4.2	68.0	-	60	:			
E1760		.3	8.0		1.3	32.0	•	60			1.3	
E1400		1.0	5.0		2.0	10.0	2	4	2.		2.0	
E1960		-	2.0		=	2.0	-	8	:		~	
E2030		::	39.0		3.4	117.0	E)	2	3.		3.4	
	GRAND T	OTALS		4431.0	16656.6	412462.0	4051		3756.	3877.0	1877-014575-0	

TODAYS DATE 03/02/76
OR INDEX(SQUARE) = 85.54
OR INDEX(CUBE) = 96.31
OR INDEX(TOTAL T/E) = 95.38

MOTES TRANSPIRE BATTALION, MARINE DIV CURTATE TZE FOR CLASS VIII, CLASS II TAM ITEMS

SQUARE OF PUBLISHED TZE IS 26935.00 SO FT CONSTRAINED TO 90.0 PCT OR 24242.00 SO FT

COME OF PUBLISHED TATE IS STIP. 34 CU FT CONSTRAINED TO 00.0 OCT OR \$141.00 CU FT

																																										0		
DEFIC-	11.NCV																										7.					•				71.		NOTE:		Unit = M1658	Constraint = 90%			
	נהשב זו	12.0	0	0.4	1.0	3.0	1.0		6.0	5.0				350.0	8.0	0.4	5.0	1.0	1.0	0.1		55.0	0.04	17.0	6.2	9.0	8.8	15.0	0.	14.8	α.	5.5	c·	3.0	13.6	20006		2.0	1.3	r.			4.2	44.0
*********	SOUASE										70.0	122.0	187.0								54.0																							
****	710	4.	:	4.		3.	1.	-	2.	5.	1.	•		:		. 6	5.	:	:	:	:	:-	. 4		20.	20.	33.	20.	•	9.	5.	34.	**	50.	500	203.	•	:	:	. 4	۶.	4.	1.	•
2317		4	*	~	2	5	4	2	4	4	4	4	4	4	•	4	4	2	٥	N	4		2	2	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-			
1/5	710	4	-	4	-	•	-	-	9	c	-	~	m	-	-	¢	N	-	-	-	-	-	4	4	50	50	40	50	•	ď	S	40	4	20	50	274	4	-	-	*	r	*	-	*
1/2	WEIGHT	188.0	50.0	43.0	42.0	0.0	10.0	45.0	132.0	280.0	4190.0	5070.0	8010.0	2575.0	139.0	120.0	26.0	50.0	55.0	15.0	2641.0	1750.0	880.0	260.0	80.0	120.0	120.0	140.0	0.4	460.0	15.0	40.0	C.4	40.0	40.0	4334.0	320.0	50.0	27.0	20.0	500.0	40.0	611-0	256.0
1/F	CUBE	12.0	1.0	4.0	1.0	3.0	1.0	1.0	0.9	5.0				350.0	8.0	0.9	2.0	1.0	1.0	1.0		55.0	40.0	17.0	6.2	9.6	10.9	:2.0	0.	14.9	8.	2.8	c.	3.0	13.6	271.3	25.5	2.0	1.3	••	16.3	5.0	۲٠٠٧	
1/5	SQUARE										10.0	122.0	180.0								24.0																							
I TEM	WEIGHT	47.0	20.0	12.0	42.0	3.0	10.0	45.0	22.0	56.0	4190.0	2535.0	2570.0	2575.0	130.0	20.0	28.6	20.0	25.0	15.0	2641.0	1750.0	220.0	140.0	0.4	0.4	3.0	7.0	1.0	0.09	3.0	1.0	0.1	2.0	2.0	16.0	80.0	20.0	27.0	2.0	40.0	10.0	51.0	0.00
ITEM	CUBE	3.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0				350.0	0.9	1.0	1.0	1.0	1.0	1.0		55.0	10.0	4.2	£.	5.	.3	.8		1.9	•5	-	0.	• 5		1.0	6.3	2.0	1.3	-	3.3	٠.	2.4	11.0
ITEM	SOUARE										10.0	61.0	0.09								24.0																							
	TAN	00.CCK	40320	00404	40716	43922	A1250	A1570	A1730	41800	41 400	41929	41930	04014	42020	42050	42480	AZTED	42710	A3280	80465	81230	41620	02220	01023	52030	05000	05023	09023	02020	C2100	09123	62230	05250	C2310	03050	000000	01040	51000	02043	04040	C4:40	09243	C4 140

### MOTOR TRANSPORT BATTALION. MARINE DIV

CURTATE TIE FOR CLASS VII. CLASS II TAM ITEMS

CURE OF PUBLISHED TZE IS 5712.38 CU FT CONSTRAINED TO 20.0 PCT DR 5141.00 CU FT

SQUARE OF PUBLISHED TZE IS 26933.00 SO FT CONSTRAINED TO 90.0 OCT OR 24242.00 SO FT

		WEIGHT		COBE	WEIGHT			410	Sec.	2000	ייירי
	7.7	50.0		23.0	140.0	E	-	3.		23.0	
	0.	1.0		1.5	151.0	151	-	151.		1.5	
	3.0	95.0		3.0	85.0	-	1	:		3.0	
	15.0	204.0		12.0	204.0	-	-	:		12.0	
	1.4	0.9		1.4	0.9	-	-	:		1.4	
	.2	2.0		• 5	2.0	-	-	-1		.2.	
	2.0	40.0		9.8	200.0	5	-	5.		6.0	
	7.7	40.0		38.4	200.0	r	1	5.		38.4	
	15.0	150.0		30.0	300.0	2	-	2.		30.0	
	6.4	85.0		51.0	680.0	8	1	8.		611.0	
	3.6	8.0		53.4	120.0	15	-	15.		53.4	
		12.0		1.4	48.0	4	-	٠,		1.4	
	3.9	0.56		3.9	95.0	-	-	:		3.9	
	14.0	150.0		224.0	2400.0	. 15	-	15.		215.R	-
	15.0	250.0		45.0	750.0	3	-	3.		45.0	
	4.0	196.0		4.0	196.0			:		0.4	
	2.7	14.0		18.6	0.80	1	-	7.		18.6	
	3.8	4.0		41.6	44.0	1.1	1			41.6	
	8.2	162.0		81.6	1620.0	10	-	10.		81.6	
	7.0	150.0		6000	1950.0	13	-	13.		900	
	0.6	131.0		0.6	131.0	-	-	:		0.0	
	55.0	353.0		20000	2824.0	•	-	ά		2000	
	4.3	34.0		34.2	304.0	80	1	ď.		34.2	
	2.8	100.0		13.8	200.0	S	-	5.		13.8	
	1.5	31.0		5.8	124.0	4	-	•		5.8	
	.2	7.0			42.0	2	-				
	• 5	5.0		5.0	20.0	4	-			2.0	
	11.0	150.0		11.0	150.0	-	-	:		11.0	
	6.3	107.0		25.2	428.0	4	-	. 4		25.2	
	5.3	140.0		88.0	2100.0	15	-	1.5.		88.0	
	7.2	257.0		35.3	1285.0	5	-	5.		35.9	
	18.0	330.0		164.0	2540.0	œ	-	•		144.0	
	119.0	2148.0		476.0	8265.0	4		4		476.0	
	1.5	62.0		42.0	1736.0	28	-	20.		29.0	å
	6.9	0.00		27.5	360.0	4	-	•		27.5	
	20.0	300.0		150.0	0.000	3		3.		150.0	
	6.	19.0		6.	18.0	-	-	:		0.	
	0.	1.0		**	37.0	37	-	37.		4.	
	1.4	24.0		1.4	24.0		4	:		1.4	
38.0		1054.0	114.0		3162.0	2	*	3.	114.0		
	4.0	517.0		72.0	0.0016	1.3	-	.8.		75.0	
119.0		5455.0	367.0		1755.0		*	:	357.0		
	1.4	0.1.		5.5	11.3.3	<					

CONSTRAINED TZE FOR UNIT M1658

MUTTER TRANSPORT BATTALION, MARINE DIV CUSTALE 12F FOR CLASS VII, CLASS II TAM ITEMS CONSTRAINED TO 90.0 PET DR 5141.00 CU FT

SQUARE OF PURLISHED TZE 15 26935-00 SO FT. CUNSTRAINED TO 90.0 PCT OR 24242.00 SO FT

(i)	SQUARE	MEIGHT SQUAR
		16.0
		11.0
		1832.0
		710.0
		9.0
		1830.0
-	598.0	570.0 598.0
_	5740.0	2750.0 5760.0
_	465.0	
_	71.0	2730.0 71.0
_	16895.0	13650.0 16895.0
_	555.0	14970.0 555.0
	0.976	2400.0 976.0
_	717.0	
		2.0
		3.0
		0.68
		24.0
		12.0
		530.0
		0.0
		0.0
		39.0
	0.25035	0.210.0

TODAYS DATE 03/03/76
OR INDEX(SQUARE) = 89.53
OR INDEX(CUBE) = 71.42
OR INDEX(TOTAL T/E) = 90.55

CONSTRAINED T/E FOR UNIT MINSH MOTOR TRANSPORT BATTALION, MARINE DIV

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

COUSTRAINED TO MS.0 PCT DR 4850.00 CU FT

SQUARE OF PUBLISHED TZE IS 26035.00 SO FT CONSTRAINED TO 85.0 PCT DR 22895.00 SO FT

-3ie:0	15 -4CY																															. 4				69.	NOTF.		112:t - M1650		Constraint = 85%			
****3/1	CUTE	0.74	1.0	4.0		3.0	1.6		0.4	2.0				350.0	R.0	6.0	2.0	c	1.0	1.0		25.0	40.0	17.0	6.2	4.0	0.0	15.0	0.	14.8	<b>u</b> •	5.2	0.	3.0	13.6	203.7	25.2	2.0	2.		16.3	2.0	4.2	6.44
A CHARGEOUCED TA											70.0	122.0	177.3								24.0																							
****	014	*	:	•	1:	3.	-		• 9	ď	1.	2.	3.	:	-	. 9	2.	-	:	-	:	:	. 4	٠,	20.	50.	33.	20.	*	8.	5.	34.		50.	50.	205.	4.	-	-	. 4	5.	4.5	-	:
CALT		4	•	C;	2	. 2	•	2	4	4	•	4	4	4	4	4	*	2	2	~	4	-	N	~	~	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	
1/5	>10	4	-	4	-	3	-	-	9	S	-	~	<b>m</b> )	-	-	ç	es.	-	••	-	-	-	4	4	50	50	04	50	4	80	2	40	4	50	50	274	4	-		4	s.	4	-	•
1/5	WEIGHT	183.0	20.0	48.0	45.0	0.0	10.0	45.0	132.0	280.0	4190.0	5070.0	8010.0	2575.0	139.0	120.0	26.0	20.0	25.0	15.0	2541.0	1750.0	830.0	560.0	0.00	120.0	120.0	140.0	0.4	480.0	15.0	40.0	4.0	40.0	0.04	4384.0	350.0	50.0	27.0	20.0	200.0	40.0	53.0	255.0
1/5	CUBE	12.0	1.0	0.4	1.0	3.0	1.0	1.0	6.0	5.0				350.0	8.0	6.0	2.0	0.1	1.0	1.0		55.0	0.04	17.0	6.2	3.6	10.8	15.0	0.	14.3	e.	2.8	0.	3.0	13.6	271.3	25.2	2.0	1.3	۴.	16.3	5-0	4.2	43.0
1/E	SQUARE										20.0	122.0	180.0								54.0																							
ITEM	WEIGHT	47.0	20.0	15.0	45.0	3.0	10.0	45.0	22.0	56.0	0.0614	2535.0	2570.0	2575.0	139.0	20.0	28.0	20.0	25.0	15.0	2641.0	1750.0	250.0	140.0	0.4	0.9	3.0	7.3	1.0	0.09	3.0	1.0	1.0	5.0	2.0	16.0	80.0	20.0	27.0	2.0	40.0	10.0	53.0	0.69
ITEM	CUBE	3.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0				350.0	8.0	1.0	1.0	1.0	1.0	1.0		55.0	10.0	4.2	۲.		.3	.8	0.	1.9	• 5		0.	• 5		1.0	6.3	2.0	1.3	-	3.3	5.	4.2	11.0
TEN	SOUARE										10.0	61.0	0.09								54.0											4												
	TAN	40030	A0320	104 40	40710	A0922	A1250	A1570	A1730	A1 400	41400	41020	41936	A1940	A2020	A2050	A2480	A2700	42710	A3280	30465	81280	91620	02620	01023	C2030	C2040	62050	65063	02070	00173	C2160	C2230	65255	62 110	C3020	54000	C4010	64015	02043	04040	C4143	04240	0 74 60

### MOTOR TRANSPORT BATTALION. MARINE DIV

# CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZF 15 5712-38 CU FT CONSTHAINED TO 85.0 PCT OR 4856-00 CU FT

SQUARE OF PUBLISHED TZE 1S 26025.60 S9 FT CUNSTRAINED TO 85.0 PCT OR 22895.00 S9 FT

1000				1							
STOPAGE	Contract	WE I CHI	SOUAKE	CUBE	WE I GHT	410		9 710	SOJASE	4600,	¥ 15 17 1
C4 190	7.7	90.09		23.0	180.0	r	-	3.		2.3.0	
04430	••	1.0		1.5	151.0	151	-	151.		¥ • 1	
Canso	3.0	85.0		3.0	85.0	-	-	:		3.0	
04040	15.0	204.0		12.0	204.0	-	-			15.0	
04470		0.9		1.4	0.9	-		1.		1.4	
C4430		2.0			2.0	-	-	1.		٠.	
	2.0	40.0		9.9	200.0	2	-	5.		9.6	
	7.7	40.0		38.4	200.0	2	-	5.		38.4	
C4 420	15.0	150.0		30.0	300.0	2	-	2.		30.08	
	0.0	85.0		51.0	680.0	ď	-	α°		51.0	
	3.6	8.0		53.4	120.0	15	-	15.		53.4	
	4.	12.0		1.4	48.0	*	-	. 4		1.4	
	3.9	0.36		3.9	95.0	-	-	:-		3.0	
	14.0	150.0		224.0	2400.0	16	-	14.		5.561	
C2030	15.0	250.0		45.0	750.0	3	-	3.		45.0	
C5030	4.0	196.0		4.0	196.0	-	-			4.0	
C5110	2.7	14.0		18.6	0.80	1	-	7.		18.6	
C5200	3.8	4.0		41.5	44.0		-			41.6	
	8.2	162.0		81.6	1620.0	10	-	10.		81.6	
	7.0	150.0		6.06	1950.0	13	-	13.		5.06	
	0.6	131.0		0.6	131.0	-	-	:		0.0	
	25.0	353.0		20000	2824.0	œ	-	æ.		200.0	
	4.3	38.0		34.2	304.0	80	-	9.		34.2	
	2.8	100.0	4	13.8	200.0	2	-	5.		13.P	
	1.5	31.0		5.8	124.0	4	1	•		5. P	
	• 5	7.0			45.0	9	1	.9		1.1	
	5.	2.0		2.0	20.0	4	1	•		2.0	
	11.0	150.0		11.0	150.0	-	-			11.0	
	6.3	107.0		25.2	428.0	4	-	٠,		25.2	
	5.9	140.0		88.0	2100.0	15		15.		80.0	
	7.2	257.0		35.9	1285.0	ıc	-	٦.		35.0	
	18.0	330.0		144.0	2640.0	00		ď.		144.0	
	119.0	2148.0		476.0	8592.0	4	-			179.7	
	1.5	62.0		45.0	1736.0	28	-	50.		30.5	· a
	6.9	0.05		27.5	360.0	4	-	4.		27.5	
	20.0	300.0		150.0	0.006	3	-	3.		150.0	
	6.	18.0		6.	13.0	-		:		0.	
	0.	1.0		٠.	37.0	37	-	37.			
	1.4	24.0		1.1	29.0	-	4	:		1.4	
38.0		1054.0	114.0		3162.0	3	4	3.	114.0		
	0.0	517.0		72.0	03060	18	-	18.		20.0	
1:9.0		5855.0	357.0		17563.0		*		337.9		

CONSTRAINED TIE FOR UNIT M1558

## MOTOR TRANSPORT BATTALION. MARINE DIV

CLATATE TZE FOR CLASS VII. CLASS II TAM ITEMS

COUST OF PUBLISHED TZE IS 5712-39 CU FT CONSTRAINED TO 45.0 PCT OR 4455.00 CU FT

SQUARE OF PUBLISHED TZE IS 26935.00 SO FT CONSTRAINED TO 85.0 PCT OR 22895.00 SO FT

PEFIC-	TENCY									14.	-		:::		5.				.6			15.				
******/1	CUBF	2.1	2.5	5.0	875.0	465.4	1.0	352.8										2.3	2.99	18.2	6.7	412.2	0.0	0.0		4856.0
RREDUCED	SOUARE								420.1	4385.5	392.3	71.0	14920.9	555.0	547.2	631.8										22895.0 4856.0
•	410	*	4.		7.	13.	3.	*	•	45.			85.	3.	11.	÷	•	19.	23.	14.	14.	15.	•	2.	-	1194.
CRIT		4	4		4		4	4	4	4	4	2	8	60	4	4	-	-	~	4	-	-	2	2	4	
1/5	710	4	4		1	13	3	4	13	9	S	-	96	3	91 .	£	4	61	31	14	-	30	4	2	-	1346
1/E	WE IGHT	64.0	64.0	77.0	12824.0	9230.0	24.0	7560.0	7410.0	165000.0	13550.0	2780.0	1311350.0	44910.0	38400.0	102750.0	9.0	57.0	2759.0	336.0	168.0	15900.0	0.0	0.0	39.0	5712.4 1830193.0
1/E	CUBE	2.1	2.5	5.0	875.0	465.4	1.0	362.8										2.3	91.8	18.2	6.7	840.0	0.0	0.0	::	5712.4
1/E	SOUAPE								598.0	5760.0	465.0	71.0	16896.0	555.0	0.910	717.0										26935.0
1154	WEIGHT	16.0	16.0	11.0	1832.0	710.0	A.0	1890.0	570.0	2750.0	2710.0	2780.0	13560.0	14970.0	2400.0	34250.0	2.0	3.0	89.0	24.0	12.0	530.0	0.0	0.0	39.0	
LTEM	CUBE	•5	9.	1.	125.0	35.8	r.	2.06									0.	-:	3.0	1.3	• 5	28.0	0.0	0.0	-:-	OTALS
ITEN	SGUASE								0.94	0.96	93.0	71.0	176.0	185.0	61.0	239.0										GRAND T
	744	00400	01400	00450	00725	50740	00100	02200	00800	99800	09860	06800	01030	01110	0110	01210	01250	ECOBO	E0980	E0430	E1120	E1150	E1155	E1156	E2030	

TODAYS DATE 03/02/76

OR INDEX(SQUARE) = 84.64

OR INDEX(CUBE) = 91.49

OR INDEX(IDTAL 7/E) = 88.35

MOTGE TRANSPURT HATTALION, MARINE DIV

CURTATE TZE FOR CLASS VII+ CLASS II TAM ITEMS

COUST OF PUBLISHED T/E IS 5712-38 CU FT CONSTRAINED TO 75.0 PCF OR 4294.00 CU FT SOUARE OF PUBLISHED T/E IS 26935.00 SO FT CONSTRAINED TO 75.0 PCT OR 20201.00 SO FT

DEFIC-												1.																							73.	NOTE:		Hait = M1658		Constraint = 75%			
TZE****	12.0	1.0	4.0	1.0	3.0	1.0	1.0	4.0	5.0				48.3	8.0	6.0	2.0	1.0	0.1	1.0		25.0	40.0	17.0	6.5	0.6	8.8	15.0	0.	14.8		2.4	0.	3.0	13.6	189.0	25.2	2.0	1.3	r) •	16.3	5.0	6.0	0.00
******EDUCED T.										69.5	109.5	148.1								54.0																							
0.77		:	4.		3.		1:	٠,	5.	1.	2.	2.	•0	1.	• 9	2.	:	:	1.	:	:	• •	. 4	20.	20.	31.	20.	. 4	æ.	٠,	34.	• •	20.	20.	191.	4	:	:	٠,	٠.٠	4.	:	4.
CRIT	4	4	2	2	. 2	4	2	4	4	4	4	4	4	4	4	4	2	2	2	4	1	2	2	-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	
17E 01Y	•	-	4	-		-	-	9	'n	-	2	٣	-	-	9	~	-	-	-	-	-	•	•	50	50	40	50	4	60	S	40	*	20	20	274	*	-	-	4	S	4	-	<
T/E WEIGHT	184.0	20.0	43.0	42.0	0.0	10.0	45.0	132.0	280.0	4190.0	5070.0	8010.0	2575.0	139.0	120.0	56.0	20.0	25.0	15.0	2641.0	1750.0	880.0	260.0	80.0	120.0	120.0	140.0	4.0	480.0	15.0	40.0	4.0	40.0	40.0	4384.0	320.0	50.0	27.0	20.€	20000	40.0	53.0	251.0
T/E CUBE	12.0	1.0	4.0	1.0	3.0	1.0	1.0	6.9	2.0				350.0	8.0	6.9	2.0	1.0	1.0	1.0		55.0	40.0	17.0	6.2	9.6	10.8	15.0	0.	14.8	۴.	2.8	0.	3.0	13.6	271.3	25.2	0.0	1.3	•	16.3	5.0	4 : 2	44.9
SQUARE										70.0	122.0	180.0								54.0																							
I TEM WE IGHT	47.0	20.0	12.0	45.0	3.0	10.0	45.0	22.0	26.0	4190.0	2535.0	2670.0	2575.0	139.0	20.0	28.0	20.0	25.0	15.0	2641.0	1750.0	220.0	140.0	0.4	0.9	3.0	7.0	1.0	0.09	3.0	1.0	1.0	2.0	2.0	16.0	80.0	20.0	27.0	5.0	0.04	10.0	53.0	0.4.9
I TEM CUBE	3.0	1.0	1.0	0.1	1.0	0.1	1.0	1.0	0.1				350.0	8.0	0.1	1.0	1.0	1.0	1.0		55.0	10.0	4.2	r.	5.	•3		•	1.9	• 5		0.	• 5		1.0	6.3	5.0	1.3	-:	3.3	• 5	4.2	11.0
SOUARE										70.0	61.0	0.09								54.0																							
TAN	A0030	A0.326	40499	A0716	20005	A1250	A1570	A1 730	41300	41300	41920	41930	A1940	A2020	A2050	A2480	A2700	A2710	A3280	80465	81280	81620	85250	C2010	C2030	C2040	C2050	C2060	C2070	00170	C2160	C2230	C2250	C2310	C3020	C4000	01040	640:5	C4020	C4040	C4140	04.230	C4 140

CONSTRAINED TZE FOR UNIT M1658

### NOTOR TRANSPORT BATTALION. MARINE DIV

# CURTATE TZE FUR CLASS VII. CLASS II TAM ITHMS

CUBS OF PURITSHED TAF IS STIP. 38 CU FT CONSTRAINED TO 25.8 PUT OR 4.244.00 CU FT

SQUARE OF OUBLISHED TZE IS 26935.00 SO FT CONSTRAINED TO 75.0 PCT OR 20201.00 SO FT

		1/E	1/5	177	1/6	CRIT	****		T/E****	DEFIC-
CUBE WEIGHT SQUARE	SQUARE		CUBE	WEIGHT	710		410	3011APE	CUPE	ADNIA
•	c		23.0	130.0	3		:		23.0	
			1.5	151.0	151	-	151.		1.5	
3.0 85.0			3.0	85.0	-	-	:		3.0	
50	0		12.0	201.0		-	:		15.0	
			• •	0.0			:			
0.5			2 8	0.00	<b>-</b> v		• u		~ .	
			19.4	2000	· "		ď		20.	
-			30.0	300.0	. ~				30.0	
	0		51.0	680.0	œ	-	•		51.0	
3.6 8.0			53.4	120.0	15	-	15.		53.4	
	0		1.7	48.0	4	-	. 4		1.4	
	0		3.9	0.56	-	-	:		3.9	
	0		224.0	2400.0	91	-	12.		170.4	
	0		45.0	150.0	m		3.		45.0	
-	0		0.4	196.0	-	-	:		0.4	
	0		18.6	0.86	~	-	۲.		10.6	
	0		41.6	44.0	=	-	11.		41.6	
8.2 162.0	0		81.6	1520.0	10	-	10.		81.6	
	0		9.06	1950.0	13	-	13.		9000	
	0		0.6	131.0	-	-	:		0.0	
25.0 353.0	0		200.0	2824.0	æ	-	8		200.0	
	0		34.2	304.0	œ	-	8.		34.2	
2.9 100.0	0		13.8	20000	S	-	5.		13.8	
E 3	0		5.8	124.0	*	-	•		5.8	
	0			45.0	c	-	• •		1:1	
	0		2.0	20.0	4	-	4.		5.0	
	0		11.0	150.0	-	-			11.0	
	0		25.2	428.0	4	-	•		25.2	
	0		88.0	2100.0	15	-	15.		86.4	
	0		35.9	1285.0	S		· 0		35.9	
	0		144.0	2640.0	00	-	•		144.0	
21	0		476.0	8535.0	4		:-		65.7	
	0		42.0	1726.0	28	-	19.		28.1	•
0.06 6.9	0		27.5	360.0	4	-	. 4		27.5	
50.0 300.0	0		150.0	0.006	٣	-	3.		150.0	
.9 18.0	0		6.	14.0	~	1			0	
	0		4.	37.0	37	-	37.			
1.4 28.0	0		1.4	28.0	-	4	:		4-1	
1054.0		114.0		3152.0	~	4		98.7		
			72.0	9306.0	1.9	-	15.		64.6	2.
5855.0	0	157.0		17555.0	n	•	٥.	258.7		:
:.4 . 21.6	0		5.4	6.41					5.5	

CONSTRAINED TIE FOR UNIT 41648

MOTOR TRANSPORT BATTAL ION. MARINE DIV

CURTATE TZE FUR CLASS VII. CLASS II TAM ITEMS

CUBE DE PUBLISHED IZE IS 5712.33 CU FT CONSTPAINED TO 75.0 PCT DR 4284.00 CU FT

SQUARE OF PUBLISHED TZE IS 26936.00 SO FT CUNSTRAINED TO 75.0 PCT UR 20201.00 SO FT

DEFIC-	TENCY									24.			10.		7.	:			10.			10.				
T/F***	CUBF	2.1	2.5	6.0	875.0	465.4	0.1	352.8									-	2.3	61.4	18.2	6.7	315.4	0.0	0.0	=	4284.0
*****REDJCED	SOUARE								359.2	3497.4	324.1	511.3	13635.8	544.7	540.3	480.6										22201.0
****	410	•	•	7.	7.	13.	3.	. 4	8	36.	3.	:	77.	3.	•	5.	. 4	19.	21.	14.	14.	11.	. 4	2.	-:	11411
CRIT		4	4	4	4	4	4	4	*	4	4	2	8	8	4	4	1	-	2	4	-	-	2	2	4	
1/E	917	4	4	1	1	13	3	4	13	60	2	-	96	3	91	3	4	10	31	14	14	30	•	2	-	1346
1/E	WEIGHT	64.0	64.0	77.0	12824.0	9230.0	24.0	7560.0	7410.0	165000.0	13550.0	2780.0	1311360.0	44910.0	33400.0	102750.0	8.0	57.0	2759.0	336.0	168.0	15900.0	0.0	0.0	39.0	5712.4 1830193.0
17.6	CUBE	2.1	5.5	5.0	875.0	465.4	1.0	362.8									:	2.3	91.8	18.2	6.7	840.0	0.0	0.0	::	5712.4
1/6	SOUARE								599.0	5760.0	465.0	71.0	16896.0	555.0	0.910	717.0										26935.0
ITEM	WEIGHT	16.0	16.0	11.0	1832.0	710.0	8.0	1890.0	570.0	2750.0	2710.0	2730.0	13660.0	14970.0	2400.0	34250.0	2.0	3.0	89.0	24.0	12.0	530.0	0.0	0.0	39.0	
ITEN	CUBE	5.	9.		125.0	35.8	•3	2.06									0.		3.0	1.3	••	28.0	0.0	0.0	1:1	OTALS
ITEN	SOUARE								45.0	0.96	93.0	71.0	176.0	185.0	61.0	239.0										GRAND TO
	TAN	00400	01400	20420	90725	09100	00100	02200	00400	D0860	06800	06800	01030	0:110	01160	01210	01250	EOUBO	06603	E0690	E1120	51150	E1155	E1156	£2030	

TODAYS DATE 03/02/76
0R INDEX(SQUARE) = 74.92
0R INDEX(CUBE) = 89.09
0R INDEX(TOTAL T/E) = 82.60

## S-INCH HOWITZER BATTERY (SP). FORCE TROUPS

CUSTATE THE FOR CLASS VII. CLASS II TAM ITHMS

CONSTRAINED TO SCHOOL DESTRUCTOR CONSTRAINED TO SCHOOL CONSTRAINED TO SCHOOL DESTRUCTOR AND SCHOOL DESTRUCTOR AND SCHOOL DESTRUCTOR OF THE SCHOOL

SQUARE OF PUBLISHED TZE IS 11027.00 SO FT CONSTRAINED TO 20.0 PCT OR 9924.00 SO FT

-51936-	* P. M. C. *																																NOTE:		Unit = M4112	Constraint = 90%	1							-1	
1/50000	CUPE	12.0	0.0	0.4	1.0	3.0	0.4	6.4	1.0	0.0	1.0	3.0	0.6	6.0	3.0	c	C	c	700.0	24.0	40.0	3.0	17.0		12.9	4.0	1.0	1.0		0.4		•		0	10.0	23.0	2031.2	35.0	•	1.0		c	145.0	410.1	
****** DEDICED I/FO***	SOJARE															140.0	183.0	60.0						354.7							54.0		12.0	22.0							378.7	36.0			
***	017		.0	4.	:	:	4.		:	1.		3.	4	.8.	9	2.	3.	-	2.	3.	5.	•	17.	٠,	. 5	•	-	-	<u>:</u>	-	-	-1	2.		-	-	2.	3.	3.	-		3.	u .	Ċ.	
CRIT		£		4	4	. 4	4	4	4	4	4	4	4	8	8	8	80		œ			80				œ	4	*	4	•	4		4	4	2	4	60	α	4	4					
1/5	OTY	*	0	4	1		4	9	-	-	1		*			2										4	-	1	-	•	-	-	2	-	-	-	3	3	3	-	3			10	
1/E	WE IGHT	188.0	180.0	48.0	42.0	0.96	12.0	78.0	25.0	252.0	10.0	135.0	180.0	132.0	168.0	8380.0	7605.0	2470.0	5150.0	303.0	695.0	0.69	340.0	20220.0	330.0	112.0	20.0	25.6	15.0	110.0	2641.0	2.0	570.0	3560.0	220.0	425.0	45800.0	165.0	3.0	68.0	142950.0	9495.0	50.0	6.63	
1/5	CUBE	12.0	0.6	6.0	1.0	3.0	0.4	6.0	1.0	8.0	1.0	3.0	4.0	6.0	3.0				20000	24.0	40.0	3.0	17.0		12.0	4.0	1.0	1.0	1.0	4.0		-			10.0	23.0	2439.0	36.0	-	**:			155.0	V . O . V	
1/10	SQUARE															1.0.0	183.0	60.0						350.0							54.0		15.0	22.0							457.0	0.05			
ITEM	WEISHT	47.0	20.0	12.0	42.0	0.96	3.0	13.0	26.0	252.0	10.0	45.0	45.0	22.0	26.0	4190.0	2535.0	2670.0	2575.0	101.0	139.0	23.0	20.0	3370.0	55.0	28.0	20.0	25.0	15.0	110.0	2641.0	4.0	285.0	3560.0	220.0	425.0	15600.0	55.0	1.0	89.0	47650.0	3165.0	0.4	0	
TLEM	CUBE	3.0	0.1	1.0	1.0	3.0	1.0	1.0	1.0	8.0	1.0	1.0	1.0	1.0	0.1				350.0	8.0	8.0	1.0	1.0		2.0	1.0	1.0	1.0	1.0	4.0		-			10.0	23.0	813.0	12.0	0.	1.4			31.0	40.0	
ITEN	SOUARE															10.0	61.0	0.09						0.09							54.0		6.9	22.0							153.0	12.0			
	TAM	40090	A0120	00000	207:0	A0730	40922	41043	41150	41240	V:250	41570	41536	41730	AIRCO	41000	41720	41930	AISAO	A2010	42020	42040	A2050	A2182	A2184	42480	A2700	42710	A3290	40030	80465	90510	30780	99999	61620	91840	95110	95:50	55.325	82340	29424	65.705	01023	65423	

### CONSTRAINED THE FOR UNIT MAILS

8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

CURTATE TZE FOR CLASS VII. CLASS !! TAM ITEMS

CORSTRAINED TO 90.0 PCT OR 6623.00 CU FT SQUARE OF PUBLISHED TZF IS 11027.00 SO FT CONSTRAINED TO 90.0 PCT OR 9924.00 SO FT

	DEF IC-																																											
	CUBE	270.0	337.6	0.	14.8	1.	1.	0.	. 8	3.4	12.6	2.0	.2	3.3	2.0	4.2	77.0	7.7	7.7	a.	24.0	1.4		2.0	7.7	45.0	19.1	30.2	3.9	189.8	10.5	15.0	2.7	21.3	22.7	16.3	27.A	0.0	100.0	17.1	16.6		1.0	
	**************************************																																											
	* >	10.		4	8	4	10.		.5	2.	2.	-	2.	:	4		7.	-	:	80.	=	-	-	-	-	3.	3.	=	-	14.	15.	-	-	8.	• •	5.	4.	-			\$			
	C8 11	-		-	-	. 1	-	-	-	-	-	-	-	-	1		-	-	-	-	-	-	-	-	-	,	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-	
!	1/E	10	r	4	8	4	10	-	S	5	2	-	2	-	4	-	1	-	-	80	-	-	-	-	-	2	•	=	-	1.4	13	-	-	8	٠	2	4	-	4	•	ç	•	0	,
!	WE I GHT	30.0	35.0	4.0	480.0	12.0	10.0	1.0	10.0	10.0	160.0	20.0	10.0	40.0	40.0	63.0	448.0	60.09	60.09	80.0	400.0	6.9	2.0	40.0	40.0	450.0	255.0	0.00	0.56	2100.0	75.0	250.0	127.0	112.0	24.0	324.0	60000	131.0	1412.0	152.0	0.009	23.0	14.0	21.4 0
	CUBE	270.0	375.0	0.	14.8			0.	5.	3.4	12.6	5.0	.2	3.3	2.0	4.2	77.0	7.7	7.7		26.0	1.4		2.0	7.7	45.0	19.1	39.5	3.3	196.0	19.5	15.0	2.7	21.3	22.1	16.3	87.3	6.6	100.0	17.1			1.0	
	SQUARE																																											
	METGHT	3.0	7.0	1.0	0.09	3.0	1.0	1.0	2.0	2.0	80.0	20.0	2.0	40.0	10.0	53.0	54.0	60.09	0.09	1.0	400.0	0.9	2.0	40.0	40.0	150.0	85.0	8.0	0.50	150.0	2.0	250.0	127.0	14.0	0.4	162.0	150.0	131.0	353.0	38.0	100.0	7.0	7.0	101101
	CUBE	27.0	75.0	0.	1.9	.2		0.	.2	1.	6.3	2.0	:	3.3	• 5	4.2	11.0	7.7	7.7	0.	26.0	1.4	• 2	2.0	7.7	15.0	6.4	3.6	3.9	14.0	1.3	15.0	2.1	2.7	3.8	8.2	7.0	0.6	25.0	4.3	2.8	• 5	٠.	1.1
	SOUARE																																											
	144	52040	62050	C2050	C2070	65100	52150	C2230	C2256	011:23	64000	01000	020+3	C4040	C4140	C4250	C4340	64330	C4390	C4436	CAAKO	07840	C4 680	C4490	C4790	C4820	C4870	C4430	09640	C4980	06640	08053	C5100.	C3110	00250	C5320	C5400	01950	C5420	02850	C2330	(0140	02230	01210

A-INCH HOWITZER BATTERY(SP), FORCE TROOPS

# CUSTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

COURT OF PUBLISHED TZE 15 7353-05 CU FT COUNTY ALMS A 14 46-0 PCT NO FOR 16,24-00 CU FT

SQUARE OF PUBLISHED TZE IS 11027.00 SO FT CONSTRAINED TO 90.0 PCT OR 9424.00 SO FT

	> \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \																											:					3.	1:					3.					
*****/1	CUBE	23.7	4.4.6	144.0	113.6	3.0	4.0	0.05	α		1.4			20.0	12.0	15.0		1.4	5.	4.	1.4	125.0	35.8	.3	0.	4000									*		0.	m	441.0	15.0	k.0	4.0	0.	
* GEOLGEO F												125.0	39.0				119.0										321.0	1018.3	44.0	372.0	71.0	804.8	2955.2	447.2	451.7	220.4								
****	710	16.	c	. 8		3.		-1	3.	32.	:	-	:	:	3.	3.	:	-1		-1		:	:		1:	:	7.	:	:	•	:		14.	2.	8.	:	-	-		3.	9	7.		.,
Colt		-	-	-	1	1	-	1	-	-	4	60	4	4	4	4	4	4	4	4	4	4	•	4	4	4	œ	8	8	ď	4	8	8	4	<b>c</b>	4	1	-	-	cı	4	c	-	5"
1/1	710	97	0	2	N	3	-	-	3	32	-	-	-	-	m	۳	-	1	-	-	8	-	-	-	-	-	~	12	-	4	-	1	17	n	ď	-	-	-	14	3	٧	1	2	-
176	WE LGHT	2240.0	2313.0	0.0475	4245.0	36.0	0.06	300.0	54.0	32.0	28.0	2650.0	1054.0	163.0	1551.0	2334.0	5855.0	21.0	16.0	16.0	22.0	1832.0	710.0	8.0	1.0	1899.0	30000	33000.0	0.019	10840.0	2780.0	51590.0	336600.0	44910.0	19200.0	34250.0	2.0	15.0	0.86	315.0	60.05	245.0	2.0	6111.0
175	CUAF	93.9	64.0	144.0	234.0	3.0	6.5	20.0	5.3	•3	1.4			20.0	12.0	15.0		1.4	• 5	٠.	1.1	125.0	35.4	•3		2.06											0.	• 3	545.0	15.0	6.0	7.0		53
1/5	SQUARE											125.0	38.0				119.0										322.0	1152.0	44.0	372.0	71.0	938.0	3502.0	255.0	œ	234.0								
1TEM	WE IGHT	140.0	257.0	330.0	2148.0	12.0	0.00	300.0	18.0	1.0	28.0	2650.0	1054.0	163.0	217.0	778.0	5855.0	21.0	16.0	16.0	11.0	1832.0	210.0	8.0	1.0	1890.0	220.0	2750.0	610.0	2710.0	2780.0	7370.0	19800.0	14970.0	2400.0	34250.0	2.0	15.0	7.0	105.0	10.0	35.0	1.0	6111.0
1154	CUBE	8.9	7.2	18.0	110.0	1.0	6.9	20.0	6.	0.	1.4			20.0	4.0	2.0		1.4	• 2	9.	.7	125.0	35.8	۴.	•	2.06											0.	• 3	30.0	2.0	1.0	1.0	0.	54.0
ITEM	SCUARE											125.0	38.0				119.0										46.0	0.96	0.00	93.0	71.0	134.0	5000	195.0	0.10	239.0								
	144	56183	62.430	Citad	02450	00540	01562	05943	02997	C6684	02000	00000	06000	00100	02110	00100	00100	061.00	00400	01400	20420	20125	20740	06750	59400	20170	00840	09800	00875	00880	06800	01050	01050	01110	09110	01210	01250	E DUSO	E0000	50170	£0100	E0205	01203	0.25.0

8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUME OF PUBLISHED TZE 1S 7359-05 CU FT CONSTRAINED TO 90-0 PCT OR 6623-00 CU FT

SQUARE OF PUBLISHED TZE IS 11027.00 SO FT CONSTRAINED TO 90.0 PCT UR 9924.00 SO FT

DEF 10-	TENCY																	
****5/1	CUBE	12.0		0.0	17.8	7.8	5.9	168.0	24.0	37.0					1.1	124.0	4.0	18.0
BEDICED .	OTY SOUARE		1393.4										193.5					
****	>10	3.		10.	,	.9		.,	3.	. 4	2.	3.	1:	-			-	:
CRIT		2	80	4	4	4	-	1	60	œ	4	œ	2	9	4	4	4	4
	710	٣	ç	01	9	\$	9	٠	٣	4	2	3	-	-	-	-	-	-
1/5	WE I GHT	240.0	351000.0	0.0	534.0	144.0	72.0	3180.0	4.50.0	240.0	2.0	0.6	48449.0	0.40	3.9.0	1960.0	200.0	365.0
TVE	CUBE	12.0		0.0	17.8	7.8	5.9	158.0	24.0	37.9	-	3.0		10.0	1:1	124.0	4.4	18.0
TVE	SOUARE		1518.0										218.0					
ITEM	METGHT	RO.0	58500.0	0.0	89.0	24.0	12.0	530.0	150.0	0.09	1.0	3.0	48449.0	94.0	39.0	1960.0	20000	365.0
LTEN	CUBE	0.4		0.0	3.0	1.3	5.	28.0	8.0	6.5	0.	1.0		10.0	1.1	124.0	4.4	18.0
LTEM	SOUNAE		253.0										218.0					
	1 44	E0230	60490	50405	50930	6660E	E1120	£1150	E1165	E1200	E1240	E1250	E1375	E1390	E2030	52030	53120	E3170

TODAYS DATE 03/03/76
OP INDEX(SQUAPE) = 92.88
OP INDEX(CUBE) = 99.30
OR INDEX(TOTAL I/E) = 97.25

631. 9924.9 6623.0

11027.0 7359.0 1239869.0 644

GRAND TOTALS

### CONSTRAINED THE FOR UNIT MAILS

## 8-INCH HOWITZER BATTERY(SP), FORCE TROODS

CURTATE TZC FIR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE 1S 7330.05 CU FT CUNSIPAINED TO 85.0 PCT OR 6255.00 CV FT

SQUARE OF PUBLISHED TZE IS 11027.00 SO FT CONSTRAINED TO 95.0 PCT OR 9373.00 SO FT

DEFIC-	TF NCV																														NOTE.	more:	Unit = M4112		Constraint = 85%								٥.
T/F***	CUBE	12.0	0.0	0.4	1.0	3.0	4.0	6.0	1.0	6.9	1.0	3.0	4.0	6.0	3.0				20007	24.0	40.0	3.0	17.0		15.0	4.0	1.0	0.		0.0		:		10.01	23.0	1927.4	36.0	-	1.4			155.0	344.5
*********	SZUARE															140.0	183.0	60.09						338.7							24.0	12.0	22.0							327.8	34.5		
****	017	4	.0	4.	:	-	. 4	•	1.		-	3.	4	• 9	3.	2.	3.	-	٠,	3.		3.	17.	•	•	4	-	•	: .	: .	: .		-	:	-		3.	۴)	-	5.	3.		• a
CRIT		8	60	•	4	4	4	4	4	4	*	4	4	8	œ	œ	8	80	ю	œ	60	60	80	œ.	æ	80	•	<b>.</b>		* <	, 0	1 4	*	2	4	8	00	•	4	4	4	-	
1/5	410	4	6	4	-	-	•	9	-	-	-	n	4	•	m	8	6	-	2	2	S	2	17	ç	ç	4						. (1	-	•••	-	3	т	n	-	2	3	r	10
1/5	WEIGHT	189.0	180.0	48.0	42.0	96.0	12.0	78.0	26.0	252.0	10.0	135.0	180.0	132.0	158.0	8380.0	1605.0	2670.0	2150.0	303.0	695.0	0.69	340.0	20220.0	330.0	112.0	20.0	0.62	0.00	2641	0.00	570.0	3560.0	220.0	425.0	46800.0	165.0	3.0	88.0	142950.0	0.5040	20.0	0.0.
1/E	CUBE	12.0	0.0	6.4	1.0	3.0	4.0	6.0	1.0	8.0	1.0	3.0	4.0	6.0	3.0				20000	24.0	40.0	3.0	17.0		12.0	4.0	1.0	•	0.1	•	•			10.0	23.0	2439.0	36.0		1.4			156.0	480.0
1/F	SOUARE															140.0	183.0	0.09						360.0						54.0		12.0	22.0							459.0	36.0		
ITEM	WEIGHT	47.0	20.0	12.0	45.0	0.56	3.0	13.0	26.0	252.0	10.0	45.0	45.0	22.0	0.95	4190.0	2535.0	2670.0	2575.0	101.0	139.0	23.0	20.0	3370.0	55.0	28.0	20.00	0.62	110-0	2641.0	2.0	285.0	3560.0	220.0	425.0	15600.0	85.0	1.0	89.0	47650.0	3165.0	4.0	0.4
ITEM	CUBE	3.0	1.0	1.0	1.0	3.0	1.0	1.0	1.0	8.0	1.0	1.0	1.0	1.0	1.0				350.0	8.0	8.0	1.0	1.0		2.0	0.1	0.1		9					10.0	23.0	813.0	12.0	0.	1.4			31.0	48.0
MUL1	SOUARE															20.0	61.0	0.09						0.09						54.0		0.9	22.3							153.0	12.0		
	1 A 4	A0090	AG320	A0490	A0710	A0730	A0422	A1083	A1:80	A1240	A1250	A1570	A1630	A1730	ATHOR	A1400	41920	A1 730	91940	A2010	A2020	42040	A2050	A2182	A2164	A2480	A2700	00000	00000	30465	80510	90780	99999	91420	H1640	92110	62160	32322	82330	32462	30126	62010	07040

CONSTRAINED TZE FOR UNIT M4112

8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

CURTATE TZE FOR CLASS VII. CLASS II TAM TTEMS

CUBE OF PUBLISHED 17F 15 7359.05 CU FT CONSTRAINED TO 85.0 PCT UP 6255.00 CU FT

SQUARE OF PUBLISHED TZE IS 11027.00 SQ FT CONSTRAINED TO 85.0 OCT OR 9373.00 SQ FT

116 6 1 7-	1 P NCY		:																											:														
1/1:	CURE	279.0	318.9	0.	14.8	1.	1.	c.	۵.	3.4	12.6	2.0	2.	3.3	2.0	4.2	77.0	7.7	7.7	.8	26.0	1.4	.2	5.0	7.7	45.0	1001	30.5	3.9	186.7	19.5	15.0	2.7	21.3	72.7	16.3	27.8	0.6	100.0	17.1	16.6		0.1	17.5
*ACOUCED																																												
****	410	10.	4	4.		4.	10.	:	٠,	5.	2.			-		.:	7.	-	-	80.	-	-	-	-	:	3.	3.	11.	-	13.	15.	-	1.	8	• 9	2.	4.	-			.6	4.	. 2	2.
CRIT		•	-	-	-	-	-	-	1	1	-	-	-	-	-	-		-	-	-	-	-			-	-	-	-	-	-	-	-	-	-	-	-	1		-	-	-		1	-
1/5	710	10	2	4	ဇာ	4	10	-	S	2	2	-	~	-	4	-	1	-	-	90	-	-	-	-	-	3	3	=	-	14	15	-	-	60	9	~	4	-	4	4	•	4	2	c,
1/5	WE I GHT	30.0	35.0	4.0	480.0	15.0	10.0	1.0	10.0	10.0	160.0	20.0	10.0	40.0	40.0	53.0	448.0	0.09	0.09	80.0	400.0	0.9	2.0	40.0	40.0	450.0	255.0	88.0	0.50	2100.0	15.0	250.0	127.0	112.0	24.0	324.0	0.009	131.0	1412.0	152.0	6.000	23.0	14.0	214.0
1/E	CUBE	270.0	375.0	0.	14.8			0.	.8	3.4	12.6	2.0	• 5	3.3	2.0	4.2	77.0	7.7	7.7	. 8	26.0	1.4		2.0	7.7	45.0	161	39.5	3.9	196.0	19.5	15.0	2.7	21.3	22.7	16.3	27.8	0.6	100.0	17.1	15.6		1.0	13.5
1/1	SOUARE																																											
ITEM	WE IGHT	3.0	7.0	1.0	0.09	3.0	1.0	1.0	2.0	2.0	80.0	20.0	5.0	40.0	10.0	53.0	64.0	60.09	0.09	1.0	400.0	0.9	2.0	40.0	40.0	150.0	85.0	8.0	0.56	150.0	2.0	250.0	127.0	14.0	4.0	162.0	150.0	131.0	353.0	38.0	100.0	0.7	3.6	107.0
LTEM	CUBE	27.0	75.0	0.	1.9	.2		0.	• 5		6.3	2.0	:	3.3	• 5	4.2	11.0	7.7	7.7	0.	26.0	1.4	•2	2.0	7.7	15.0	6.4	3.6	3.9	14.0	1.3	15.0	2.7	2.7	3.8	8.2	7.0	0.0	25.0	4.3	2.8	• 5	5.	5.5
7311	SCUARE																																											
	* 4 *	62040	03077	09020	C.2070	C2:00	52160	02230	C2250	C2.310	54000	04010	C4020	C4040	C4140	C4250	C4.340	066 43	C4390	C4436	C4450	C4670	C4680	06940	C4 790	C4826	C4470	C4880	C4960	64930	06640	08053	C2100	C5110	C5200	C5320	C5400	C5410	25820	C5870	05650	CV140	C62240	07110

## 8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

# CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE IS 7359-05 CU FT CONSTRAINED TO 85-0 PCT OR 6255-00 CU FT SQUARE OF PUBLISHED TZE IS 11027-00 SO FT CUNSTRAINED TO 85-0 PCT OR 9373-00 SO FT

DEFIC-	IE NC				2.																							2.					3.	:	:				4.					
1/F****	CUBE	93.5	64.6	144.0	30.05	3.0	0.4	20.0	2.8		1.4			20.0	12.0	15.0		4:1	• 5	۷.	1.4	125.0	35.8	•.3	0.	4.00											0.	r.	349.8	15.0	6.0	7.0	0.	54.0
*********												125.0	38.0				106.4										308.9	0.540	6.44	358.3	70.3	859.6	2855.9	333.5	447.3	178.3								
****	710	16.	3.		• 0	3.	:	1.	3.	32.	:			-	3.	3.	•	-	:	-	2.	:	:	:	:	-1	7.	10.	:	4.	:	• •	14.	2.	7.	:-	:	:	10.	in		7.		:
CRIT		-	-	-	-	-	1	-	-	-	4	60	4	4	•	4	4	4	4	4	•	4	4	4	4	4	80	60	8	8	4	8	œ	4	0	4	-	-	-	2	4	6	-	c
1/5	410	16	0	œ	2	19	-	-	3	32	-	-	-	-	3	3	-	-	-	-	~	-	-	-	-	-	1	12	-	•	-	1	17	3	ď	-	-	-	14	r	٤	1	~	-
1/E	WEIGHT	2240.0	2313.0	2640.0	0.296.0	35.0	0.06	300.0	54.0	32.0	28.0	2650.0	1054.0	163.0	1551.0	2334.0	5855.0	21.0	16.0	16.0	22.0	1832.0	710.0	8.0	1.0	1890.0	3990.0	33000.0	610.0	10840.0	2780.0	51590.0	336600.0	44910.0	19200.0	34250.0	2.0	15.0	0.86	315.0	0.09	245.0	5.0	511.0
1/5	CUBE	93.9	64.6	144.0	238.0	3.0	6.9	20.0	2.3	.3	1.4			20.0	12.0	15.0		1.4	.5	9.	1.4	125.0	35.8	•3	0.	4.06											0.	.3	546.0	15.0	6.0	7.0	· ·	24.0
T/E	SQUARE											125.0	38.0				119.0										322.0	1152.0	44.0	372.0	71.0	933.0	3502.0	255.0	488.0	239.0								
ITEM	WEIGHT	140.0	257.0	330.0	2148.0	12.0	0.06	300.0	18.0	1.0	28.0	2650.0	1054.0	163.0	517.0	778.0	5855.0	21.0	16.0	16.0	11.0	1832.0	710.0	8.0	1.0	1890.0	220.0	2750.0	610.0	2710.0	2780.0	7370.0	19800.0	14970.0	2400.0	34250.0	5.0	15.0	2.0	105.0	10.0	35.0	0.1	0.11.
ITEM	CUSE	5.9	7.2	18.0	119.0	1.0	6.9	20.0	6.	0.	1.4			20.0	4.0	2.0		1.4	• 5	9.	.7	125.0	35.8	•3	0.	2.06											••	.3	33.0	2.0	1.0	1.0	0.	24.0
ITEN	SQUARE											125.0	38.0				119.0										46.0	0.96	44.0	93.0	71.0	134.0	206.0	185.0	61.0	239.0								
	TAM	C6398	C6340	06410	C4420	00490	C6510	05990	02490	66684	02000	09000	06000	00100	00170	09166	06100	06800	00400	01400	02450	00725	00140	09200	00765	00170	09860	09400	00875	09800	00800	02010	01030	01110	01110	01210	01250	E0020	60003	E0170	E0140	E0203	E0210	E02.40

CONSTRAINED TZE FOR UNIT MAILS

8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CURE OF PUBLISHED TZE IS 7359.05 CU FT CONSIGNAINED TO H5.0 PCT OR 6255.00 CU FT

SQUARE OF PUBLISHED TZE IS: 11027.00 SO FT CONSTRAINED TO 85.0 PCT OR 9373.00 SO FT

PEF IC-	AUNEL		:																
*****/L	CUSE	12.0		0.0	17.8	7.8	5.0	168.0	24.0	37.9	•	3.0			::	124.0	4.4	18.0	
*****	SOUARE		1317.9										120.5						!
****	9T.Y	3.	5.	10.	.6.	.9	• 9	.9	3.	. 4	2.	3.	-	-	-	:	-	:	
1143		~	œ	4	4	*	-	-	00	œ	4	8	~	82	4	4	4	4	
1/5	710	8	9	01	9	9	ď	9	6	4	~	3	-	-	-	-	1	-	
1/E	WE I GHT	240.0	351000.0	0.0	534.0	144.0	72.0	3180.0	450.0	240.0	2.0	0.6	48443.0	94.0	39.0	1960.0	200.0	365.0	
TZE	CUBE	12.0		0.0	17.9	7.8	2.9	168.0	24.0	37.9	••	3.0		10.0	::	124.0	4.4	18.0	
1/E	SOUARE		1518.0										218.0						
ITEM	WEIGHT	90.0	58500.0	0.0	89.0	24.0	12.0	530.0	150.0	0.09	1.0	3.0	48448.0	0.46	39.0	1960.0	200.0	365.0	
ITEM	CUBE	4.0		0.0	3.0	1.3	• 5	28.0	8.0	9.6	0.	1.0		10.0	1.1	124.0	4.4	18.0	
I TEM	SOUARE		253.0										218.0						
	124	09763	06903	26803	0860	06603	1120	1150	1165	1200	1240	1260	1375	1 390	2030	2090	3150	3170	

TODAYS DATE 03/02/76
OR INDEX(SQUARE) = 89.21
OR INDEX(CUBE) = 98.96
OR INDEX(TOTAL T/E) = 95.84

CONSTRAINED TZE FOR UNIT MAILS

8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS CURE OF PUBLISHED TZE IS 7353.05 CU FT CONSTRAINED TO 75.0 PCT OR 5519.00 CU FT

SQUARE OF PUBLISHED TZE IS 11067-00 SO FT CONSTRAINED TO 75-0 PCT OR 8270-00 SO FT

																											NOTE.		Wait = 4.119		Constraint = 75%													
DEFIC-	• JN 31																							:			N		11.	5	Ö						:							٠
/F****	CURE	12.0	0.0	0.0	1.0	3.0	4.0	6.0	1.0	c . x	1.0	3.0	4.0	0.4	3.0				700.0	24.0	0.04	3.0	17.0		12.0	4.0	1.0	1.0	1.0	0.4		:			10.0	23.0	1721.5	36.0	:	1.4			155.0	240.8
**************************************	SOUADE															131.8	177.6	60.09						314.2							42.6		12.0	21.4							225.9	40.02		
****	014		•		:	-	•	.9	1.	:	-	3.	*	• •	3.	2.	3.	1.	2.	3.		3.	17.	5.		4.	-:	:		-	:	1.	5.	:	:	:	2.	3.	3.	:	-	3.1	٢.	• 5
CPIT		80	60	4	4		4	4	•	4	4	•	4	82	<b>&amp;</b>	8	80	80	ю	60	6	80	æ	80	8	8	4	4	4	3	4	2	4	4	2	4	8	8	4	4	4	4	1	-
1/6	977	•	6	4	-	-	•	4	-	-	-	n	4	c	<b>۴</b>	~	m	-	~	•	co	m	17	9	\$	4	-	-	-	-	-	-	~	-	-	-	3	r	n	-	3	3	ľ	01
1/E	WE IGHT	188.0	190.0	45.0	42.0	0.96	15.0	78.0	26.0	252.0	10.0	135.0	180.0	132.0	168.0	8380.0	1605.0	2670.0	5150.0	303.0	695.0	0.69	340.0	20220.0	330.0	112.0	20.0	25.0	15.0	110.0	2641.0	2.0	570.0	3560.0	220.0	425.0	45800.0	165.0	3.0	68.0	142950.0	9495.0	20.0	0.00
1/E	CUBE	12.0	0.0	0.4	1.0	3.0	0.4	0.9	1.0	8.0	1.0	3.0	4.0	0.9	3.0				200.0	24.0	40.0	3.0	17.0		12.0	0.4	1.0	1.0	1.0	4.0		-			10.0	23.0	2439.0	35.0	:	1.4			155.0	0.000
1/5	SOUARE															140.0	183.0	0.09						350.0							54.0		12.0	22.0							459.0	36.0		
ITEM	WEIGHT	47.0	20.0	12.0	45.0	0.96	3.0	13.0	26.0	252.0	10.0	45.0	45.0	22.0	26.0	4190.0	2535.0	2670.0	2575.0	101.0	130.0	23.0	20.0	3370.0	25.0	28.0	20.0	25.0	15.0	110.0	2641.0	2.0	285.0	3560.0	220.0	425.0	15600.0	55.0	1.0	0.84	47650.0	3165.0	0.4	0.,
ITEM	CUBE	3.0	1.0	1.0	1.0	3.0	0.1	1.0	1.0	8.0	1.0	0.1	1.0	1.0	1.0				350.0	8.0	8.0	1.0	0.1		2.0	0.1	1.0	1.0	0.1	4.0		-			10.0	23.0	813.0	12.0	0.	1.4			31.0	0.84
ITEN	SGUARE															10.0	61.0	0.09						0.09							54.0		6.0	55.0							153.0	12.0		
	TAM	A0050	A0 320	00000	AC 7 10	A3730	A0922	A1 083	A1100	A1240	A:250	41570	A1630	41730	A1 850	A1900	A1920	A1930	41040	A2010	A2020	A2040	A2050	A2182	A2184	A2400	A2700	42710	13280	90000	80408	90510	30780	80480	61620	91640	H2110	35.66	32 322	82.180	62462	82705	C1073	67073

## 8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

CURIATE TZE FOR CLASS VII. CLASS IT TAM ITEMS

COUSTRAINED TO 75.0 PCT OR 5519.00 CU FT

SQUARE OF PURLISHED TZE IS 11027.00 SQ FT CONSTRAINED TO 75.0 PCT OR 8270.00 SO FT

DEFIC-	TENCY	:	.,																											2.														
T/F***	CUBE	233.6	44.0	0.	14.8			0.	œ.	3.4	12.6	2.0	٠.	3.3	2.0	4.2	77.0	7.7	7.7	8.	26.0	1.4	2.	2.0	7.7	45.0	1001	30.2	3.9	166.0	10.5	15.0	7.7	21.3	22.7	16.3	27.8	0.0	100.0	17.1	16.6		0.1	15.5
*PEDUCED																																												
****		.6	-	4	9.	4.	10.	-	٠,	5.	2.	-	2.	:	4.	-	7.	:	-	80.	1.	:	-	:	:	3.	3.	::-	:	12.	15.	-	-	ά.	• 9	2.		:	4.	4.	.9	. 0	2.	
CRIT		-	-	-	-	. 1	-	-	-	-	7	-	-	-	-	-		-	-	-	1	-	-	1	-	-	-	-	-	-	7	1	-		-	-	-	-	-	-	-	-	1	-
	OTY	10	2	4	80	4	01	-	2	S	2	-	2	-	4	-	1	-		80	-	-	-	1	-	3	3		-	14	15	-	-	00	9	2	4	-		4	9	4	2	6
1/E	WEIGHT	30.0	35.0	4.0	480.0	12.0	10.0	1.0	10.0	10.0	160.0	20.0	10.0	40.0	40.0	53.0	448.0	0.09	0.09	80.0	400.0	6.0	2.0	40.0	40.0	450.0	255.0	94.0	0.50	2100.0	75.0	250.0	127.0	112.0	24.0	324.0	60000	131.0	1412.0	152.0	0.009	0.45	14.0	210.0
17.6	CUME	27002	375.0	0.	14.8			0.	.8	3.4	12.6	2.0	• 5	3.3	2.0	4.2	77.0	7.7	7.7	• 8	26.0	1.4	• 5	2.0	7.7	45.0	19.1	30.5	3.9	196.0	19.5	15.0	2.7	21.3	22.7	15.3	27.8	6.0	100.0	17.1	16.6		1.0	12.0
TZE	SQUARE																																											
ITEM	WE IGHT	3.0	7.0	1.0	0.09	3.0	1.0	1.0	2.0	2.0	80.0	20.0	5.0	40.0	10.0	53.0	64.0	60.09	0.09	1.0	400.0	0.9	2.0	40.0	40.0	150.0	85.0	0.9	0.56	150.0	2.0	250.0	127.0	14.0	4.0	162.0	150.0	131.0	353.0	38.0	100.0	7.0	7.0	:07.0
ITEM	CUBE	27.0	75.0	0.	6.1	•5	-	••	.2	.7	6.3	2.0		3.3	• 5	4.2	11.0	7.7	7.7	0.	26.0	1.4	•5	2.0	7.7	15.0	6.4	3.6	3.9	14.0	1.3	15.0	2.7	2.1	a.e	8.2	7.0	0.6	25.0	4.3	2.8	• 5	5.	6.3
ITEM	SOUARE																																											
	X A Y	05000	05023	05020	C2070	C2100	C2150	C2230	C2250	C2310	C4 0 0 0	01043	02060	64940	06160	C4250	C4340	C4390	.04390	C44 36	C4450	C4670	C4680	06940	. C4190	C4820	C4H70	C4880	09640	C4930	0667	C2080	00150	C2110	C5200	C5320	C5400	C5410	C5430	C5870	02650	66140	06693	0.830

### CONSTRAINED THE FOR UNIT MAILS

# 8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

CURTATE TIE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE IS 7359-05 CU FT CONSTRAINED TO 75-0 PCT OR 5519-00 CU FT

SOUARE OF PUBLISHED T/F IS 11027.00 SO FT CONSTRAINED TO 75.0 PCT OR 8270.00 SO FT

SQUARE	CUBE	WEIGHT	SQUARE	CUBE	WEIGHT	OTY		OTY SOUARE	SOUARE	CUBE	Y DN DI
	0.5	140.0		93.9	2240-0	4	•	. 51		67.	•
	7.2	257.0		64.6	2313.0	. 0				64.6	
	18.0	330.0		144.0	2640.0	80	-	•		144.0	
	119.0	2148.0		238.0	4296.0	2	-	•0		27.0	2.
	1.0	12.0		3.0	36.0	n		3.		3.0	
	6.9	0.06		6.9	0.05	-	-	1.		6.9	
	20.0	30000		20.0	300.0	-	-	:		20.0	
	6.	18.0		2.8	54.0	n	-	3.		2.8	
	0.	0.1		•3	32.0	32	-	32.		.3	
	1.4	23.0		1.4	28.0	-	4	1.		1.4	
125.0		2650.0	125.0		2650.0	-	60		125.0		
38.0		1054.0	38.0		1054.0	-	4	:	32.9		
	20.0	163.0		20.0	163.0	-	4	1:		20.0	
	4.0	517.0		12.0	1551.0	Đ	4	3.		12.0	
	5.0	778.0		15.0	2334.0	3	4	3.		15.0	
119.0		5855.0	119.0		5855.0	-	*		6006		
	1.4	21.0		1.4	21.0	-	4	:		1.4	
	• •	16.0		c.	16.0	-	4	1.			
	9.	16.0		ç.	16.0	-	4	:			
		11.0		1.4	22.0	2	4	2.		1.4	
	125.0	1832.0		125.0	1832.0	-	4	:		125.0	
	35.8	210.0		35.8	710.0	-	4	1.		35.9	
	.3	8.0		.3	8.0	-	4	:		.3	
	•	1.0		0.	1.0	-	4	1:		0.	
	1.06	1890.0		4.06	1890.0	-	4			4000	
46.0		570.0	322.0		3990.0	7	60	٠,	221.0		:
0.96		2750.0	1152.0		33000.0	12	œ	10.	916.0		2.
44.0		0.019	44.0		610.0	-	8	1.	44.0		
93.0		2710.0	372.0		10840.0	4	8		325.6		
71.0		2780.0	71.0		2780.0	-	4	1.	51.4		
134.0		7370.0	938.0		51590.0	1	8	٠,	794.9		
200.0		19800.0	3502.0		336600.0	17	6	13.	2655.8		
185.0		14970.0	555.0		44910.0	n	4	-1	264.6		
61.0		2400.0	488.0		19200.0	80	æ	7.	413.5		:
239.0		34250.0	239.0		34250.0	-	4	• 0	94.4		
	••	5.0		· ·	2.0	-	-	:		0.	
	•3	15.0		£.	15.0	-	-	1.			
	39.0	7.0		546.0	98.0	7 7	-	7.		275.0	7.
	2.0	105.0		15.0	315.0	•	2	3.		15.0	
	1.0	10.0		6.9	6000	9	4	4		6.0	
	1.0	35.0		7.0	245.0		6	7.		.,	
	0.	0.1		0.	0.0	~		2.			
	0 00			,							

## 8-INCH HOWITZER BATTERY(SP), FORCE TROOPS

CURTATE TZE FUR CLASS VII. CLASS II TAM ITEMS

CUSE OF PUBLISHED TZE 15 7359-05 CU FT CONSTRAINED TO 75-0 PCT OP 5519-00 CU FT

SQUARE OF PUBLISHED TZE 15 11027.00 SQ FT CONSTRAINED TO 75.0 PCT OR 8270.00 SQ FT

	I TEM	I TEM	ITEM	1/6	17.6	1/E	1/E	CRIT	****	*********	T/E***	DFF:C-
TAM	SQUARE	CUBE	WEIGHT	SQUARE	CURE	WEIGHT	017		440	SOUADE	CUBE	1ENCY
50280		4.0	90.0		12.0	240.0	n	~	3.		12.0	
664	253.0		58500.0	1518.0		351000.0	c	8		1174.0		1.
264		0.0	0.0		0.0	0.0	10	4	10.			
980		3.0	0.68		17.8	534.9	c	4			17.0	
066		1.3	24.0		7.8	144.0	9		• •		7.8	
120		· .	12.0		2.9	72.0	9		• •		5.9	
130		28.0	530.0		158.0	3183.0	9	1	•9		158.0	
59:		8.0	150.0		24.0	450.0	2	£	3.		24.0	
200		6.6	0.09		37.9	240.0	4	8	4.		37.9	
540		0.	1.0		-	2.0	2	4	2.		-	
250		1.0	3.0		3.0	0.6	6	8	3.		3.0	
375	218.0		48448.0	218.0		48448.0	-	2	•0	11.3		•
1.30		10.0	0.46		0.01	94.0	-	80	:		10.0	
730		1.1	39.0		1.1	39.0	-	4	:		1.1	
060		124.0	1960.0		124.0	1960.0	-	4	:		124.0	
150		4.4	200.0		4.4	20000	-	4			4.4	
1 20		18.0	365.0		18.0	365.0	-	•	-		18.0	
	GRAND T	OTALS		11027.0	7359.0	7359.0 1239869.0	644		602.	8270.0	8270.0 5519.0	

TODAYS DATE 03/02/76

OR INDEX(SQUARE) = 81.82

OR INDEX(CUBE) = 97.92

OR INDEX(TOTAL 1/E) = 92.78

. CONSTRAINED TZE FOR UNIT MIGGA
HEADGUARTERS BATTALION. MARINE DIVISION

CURE OF PUBLISHED T/F IS 21615.34 CU FT CONSTRAINED TG 90.0 PCT OR 19455.00 CU FT SQUARE OF PUBLISHED T/F IS 21537.00 SO FT CONSTRAINED TU 90.0 PCT OR 19383.00 SO FT

	ITEM	ITEN	N EL T	1/E	1/E	1/E	1/5	CRIT	* * * *	1/5	PEFIC-
MA 1	SGUARE	CUBE	WEIGHT	SQUARE	CUBE	WEIGHT	4		710	SOUADE CURE	LENCY
AOUDS		5.0	159.0		15.0	477.0	n	60	3.	14.0	
0600V		3.0	47.0		36.0	564.0	12	œ	12.	36.0	
40130		1.0	3.0		2.0	0.9	2	4	2.	2.0	
40200	162.0		0.0019	162.0		8100.0	-	80	.1.	162.0	
80500		0.0	0.0		0.0	0.0	8	. 60	2.	0.0	
A5270	41.0		1975.0	205.0		9875.0	S	œ	5.	205.0	
A9320		1.0	20.0		25.0	500.0	25	8	25.	25.0	
43.328		1.0	0.6		10.0	0.06	10	60	10.	10.01	
A0440		1.0	12.0		10.0	120.0	01	8	10.	10.01	
A0650		1.0	42.0		2.0	84.0	8	4	2.	5.0	
40685		0.0	0.0		0.0	0.0	-	•		0.0	
012CV		0.1	42.0		1.0	42.0	-	4	1.	1.0	
05.40V		3.0	0.96		6.9	192.0	~	4	2.	6.0	
40800		2.0	0.46		5.0	0.46	-	•		S. C.	
A3810		0.4	115.0		8.0	230.0	~	. 3	2.	8.0	
40870		7.0	182.0		21.0	546.0	<b>E</b>	8	3.	21.0	
21004		1.0	42.0		1.0	42.0	-	4	-:	1.0	
A1180		1.0	26.0		3.0	78.0	6	4	3.	0.5	
A1190		4.0	104.0		8.0	204.0	2	*	2.	0.9	
A1250		1.0	10.0		4.0	0.04	4	4	. 4	0.0	
A1299		36.0	1122.0		72.0	2244.0	8	60	2.	72.0	•
A1 100		7.0	523.0		14.7	1046.0	8	6	2.	14.0	
A1420		11.0	93.0		22.0	186.0	2	8	2.	22.0	
A1570		1.0	45.0		1.0	45.0	-	8	1:	1.0	
A1630		1.0	33.0		2.0	66.0	~	60		2.0	
A1730		1.0	22.0		25.0	550.0	25	60	25.	25.0	
A1800		1.0	26.0		14.0	784.0	1.4	8	14.	14.0	
A1990		1242.0	0.0500		3726.0	29850.0	3	σ	3.	3726.0	
A1900	70.0		4190.0	1050.0		62850.0	15	8	14.	1005.8	:
A:920	61.0		2535.0	365.0		15210.0	c	œ	• 9	356.0	
A1930	0.09		2670.0	360.0		16020.0	9	60	. 4	360.0	NOTE:
A1940		350.0	2575.0		5250.0	38625.0	15	0	15.	5250.0	
A1950		0.0-	0.0		0.0	0.0	2	00	2.	0.0	Unit
A2010		8.0	101.0		64.0	808.0	œ	80	ď	0.46	
A2020		8.0	139.0		128.0	2224.0	14	•	16.	128.0	Const
42040		1.0	2.3.0		8.0	184.0	œ	80	ά	0.4	
A2050		1.0	20.0		44.0	0.088	44	6	44.	0.44	
A2182	0.09		3370.0	240.0		13480.0	4	8		240.0	
A2183	0.09		2751.0	1560.0		71786.0	56	σ	24.	1426.5	
42134		5.0	88.0		16.0	440.0	α	6	3.	14.0	
02228		0.7	42.0		19.0	7.38.0	C	8	•	18.0	
01264		2.0	0.45		36.0	694.0	13	5	14.	35.0	
42110	68.0		3.000.0	264.0		6.0000	-	c		264.0	

= M1988 traint = 90%

### CONSTRAINED TIE FOR UNIT MISSS

HEADQUARTERS BATTALION. MARINE DIVISION

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS CURE OF OUBLISHED TZE IS 21615.34 CU FT CLASTRALMED ID 30.0 PCT OR 19455.30 CU FT

CONSTRAINED TO 90.0 PCT OR 19383.00 SO FT

15 404																																	. 4	5	0								
TVETTE				14.0	30.0	106.0	40.0	28.0	2.0	4.0	10.0	0.0	10.0	1.0	12.0	3.0			0.0		41.2	20.0		32.0	30.0	31.0	0.0	10.0	74.0	2.3	4.2	6.9	6.0	14.4	4.81	21.0	0	14.8	4	0.4			20.70
OTY SOUARE	175.0	44.0	80.0														10.0	15.4		54.0																					-		
917	2.	•	:	14.	3.		.8	28.	2.	:	:	2.	:	:	,	3.	2.	.8	*	1.	.9	:	:		4.	:	:	:	:	• •	:	:	31.	30.	62.	20.	. 4	. 6	2.	70.	6.	1.2	
CRIT	•	4	4	8			8	8	4	0	4	•	*	4	8	•	•	•	-	2	2	8	4	4	80	80	80	4	8	8	4	2	-	-	-	-			1	-	1		
1/F 017	~	-	-	14	3	2	8	53	2	*	-	~	-	-	c	3	2	8	•	-	9		-	4	4	-	-	-	-	9	-	-	35	35	20	35	4	00	r.	70	ç	10	12.
T/E WEIGHT	6200.0	4750.0	4750.0	392.0	785.0	290.0	720.0	280.0	40.0	100.0	115.0	0.0	42.0	15.0	126.0	45.0	400.0	2120.0	0.0	2641.0	780.0	312.0	225.0	1020.0	552.0	407.0	0.0	220.0	4471.0	24.0	140.0	100.0	140.0	210.0	210.0	245.0	4.0	480.0	15.0	20.0	6.0	20.07	70.07
CUSE				14.0	30.0	106.0	40.0	28.0	2.0	4.0	10.0	0.0	10.0	1.0	12.0	3.0			0.0		41.2	29.0	3.1	32.0	30.0	31.0	0.0	10.0	74.0	2.3	4.2	6.5	10.8	16.3	18.0	26.3	.0.	14.9	m.	4.3			****
SOUARE	176.0	88.0	80.0														10.0	16.0		54.0																							
WEIGHT	3100.0	4750.0	4750.0	24.0	252.0	145.0	0.00	10.0	20.0	25.0	115.0	0.0	42.0	15.0	21.0	15.0	200.0	255.0	0.0	2641.0	130.0	312.0	225.0	255.0	138.0	407.0	0.0	220.0	4471.0	0.6	140.0	100.0	4.0	9.0	3.0	.7.0	1.0	0.09	3.0	1.0	1.0	2.0	0.0
CUBE				1.0	10.0	53.0	5.0	1.0	1.0	1.0	10.0	0.0	10.0	1.0	2.0	1.0			0.0		6.9	29.0	8.1	8.0	7.5	31.0	0.0	10.0	74.0		4.2	6.5	.3	• 5	7.	.8	0.	1.9	.2		0.		.,
SQUARE	0.4E	98.0	80.0		,												2.0	2.0		54.0																							
	42320	A2340	A2350	12480	42500	42510	62454	42635	00154	42710	A2923	A3012	41060	A3065	A3238	13290	10000	H0003	80011	40455	30470	90430	60508	91350	31430	81440	81445	91620	81755	H2090	82220	92390	01023	C2030	C2040	22050	C2060	62020	C2100	62163	62230	05023	62310

HEADOUARTERS BATTALION, MARINE DIVISION CURTATE TZF FRA CLASS VII. CLASS II TAM ITEMS

CUSE OF PUCLISHED TZE IS 21615-34 CU FT CONSTRAINED TO 20.0 PCT OR 19455-00 CU FT

SQUARE OF PUBLISHED TZE IS 21537.00 SQ FT CONSTRAINED TO 40.0 PCT OR 19383.00 SQ FT

	ITEN	ITEM	TTEM	1/E	1/5	TVF	TIF	CRIT	****	*PEDUCED TA	T/Ess*	DEFIC-
144	SOUARE	CUBE	WE 1GHT	SOUARE	CUBE	WEIGHT	410				CUBE	TFNCY
03063		1.0	16.0		486.1	7856.0	164	-	403.		1.066	20.
64000		6.3	80.0		100.9	1290.0	16	-	15.		100.8	
54010		2.0	50.0		26.0	650.0	13	-	13.		25.0	
21013		1.3	27.0		1.3	27.0	-	1	:		1.3	
64020		:	5.0		9.	40.0	6	-			•	
C4040		3.3	0.04		68.5	840.0	21	-	21.		68.5	
C4140		.5	10.0		3.4	70.0	1	-	7.		3.4	
54230		4.	45.0		3.4	225.0	r	-	2.		4.5	
C4250		4.2	53.0		21.0	265.0	5	-	5.		21.0	
C4340		11.0	64.0		44.0	256.0	4	-	•		44.0	
001 00		7.7	20.0		15.3	120.0	~	-	2.		15.3	
C4436		•	1.0		6.4	638.0	638	-	638.		4.4	
04940		72.0	918.0		72.0	914.0	-	œ	:1		72.0	
54650		3.0	85.0		18.0	510.0	ç	-	• •		18.0	
C0 460		12.0	204.0		0.09	1020.0	S	-	2.		6.09	
C4670		1.4	0.9		2.8	12.0	2	-	2.		2.8	
64480		• 5	2.0		•5	0.9	n	-	3.		.5	
06443		2.0	40.0		2005	1040.0	56	-	23.		44.7	*
06240		7.7	40.0		192.2	1000.0	25	-	20.		156.1	.5
C4820		15.0	150.0		270.0	2700.0	18	-	18.		266.7	
C4830		1.	50.0		.8	750.0	13	-	15.		۵.	
64870		6.4	95.0		101.9	1350.0	91	-	16.		101.0	
CARRO		3.6	8.0		213.5	480.0	69	-	45.		140.4	15.
C4 930		14.0	150.0		476.0	5100.0	34	-	23.		315.7	::
02050		4.2	74.0		8.4	149.0	2	-	2.		4.5	
08050		15.0	250.0		30.0	20000	~	-	2.		30.0	
06053		0.4	196.0		15.1	588.0	3	-	3.		12.1	
C5110		2.7	14.0		93.1	440.0	35	-	27.		71.6	ď
C5200		3.8	0.4		564.6	280.0	10	-	52.		197.9	13.
00250		:	1.0		2.2	44.0	44	-	44.		2.2	
C5310		0.99	1012.0		0.99	1012.0	-		:		0. 39	
CS 120		8.2	162.0		100.0	14094.0	87	-	.19		496.9	56.
C5330		9.9	86.0		9.9	96.0	-	-	:		4.6	
C5340		9.6	0.56		42.7	475.0	r	-			45.7	
C5370		145.0	2375.0		1740.0	28500.0	12	-	10.		1495.0	2.
C5 180		101.0	1306.0		101.0	1305.0	-		:		101.0	
06233		46.7	756.0		46.7	156.0	-	-	:		46.7	
69469		7.0	150.0		577.7	12450.0	83	-	59.		410.2	24.
01950		0.6	131.0		0.00	1310.0	10	-	10.		0.00	
55420		25.0	353.0		725.0	10237.0	50	-	14.		440.4	-:-
C-1.P.30		6.	10.0		21.4	5.0.0	24	-	54.		21.4	
CS 376		4.3	33.0		34.2	304.0	8	-	·		30.01	
01053		15.3	1 100.0		33.0	0.0022	0	-	•		20.00	

STANFORD RESEARCH INST MENLO PARK CALIF NAVAL WARFAR--ETC F/G 15/5
MATERIEL WEIGHT AND CUBE CONTROL (1975-1980).(U)
MAR 76 T H ALLEN, R B RINGO N00014-75-C-0708 AD-A041 598 NL UNCLASSIFIED 5 OF 7 ADAO41598

# HEADQUARTERS BATTALION, MARINE DIVISION CURTATE TVE FOR CLASS VII. CLASS II TAM TTEMS

CONSTRAINED TO 90.0 PCT DR 19455.00 CU FT CONSTRAINED TO 90.0 PCT DR 19455.00 CU FT SQUARE OF PUBLISHED TZE IS 21537.00 SO FT CONSTRAINED TO 90.0 PCT OR 19383.00 SO FT

TAN

	F IFNCY	·			c				3	0	0	. v .			.2 15.	0	2		0	4	.3 7.		3	8		0	0			.5	2		0	0	4		0.	8		3.			2.	
1/E**	CURE	99.06	124.8	4.1	4.0	-	1:1	4.0	5.5	64.0	126.0	130.2	50.7	320.3	400.5	238.0	34.2	27.5	100.0	47.4	31.3	2.0	3.3	2.8		0.04	16.0		2.7	•	1.2	1.4	250.0	87.0	107.4	£.	•	362.8	4	2	•	,		
***** TE****	SOUARE																								74.0			119.0											2355.6	2359.2	433.9	71.0		
****	017	3.	45.	3.	:	:	• 9	:	11.	٠.	• 9	21.	10.	45.	29.	2.	23.	. 4	2.	15.	33.	2.	327.	2.	2.		•	:		:	5.	5.		3.	3.	:	:		51.	25.	·	:		• 0
CRIT		-	-	-	-	1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2	4	2	-	2	2	2	2	2	63	2	2	2	٥.	2	4	4	4	2		**
1/5	014	0	65	3	-	-	9	-	=	9	9	52	01	63	4.3	2	23	4	~	15	40	~	327	2	2	2	4	-	2	-	2	2	2	m	n	-	-	*	57	28	ď	1		7
17.6	WE TGHT	8280.0	290000	93.0	134.0	3.0	45.0	138.0	77.0	30.0	1380.0	2675.0	1400.0	14191.0	14190.0	4296.0	1426.0	360.0	60000	450.0	720.0	20.0	327.0	56.0	2103.0	326.0	2068.0	5955.0	45.0	16.0	32.0	22.0	3654.0	1980.0	2130.0	8.0	1.0	7560.0	32400.0	77000.0	13551.0	2730.0		0.00445
TVE	CUBE	0.66	162.8	4.3	4.0	-	1.1	4.0	5.5	66.0	126.0	157.5	58.7	452.3	774.0	238.0	34.5	27.5	100.0	47.4	38.0	2.0	3.3	2.8		40.0	16.0		2.1	r.	1.2	1.4	250.0	67.0	107.4	•3	c.	362.9						
17.5	SOUARE																								16.0			119.0											2622.0	2688.0	465.0	71.0		0.5091
ITEM	WEIGHT	920.0	100.0	31.0	134.0	3.0	7.0	138.0	7.0	5.0	230.0	107.0	140.0	257.0	330.0	2148.0	62.0	0.06	300.0	30.0	18.0	25.0	1.0	28.0	1054.0	163.0	517.0	5855.0	21.0	16.0	15.0	11.0	1932.0	660.0	710.0	8.0	0.1	1890.0	570.0	2750.0	0.0:75	2780.0		0.01:1
ITEM	CUBE	11.0	2.8	1.5	4.0	•	.2	4.0	\$.	11.0	21.0	6.3	5.9	7.2	18.0	119.0	1.5	6.9	20.0	3.2	6.	1.0	0.	1.4		20.0	4.0		1.4	• 5	9.		125.0	29.0	35.8	•3	0.	1.00						
ITEM	SQUARE																								38.0			119.0											0.90	0.96	03.0	71.0		

C5923 C5930 C5930 C5930 C6140 C6140 C65370 C

## HEADQUARTERS BATTALION. MARINE DIVISION

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE 1S 21616.34 CU FT CONSTRAINED TO 90.0 PCT 09 19455.00 CU FT

SQUARE OF PUBLISHED TZE IS 21537.00 SO FT CONSTRAINED TO 90.0 PCT OR 19383.00 SO FT

DEF IC-		7.				.9											
CUBE				-	218.4	631.6	:	35.7	20.7	7.8	0.0	0.0	0.	:	1.0	2.0	2.3
*****REDUCED 1	747.3	3598.9	239.0														
017	ř	.65	:	. 4	18.	16.	.1.	. 4	7.	.9	•		:	2.	,	2.	
CR 11	•	4	2	-			-	2	8	4	8	2	4	~	2	60	~
1/E 01Y		99	-	4	27	22	=	4	1	·	60	2	-	2	9	8	8
17.E WE1GHT	68880.0	158400.0	34250.0	8.0	91.0	154.0	11.0	432.0	623.0	144.0	0.0	0.0	0.1	0.4	43.0	10.0	78.0
TZE				-	324.0	858.0	:	35.7	20.1	7.8	0.0	0.0	c.	-	1.9	2.0	2.1
SOUARE	768.0	4025.0	239.0														
ITEN WEIGHT	22960.0	2400.0	34250.0	2.0	3.0	7.0	1.0	108.0	89.0	24.0	0.0	0.0	1.0	2.0	8.0	2.0	34.0
I TEM CUBE				•	12.0	29.0	0.	8.9	3.0	1.3	0.0	0.0	0.	0.	.3	1.0	:
SQUARE	256.0	61.0	239.0														
TAM	09010	09110	01210	01250	E0090	E0000	E02:0	50 520	60980	FC330	E1155	51156	51240	C1403	E1760	61900	£2030

IODAYS DATE 03/03/76
OR INDEX(SQUARE) = 91.84
OR INDEX(CUBE) = 94.55
OR INDEX(IOTAL I/E) = 94.03

3283. 19383.019455.0

21537.0 21616.3 1316053.0 3625

GRAND TOTALS

HEADQUARTERS BATTALTON, MAYING DIVISION CONTATE TX: FOR CLASS VII. CLASS II TAM ITEMS

CONE OF PUBLISHED TZE IS 21616-34 CU FT CONSTRAINED TO NB-0 PCT OR 18374-00 CU FT

SQUARE OF PUHLISHED TZE 15 21537.00 50 FT CONSTRAINED TO 85.0 PCT OR 18306.00 SO FT

																																			886	4 - 85%	1							
- 1.1.1.	×1201																													:			NOTE:		Unit = M1988	Constraint	Collectain							
1/5***	2000	·	0.75			0.0		25.0	10.0	10.0	5.0	0.0	1.0	6.0	0.6	0.4	21.0	1.0	3.0	8.0	0.4	72.0	14.0	22.0	1.0	2.0	25.0	14.0	3726.0				5250.0	0.0	61.0	128.0	8.0	44.0			16.0	0.41	36.0	
******					162.0		205.0																							993.7	366.0	340.0							240.0	1359.7				564.3
****	710	3.	12.		:		• 10	25.	10.	10.	5.	1:	:	2.	:	2.	3.		3.	2.	4.	2.	2.	2.	:	2.	25.	14.	3.	14.	. 9	٠,	15.	٠,	ď	16.	9.	***	4.	23.	я.	ċ	1 %	
CRIT		α	8	4	œ	co	a:	œ	œ	80	4	4	4	•	4	8	œ	*	٩	4	4	60	80	8	8	60	00	60	8	8	8	8	80	8	8	60	T	8	8	8	60	80	8	a.
1/F	410	3	12	N	-	٥.	ທ	25	10	10	~	-	-	2	-	2	2	-	3	2	4	2	2	2	-	~	25	14		15	9	0	15	2	T	16	ď	44	*	26	r	6		~
1/5	WE IGHT	477.0	564.0	0.9	8100.0	0.0	9875.0	200.0	0.06	120.0	84.0	0.0	42.0	192.0	0.46	230.0	546.0	45.0	78.0	208.0	40.0	2244.0	1046.0	186.0	45.0	66.0	550.0	784.0	29850.0	62850.0	15210.0	16020.0	39625.0	0.0	808.0	2224.0	184.0	880.0	13480.0	71785.0	440.0	7.4.0	6.44.0	0.000
1/1	CUBE	15.0	36.0	2.0		0.0		25.0	10.0	10.0	2.0	0.0	1.0	0.9	5.0	8.0	21.0	1.0	3.0	0.8	4.0	72.0	14.0	22.0	1.0	2.0	25.0	14.0	3726.0				5250.0	0.0	64.0	128.0	8.0	44.0			14.0	14.0	36.0	
1/5	SQUARE				162.0		205.0																							1050.0	365.0	360.0							240.0	1560.0				345.09
7 1 2	WEIGHT	159.0	47.0	3.0	8100.0	0.0	1975.0	20.0	0.6	12.0	45.0	0.0	45.0	0.96	0.46	115.0	182.0	45.0	26.0	104.0	10.0	1122.0	523.0	93.0	45.0	33.0	22.0	26.0	0.0566	4190.0	2535.0	2670.0	2575.0	0.0	101.0	139.0	23.0	20.0	1370.0	2761.0	55.0	42.0	30.0	3.001.0
N.H.I	CUBE	5.0	3.0	1.0		0.0		1.0	1.0	1.0	1.0	0.0	1.0	3.0	2.0	4.0	7.0	1.0	1.0	4.0	1.0	36.0	7.0	11.0	1.0	1.0	1.0	1.0	1242.0				350.0	0.0-	8.0	8.0	0.1	1.0			2.0	2.0	2.0	
7 1 1	SCJARE				162.0		41.0																							20.0	61.0	0.09							60.09	0.09				38.0
	1 44	43205	40000	A71 10	A02+0	40265	075CA	A3 520	A0 324	43430	90000	A3685	40710	A0730	0086V	A3810	A0870	A0012	AIIRO	A1190	A1250	A1290	A1.500	A1420	A1570	A1630	A1730	A1800	A1890	A1900	41920	A1 430	A1940	A1950	A2010	A202A	A2040	42030	32182	A2193	A2144	A2220	A2270	A2 210

### CONSTRAINED TIE FOR UNIT MISSR

HEADQUARTERS BATTALION. MARINE DIVISION

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS
CURE OF PUBLISHED TZE IS 216,16.34 CU FT
CONSTRAINED TO 85.0 PCT OR 18374.00 CU FT

SQUARE OF PUBLISHED TZE IS 21537.00 SO FT CONSTRAINED TO 85.0 PCT OR 18326.00 SO FT

DEFIC-	1F NCY																																	• •	7.	11.	.0				7.		۶.	
1/5***	CURE				14.0	30.0	104.0	40.0	28.0	2.0	4.0	10.0	0.0	10.0	1.0	12.0	3.0			0.0		41.2	29.0	8.1	32.0	30.0	31.0	0.0	10.0	74.0	2.3	4.2	5.5	0.0	13.6	15.8	20.6	0.	14.8	٠.	4.4	:	4.5	4.
*REDUCED T	SOJAPE	176.0	648	80.0														10.0	15.1		54.0																							
****	710	2.	:	:-	14.	3.	2.	· α	28.	2.	•	:	2.	:		• 9	3.		· α	٨.	:		1.	:	. 4	*	:-	:	:	1:	• •	:1	:	29.	28.	.65	27.	*	ъ.	۶.	63.		30.	29.
CRIT		4	4	4	60	60	4	80	60	4	4	4	2	4	4	æ	4	4	4	-	2	2	æ	•	4	8	89	60	4	œ	80	4	~	-	-	-	-	-	-	-	-	-	-	-
1/E	¥10	8	-	-	4	3	2	60	28	8	4	-	2	-	-	9	3	2	œ	4	-	٠	-	-	4	4	-	-	-	-	¢	-	-	35	35	20	35	4	8	S	20	¢	35	35
1/5	WE IGHT	6200.0	4750.0	4750.0	392.0	786.0	290.0	720.0	280.0	40.0	100.0	115.0	0.0	42.0	15.0	126.0	45.0	400.0	2120.0	0.0	2641.0	780.0	312.0	225.0	1020.0	552.0	407.0	0.0	220.0	4471.0	54.0	140.0	100.0	140.0	210.0	210.0	245.0	4.0	4.0.0	15.0	70.0	6.9	20.0	10.0
TVE	CUBE				14.0	30.0	106.0	40.0	28.0	2.0	4.0	10.0	0.0	10.0	1.0	12.0	3.0			0.0		41.2	29.0	9.1	32.0	30.0	31.0	0.0	10.0	74.0	2.3	4.2	6.5	6.01	16.3	18.9	26.3	0.	14.8	æ.	6.4	••	5.3	28.4
TVE	SOUARE	176.0	88.0	80.0														10.0	16.0		54.0																							
1 TEM	WEIGHT	3100.0	4750.0	4750.0	23.0	252.0	145.0	0.06	10.0	20.0	25.0	115.0	0.0	42.0	15.0	21.0	15.0	200.0	265.0	0.0	2641.0	130.0	312.0	225.0	255.0	138.0	407.0	0.0	220.0	4471.0	0.6	140.0	100.0	4.0	0.9	3.0	7.0	0.1	0.09	3.0	1.0	1.0	2.0	2.0
ITEM	CUBE				1.0	10.0	53.0	5.0	1.0	0.1	1.0	10.0	0.0	10.0	1.0	2.0	0.1			0.0		6.9	29.0	8.1	8.0	7.5	31.0	0.0	10.0	74.0	•	4.2	6.5	£.	• 5	.3	. 3	0.	1.9	.2	-	0.		
I TEN	SOUAHE	98.0	88.0	90.0														2.0	2.0		54.0																							
	TAM	A2.320	A2.340	A2350	42430	A2500	A2510	A2660	A2535	A2700	427:0	42920	A3012	A3060	A3055	A3238	A3280	10008	B0003	11006	30465	80470	00400	90509	31 360	91430	81440	91445	81620	81755	95030	82220	82390	C2010	52030	62040	C2050	C2060	C2070	C2100	C2160	C2230	C2220	C2310

HEADQUARTERS BATTALION. MARINE DIVISION

CUSTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUME OF PUMLISHED TZE 15 21616.34 CU FT CUNSTRAINED TO 95.0 PCT OR 18374.00 CU FT

SQUARE OF PUBLISHED TZE IS 21537.00 SO FT CONSTRAINED TO 85.0 PCT OR 18306.00 SO FT

OFF IC.	11 NCY	113.																		7.	2.			.01	14.				10.	22.			33.			5.			30.		14.	:		
1/54044	CURE	373.8	100.6	26.0	1.3	٠.	64.8	3.4	3.4	21.0	44.0	15.3	4.4	72.0	18.0	60.09	2.8	• 5	41.7	141.5	240.0	c.	101.0	146.6	276.6	4.4	30.0	15.1	65.7	180.5	2.2	66.0	443.R	4.4	42.7	0.180	101.0	46.7	368.3	30.00	332.6	20.4	34.2	30.0
* DEDITORD																																												
****	710	378.	16.	13.		8.	20.	7.	5.	5.	4	2.	638.	-	•	ď	2.	3.	21.	18.	16.	15.	16.	41.	20.	2.	2.	3.	25.	48.	44.	-1	54.	:		7.	-	:	53.	10.	15.	23.		2.
CPIT		-	-	-	-	-	-	-	-	-	-	-	-	80	-	1	-	-	-	-	-	-	-	-	-	1	-	1	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-
1/5	017	164	16	13	-	80	12	1	5	2	4	2	638	-	9	S	2	3	56	52	18	15	16	09	34	2	~	n	35	7.0	44	-	87	-	5	12	-	-	83	10	66	24	6	2
1/5	WE LGHT	7856.0	1280.0	650.0	27.0	40.0	840.0	70.0	225.0	265.0	255.0	120.0	639.0	914.0	510.0	1020.0	12.0	6.5	1040.0	100000	2700.0	750.0	1360.0	480.0	5100.0	148.0	20000	583.0	430.0	280.0	44.0	1012.0	14004.0	86.0	475.0	28500.0	1306.0	756.0	12450.0	1310.0	19237.0	240.0	304.0	0.0225
1/5	CUBE	486.1	100.8	26.0	1.3	4.	68.5	3.4	3.4	21.0	44.0	15.3	6.4	72.0	18.0	0.09	2.8	• 5	50.7	192.2	270.0	8.	101.9	213.6	476.0	8.4	30.0	12.1	93.1	264.6	2.2	0.99	40602	9.9	42.7	1740.0	101.0	45.7	517.7	30.0	725.0	21.5	34.2	30.0
1/5	SQUARE																																											
ITEM	WEIGHT	16.0	80.0	20.0	27.0	2.0	40.0	10.0	45.0	53.0	64.0	0.09	1.0	918.0	85.0	204.0	0.9	2.0	40.0	40.0	150.0	20.0	85.0	8.0	150.0	74.0	250.0	196.0	14.0	0.4	1.0	1012.0	162.0	86.0	0.56	2375.0	1306.0	756.0	150.0	131.0	353.0	10.0	3.1.0	1365.0
ITEM	CUBE	1.0	6.3	2.0	1.3	-:	3.3	• 5	2.	4.2	0.11	7.7	0.	72.0	3.0	12.0	1.4	.2	2.0	7.7	15.0		6.4	3.6	14.0	4.2	15.0	4.0	2.7	3.8	:	0.99	8.2	9.9	8.6	145.0	101.0	46.7	7.0	0.6	25.0	6.	4.3	15.0
LTEM	SOUARE																																											
	TAN	C3020	C4000	C4010	C4015	04020	C4040	C4140	C4230	C4250	C4 340	C4330	C4436	C4640	05943	C4660	01000	C4680	06940	C4 7:30	C4 920	C4830	C4870	CARHO	C4 380	02050	CS080	06050	C5110	C5200	C5300	C5310	C\$320	C5330	C5340	C5.370	C5.380	C5.190	C5400	C5410	CSF20	C5 430	CSHTO	01693

## HEADQUARTERS BATTALION. MARINE DIVISION

CURTATE TZE FUR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE IS 21616.34 CU FT CONSTRAINED TO 85.0 PCT OR 18374.00 CU FT

SQUARE OF PUBLISHED TZE IS 21537.00 SO FT CONSTRAINED TO 85.0 PCT OR 18306.00 SO FT

DEFIC-	I E NC Y		17.									٠,		23.	10.						•																		•	•	:		ŕ	
T/E***	CUBE	0.00	114.6	4.3	4.0	:	1:1	4.0	6.5	66.0	126.0	118.8	58.7	287.3	432.5	238.0	32.4	27.5	100.0	47.4	29.3	2.0	3.3	2.8		40.0	16.0		2.7	6.	1.2	1.4	250.0	A7.0	107.4	r.	0.	362.8						
CHORCHARA	SQUARE																								76.0			119.0											2239.9	2194.8	419.2	21.0	1104.4	3314.0
****	0TY	•	42.	3.	1.	1.	• •	:	.11	• 9	• 9	10.	10.	*0*	24.	2.	22.	•	2.	15.	31.		327.	2.	2.	5.	4	:	2.	:	2.	2.	2.	3.	3.	:	:	. 4	40.	23.	4	:	ċ	
CRIT		-	-	-	-	. 1	-	-	1	-	-	-	-	-	-	1	-	-	-	-	-	-	-	2	4	2	-	2	2	2	2	2	2	2	2	2	2	2	4	4	•	2	•	*
1/5	710	0	63	9	-	-	9	-	1.1	c	9	52	10	63	43	2	53	4	2	15	40	2	327	2	2	2	4	-	2	-	2	2	2	m	n	-	-	4	21	28	5	-	12	24
1/5	WEIGHT	8280.0	290000	93.0	134.0	3.0	45.0	138.0	77.0	30.0	1380.0	2675.0	1400.0	16191.0	14190.0	4296.0	1426.0	360.0	60000	450.0	720.0	20.0	327.0	56.0	2108.0	326.0	2068.0	5855.0	45.0	16.0	32.0	22.0	3664.0	1980.0	2130.0	8.0	1.0	7560.0	32490.0	77000.0	13550.0	2789.0	84440.0	327770.0
1/E	CUBE	0.66	162.9	4.3	4.0	:	::	4.0	5.5	66.0	126.0	157.5	58.7	452.3	774.0	238.0	34.5	27.5	100.0	47.4	38.0	2.0	3•3	2.8		40.0	16.0		2.7	• 5	1.2	1.4	250.0	87.0	107.4	•3	0.	362.8						
1/5	SQUARE																								16.0			119.0											2622.0	2688.0	465.0	71.0	1608.0	4254.0
ITEM	WEIGHT	950.0	100.0	31.0	134.0	3.0	7.0	138.0	7.0	2.0	230.0	107.0	140.0	257.0	330.0	2148.0	62.0	0.06	30000	30.0	18.0	25.0	1.0	28.0	1054.0	163.0	517.0	5855.0	21.0	16.0	16.0	11.0	1832.0	0.099	710.0	8.0	1.0	1890.0	570.0	2750.0	2710.0	2780.0	7370.0	13000-0
LTEN	CUBE	11.0	2.8	1.5	0.4	:	• 5	4.0	• 5	11.0	21.0	6.3	5.9	7.2	18.0	119.0	1.5	6.9	20.05	3.2	6.	1.0	0.	1.4		50.0	4.0		1.4	••	9.	.7	125.0	29.0	35.8	•3	0.	2.06						
KELI	SOUARE																								38.0			119.0											46.0	0.96	93.0	71.0	134.0	176.0
	TAM	C5920	C5+30	06650	C4000	C\$030	C6140	56150	66220	09293	66350	C6370	C6388	C6.390	66410	C6420	C6490	01500	C6550	C5550	C6670	C6680	C6684	02000	06000	00100	02100	06100	06800	00400	01400	00450	00725	00730	50740	00750	59700	00220	00800	09860	00000	06800	01020	01010

### HEADQUARTERS BATTALION, WARINF DIVISION

CUSTATE TZF FUR CLASS VIII. CLASS II TAM ITFMS

CORE OF PURE ISHED TZE IS 21646.34 CO FT CONSTRAINED TO 84.0 PCT OR 183.44.00 CU FT

SQUARE OF PUBLISHED TZE IS 215.37.00 SO FT CONSTRAINED TO 85.0 PCT OR 19306.00 SO FT

JE NOV		.11.				c.												
CURE CORE				-	192.5	532.3	:	35.7	20.7	7.8	0.0	0.0	· ·	:	1.0	2.0	2.3	0.97591
*****REDUCED 1/E**** DIY SCUANE CURE	737.9	3385.4	233.0															18306-018374-0
, v t c	3.	.55.	:	. 4	16.	14.		4.	7.	• 5	e.	٠,	:-	۶.	٠,	2.	٠.	3165.
CP11	4	4	~	-	. 1	-	-	2	2	4	2	2	4	2	2	œ	2	
17.E 017	2	99	-	*	27	22	11	4	1	٠	Œ	2	-	~	•	2	~	3625
. TZE	63880.0	158400.0	34250.0	9.0	81.0	154.0	11.0	432.0	623.0	144.0	0.0	0.0	1.0	0.0	48.0	10.0	78.0	21616.3 1316058.0 3625
T/E CUBE				-	324.0	859.0	-	35.7	20.7	7.8	0.0	0.0	0.	-	1.0	2.0	2.3	21616.3
SOUANE	768.0	4026.0	239.0															21537.0
1TEN WEIGHT	22950.0	2400.0	34250.0	2.0	3.0	7.0	1.0	108.0	89.0	24.0	0.0	0.0	1.0	2.0	8.0	2.0	39.0	
LTEM				0.	12.0	39.0	••	8.9	3.0	1.3	0.0	0.0	••	••	•3	1.0	1.1	OTALS
SZUAZE	256.0	0:10	239.0															GRAND TO
24 2	01000	01:00	01210	01250	60090	ECODS	50210	E0.520	50480	00000	51155	51156	E1240	E1403	E1750	E1900	E2030	

TODAYS DATE 03/02/76
OR INDEX(SQUAPE) = 87.76
OR INDEX(CUBE) = 92.73
OR INDEX(TOTAL 7/E) = 91.78

READQUARTERS HATTALION, MARINE DIVISION CLASS II FAM ITEMS

CONSTRAINED TO 75.0 PCT OR 16212.00 CU FT

SQUARE OF PURISHED TZE 15 21537.00 SO FT CUNSTRAINED TO 75.0 PCT OR 16153.00 SO FT

0=r.1C-	TENCY																												•	.2		NOTE:		Init = M1988		Constraint = 75%								
T/E***	SQUADE CUBE	15.0	3.11	¢ • 4	152.0	0.0	205.0	25.0	10.0	10.0	2.0	0.0	1.0	6.0	3.6	R.O.	21.0	1.0	3.0	0.3	4.0	72.0	14.0	22.0	1.0	5.0	25.0	0.4:	2640.8	938.3	365.4	359.6	5250.0	0.0	64.0	128.0	c. a	0.44	240.0	1292.1	16.0	0.61	36.0	254.0
****	710	<b>m</b>	12.	2.	••	2.	5.	25.	10.	10.	2.	:	:1	2.		5.	3.	:	3.		4.		2.	2.	:		25.	14.	5.	13.	• 9	•	15.	٠.	•	14.	8	. 44	4	22.	•	ċ	13.	•
CRIT		8	9	4	8	. 80	80	60	æ	80	4	•	4	•	4	8	œ	4	4	4	4	60	60	60	œ	60	80	80	œ	80	80	60	en on	60	8	8	89	8	8	80	8	6	8	ε.
1/E	710	r	12	2	-	2	S	52	10	10	٨	-	-	2	-	8	9	-	r	2	4	2	8	2	-	~	25	4	n	15	c	•	15	~	00	15	œ	44	•	52	0	c	13	~
1/E	WEIGHT	477.0	564.0	0.9	8100.0	0.0	9875.0	20000	0.06	120.0	34.0	0.0	45.0	192.0	0.00	230.0	246.0	42.0	78.0	208.0	40.0	2244.0	1046.0	186.0	45.0	0.59	250.0	784.0	29850.0	52850.0	15210.0	16020.0	38625.0	0.0	808.0	2224.0	134.0	880.0	13480.0	71786.0	0.054	738.0	684.0	0.0000
THE	CUBE	15.0	36.0	2.0		0.0		25.0	10.0	10.0	2.0	0.0	1.0	0.9	2.0	8.0	21.0	1.0	3.0	8.0	4.0	72.0	14.0	22.0	1.0	2.0	25.0	14.0	3726.0				2520.0	0.0	0.49	128.0	8.0	44.0			16.0	18.0	36.0	
1/E	SGUARE				162.0		205.0																							1050.0	366.0	360.0							240.0	1560.0				264.0
ITEM	WEIGHT	159.0	47.0	3.0	8100.0	0.0	1975.0	20.0	0.6	12.0	42.0	0.0	42.0	0.96	0.46	115.0	182.0	45.0	25.0	104.0	10.0	1122.0	523.0	93.0	45.0	33.0	22.0	26.0	0.0506	4190.0	2535.0	2670.0	2575.0	0.0	101.0	139.0	23.0	20.0	3370.0	2761.0	55.0	42.0	38.0	3330.0
TEM	CUBE	5.0	3.0	1.0		0.0		1.0	1.0	1.0	1.0	0.0	1.0	3.0	2.0	4.0	2.0	1.0	1.0	4.0	1.0	36.0	2.0	11.0	0.1	1.0	1.0	1.0	1242.0				320.0	0.0-	8.0	8.0	1.0	1.0			2.0	2.0	2.0	
ITEX	SQUARE				162.3		41.0																							20.0	0.19	0.09							0.09	0.09				98.0
	74%	4000\$	46030	40:30	40240	40004	0750x	Ac320	A0 328	A0400	40560	AOGAS	A9710	A0730	A0800	47910	40470	A0912	A1140	A1190	A1250	A1290	A1 300	A1420	A1570	A1630	A1730	A1H00	0681V	A1 900	A1920	A1930	A1940	A1950	A2010	A2720	42040	A2050	A2182	A2183	A2184	A2220	42270	42 110

HEADQUARTERS BATTALION, MARINE DIVISION CURTATE TZE FOR CLASS VII, CLASS II TAM ITEMS

CONSTRAINED TO 75.0 PCT OR 15212.00 CU FT CONSTRAINED TO 75.0 PCT OR 15212.00 CU FT

SQUARE OF QUALISHED TZE IS 21537.00 SQ FT CUNSTRAINED TO 75.0 PCT OR 16153.00 SQ FT

	ITEM	I TEM	ITEM	1/5	1/5	17.6	1/E	211	****	********	1/F***	Creffe.
144	SOUARE	CUSE	WEIGHT	SQUARE	CUBE	WE IGHT	VT0		710		CUBE	11.404
A2.120	98.0		3100.0	176.0		6200.0	~	•	2.	176.0		
A2340	88.0		4750.0	88.0		4750.0	-	4	:	98.0		
A2350	96.0		4750.0	80.0		4750.0	-	•	-	80.0		
42480		1.0	28.0		14.0	392.0	14	60	14.		14.0	
A2560		10.0	262.0		30.0	786.0	n	. 8	3.		30.0	
A2510		53.0	145.0		106.0	200.0	2	4	2.		106.0	
A2550		5.0	0.06		40.0	720.0	8	8	8.		40.0	
A2635		1.0	10.0		28.0	280.0	28	89	28.		28.0	
A2700		1.0	20.0		2.0	40.0	8	4	2.		2.0	
A2710		1.0	25.0		4.0	100.0	4	4	• •		0.4	
42920		10.0	115.0		10.0	115.0	-	•	1:		10.0	
A3012		0.0	0.0		0.0	0.0	N	2	5.		0.0	
A3050		10.0	45.0		10.0	45.0	-	4	1:		10.0	
A3065		1.0	15.0		1.0	15.0	-	4	:-		1.0	
A3238		2.0	21.0		12.0	125.0	9	Œ	.4		12.0	
43280		1.0	15.0		3.0	45.0	3	4	3.		3.0	
10005	2.0		200.0	10.0		400.0	2	4	2.	10.0		
90009	2.0		265.0	16.0		2120.0	•	4	7.	13.7		:
11008		0.0	0.0		0.0	0.0	4		. 4		0.0	
30465	24.0		2641.0	54.0		2641.0	-	2	:	54.0		
80470		6.9	130.0		41.2	780.0	S	2	.,		41.2	
80490		29.0	312.0		29.0	312.0	-	Œ	:		29.0	
80500		8.1	225.0		8.1	225.0	-	4	:		1.9	
91360		8.0	255.0		32.0	1020.0	4	4	•		32.0	
81430		7.5	138.0		30.0	552.0	4	8	• •		30.0	
B1440		31.0	407.0		31.0	407.0	-	8	:		31.0	
81445		0.0	0.0		0.0	0.0	-	8	:		0.0	
9:620		10.0	220.0		10.0	220.0	-	4	:		10.0	
91755		74.0	4471.0		74.0	4471.0	-	60	:		74.0	
85080		4.	0.6	4.	2.3	54.0	ç	89	•		2.3	
85550		4.2	140.0		4.2	140.0	-	*	-1		4.2	
92.590		6.5	100.0		6.5	100.0	-	2	:		6.5	
C2010		۳.	4.0		10.8	140.0	35	-	28.		8.8	7.
C2030		.5	6.0		16.8	210.0	35	1	27.		13.2	8.
C5040		••	3.0		18.9	210.0	7.0	1	57.		15.4	13.
C2050		.8.	. 7.0		26.3	245.0	35	-	27.		19.9	8.
C2060		0.	1.0		0.	4.0	•	-	•		0.	
C2070		1.9	60.09		14.8	480.0	8	-	٠,		14.9	
C2100		.2	3.0		£.	15.0	2	-	•		8.	
C2160		:	1.0		4.3	70.0	10	-	62.		4.3	v
C2230		0.	0.1		:	2.0	9	-			:	
05273		.2	5.0		5.3	20.0	35		30.		4.5	5.
01110			0.6		24.0	10.0	13	1 .	.27.		18.2	α.

HEADQUARTERS BATTALION, MARINE DIVISION

CLRIATE TZE FUR CLASS VII. CLASS II TAM ITEMS

COUE OF PUBLISHED TZE IS 21616-34 CU FT CONSTRAINED TO 25.0 PCT OR 16212-00 CU FT

SQUARE OF PURLISHED TZE IS 21537-00 SO FT CONSTRAINED TO 75.0 PCT OR 16153-00 SO FT

DF F 10-	TE NCY	127.																	•		3.			21.	16.				11.	24.	. 4		35.			10.			33.		15.	2.		
1/5****	CUBE	360.7	100.8	26.0	1.3	٠.	61.1	3.4	3.4	21.0	0.44	15.3	4.9	72.0	18.0	0.09	2.8	5.	30.0	132.8	219.0	8.	101.9	140.3	258.9	8.4	30.0	12.1	63.1	172.6	5.0	64.0	420.2	6.6	42.7	219.7	101.0	46.7	340.5	0.00	351.2	10.5	34.2	30.0
************	SOUARE																																											
****	410	364.	15.	13.	-	8.	19.	7.	2.	٠,	. 4	5.	638.	:	•	5.	2.	3.	20.	17.	15.	15.	16.	39.	18.	٠,	2.	3.	24.	46.	40.	:	55.	:-	5.	2.	:	-	20.	10.	14.	22.	.0	٠.
CRIT		-	-	-	-	-	-	-	-	-	-	-	-	æ	1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1/5	710	491	16	13	-	8	12	1	2	S	4	2	638	-	·	S	2	r	56	52	18	15	16	9	34	2	^	٣	35	20	44	-	87	1	2	12	-	-	83	10	50	54	8	Ν.
17.6	WEIGHT	7856.0	1280.0	650.0	27.0	40.0	840.0	10.07	225.0	265.0	256.0	120.0	638.0	918.0	510.0	1050.0	12.0	0.9	1040.0	100000	2700.0	750.0	1360.0	480.0	5100.0	148.0	200.0	588.0	4 90.0	280.0	44.0	1012.0	14094.0	86.0	475.0	28500.0	1306.0	756.0	12450.0	1310.0	10257.0	240.0	304.0	2720.0
17E	CUBE	486.1	100.8	26.0	1.3	٠٠	68.5	3.4	3.4	21.0	44.0	15.3	6.4	72.0	18.0	0.09	2.8	·.	2005	192.2	270.0	.8	101.9	213.6	476.0	8.4	30.0	12.1	. 93.1	564.6	2.2	0.99	6.602	9.9	42.7	1740.0	101.0	46.7	577.7	0.00	725.0	51.6	34.2	C • 33
1/E	SQUARE																																											
ITEM	WEIGHT	16.0	80.0	20.0	27.0	5.0	40.0	10.0	45.0	53.0	0.49	0.09	1.0	918.0	85.0	204.0	0.9	2.0	40.0	40.0	150.0	20.0	88.0	8.0	150.0	74.0	250.0	196.0	14.0	0.4	1.0	1012.0	162.0	86.0	0.56	2375.0	1306.0	756.0	150.0	131.0	353.0	10.0	38.0	1350.0
ITEM	CUBE	1.0	6.3	2.0	1.3		3.3	5.	2.	4.2	11.0	7.7	0.	72.0	3.0	12.0	1.4	.2	2.0	7.7	15.0	:	4.9	3.6	14.0	4.2	15.0	4.0	2.7	3.8		0.99	8.2	9.9	8.6	145.0	101.0	46.7	7.0	0.6	25.0	6.	4.3	15.0
ITEM	SQUARE																																											
	144	03050	00040	04010	C4015	64020	C4040	C4140	C4230	64250	C4340	C4390	64436	C4640	C4650	C4660	C4470	C4630	C4890	C4790	C4820	C4830	C4870	C4 830	C4980	C2070	08053	06050	C5110	C2200	C5300	C5310	C5320	C5330	C5340	C5370	C5380	65330	C6460	C5410	C582G	C5830	02953	0.653

# HEADQUARTERS BATTALION. MARINE DIVISION

CURTATE THE FOR CLASS VII. CLASS II TAM ITEMS

CUBE DF PUBLISHED TZE IS 216,16.34 CU FT CONSTRAINED TO 75.0 PCT OR 16212.00 CU FT

SOUAPE OF PUBLISHED TZE IS 21537.00 SO FT CONSTRAINED TO 75.0 PCT OR 16153.00 SO FT

PEFIC-		10.									7.		25.	21.						10.	•																	15.	•	1.		5.	
T/E****	0.00	100.0	4.3	0.4	-	1:1	4.0	5.5	65.0	126.0	1111.0	58.7	272.5	401.8	230.0	30.0	27.5	100.0	47.4	28.3	2.0	3.3	2.8		40.0	16.0		2.7	5.	1.2	1.4	250.0	97.0	107.4	£.	0.	342.8						
*****REDUCED																								75.0			110.0											1943.5	1853.1	365.8	21.0	075.4	
, 710	•	40.	•	:	:	.0		11.	.9	٠,	18.	10.	38.	22.	2.	-12	4.	2.	15.	30.	2.	327.	2.	2.		. 4	-	2.	:	2.	2.		3.	3.	:	:	. 4	42.	19.	. 4		7.	
CRIT	-	-	1	-	-	-	-	-	-	-	1	-	1	-	-	-	-	-	-	-	-	-	2	4	2	1	2	2	2	2	CJ	2	2	2	2	2	2	4	v	*	2	4	4
17E	6	29	3	-	-	•	-	=	9	9	52	10	63	43	~	23	4	2	15	40	2	327	2	2	2	*	-	2	-	2	2	2	2	3	-	-	4	57	28	5	1	1.2	24
T/E WEIGHT	8280.0	200000	93.0	134.0	3.0	42.0	138.0	77.0	30.0	1380.0	2675.0	1400.0	16191.0	14190.0	4296.0	1426.0	350.0	60000	450.0	720.0	20.0	327.0	26.0	2108.0	326.0	2069.0	5855.0	45.0	16.0	32.0	22.0	3664.0	1980.0	2130.0	8.0	0.1	7550.0	32490.0	77000.0	13550.0	2780.0	38440.0	127540.0
T/E CUBE	0.66	162.8	4.3	0.4		1.1	4.0	5.5	0.99	125.0	157.5	58.7	452.3	774.0	238.0	34.5	27.5	100.0	47.4	38.0	2.0	3.3	2.8		40.0	16.0		2.7	5.	1.2	1.4	250.0	87.0	107.4	.3	c.	362.8						
T/E SQUARE																								76.0			113.0											2522.0	2688.0	465.0	71.0	1608.0	0.4000
ITEM	0.026	10000	31.0	134.0	3.0	7.0	138.0	7.0	2.0	230.0	107.0	140.0	257.0	330.0	2148.0	62.0	0.06	300.0	30.0	18.0	25.0	1.0	28.0	1054.0	163.0	517.0	5855.0	21.0	16.0	16.0	11.0	1832.0	0.099	710.0	8.0	1.0	1890.0	620.0	2750.0	2710.0	2780.0	7370.0	13560.0
LTEM	0.11	2.8	1.5	4.0	:	• 5	4.0	• 5	11.0	21.0	6.3	5.9	7.2	18.0	119.0	1.5	6.9	20.0	3.2	6.	1.0	0.	1.4		20.0	4.0		1.4	• 5	9.	1.	125.0	29.0	35.8	.3	0.	2.06						
SGUARE																								38.0			119.0											46.0	0.96	93.0	71.0	134.0	176.0
TAM	02650	C5930	05650	00090	C6030	C6140	66150	C6220	09290	C6350	C6370	C6388	Ce390	C6410	02490	C5430	01590	CF650	C6650	02990	C6480	C6684	02000	06000	00100	00110	00100	06800	00400	01400	00450	00725	00730	00740	00100	00165	02100	00840	09990	08866	06800	01020	01010

CONSTRAINED THE FOR UNIT MI988

HEADQUARTERS BATTALION. MARINE DIVISION

CLEIATE TZE FOR CLASS VIII. CLASS II TAM ITEMS

CURE OF PUBLISHED TZE IS 21616.34 CU FT CENSIVAINED TO ZN.0 PCT OF 16212.00 CU IT

SQUARE OF PUBLISHED TZE IS 21537.00 SO FT CONSTRAINED TO 75.0 PCT OR 16153.00 SO FT

-31230	15 NC Y	-	1 8.			12.	10.												
*/E****	CURE					180.8	440.3		15.7	20.7	7.8	0.0	0.0	0.	-	1.9	2.0	2.3	16212.0
******	SOUARE	6.054	2312.7	213.2															16153.016212.0
:	7 10	٠,	48.	:	*	15.	12.	11.	4.	7.	.0	•	2.	:	2.	.9	2.	2.	3078.
CPIT		4	4	2		. 1	1	-	2	2	4	2	2	4	2	2	80	2	
1/5	410	3	99	-	4	27	22	11	4	1	9	0	2	-	~	9	2	2	3625
1/E	WEIGHT	68880.0	158400.0	34250.0	9.0	81.0	154.0	11.0	432.0	623.0	144.0	0.0	0.0	1.0	4.0	48.0	10.0	78.0	21615.3 1315058.0
1/E	CUBE				•	324.0	858.0	:	35.7	20.7	7.8	0.0	0.0	0.		1.9	2.0	2.3	21616.3
1/E	SOUARE	768.0	4026.0	239.0															21537.0
ITEM	WEIGHT	22950.0	2400.0	34250.0	2.0	3.0	7.0	1.0	108.0	89.0	24.0	0.0	0.0	1.0	2.0	8.0	5.0	39.0	
1 TEN	CUBE				0.	12.0	39.0	0.	6.9	3.0	1.3	0.0	0.0	0.	0.	.3	1.0	1.1	OTALS
TEN	SQUARE	256.0	61.0	239.0															GRAND T
	TAM	01000	0110	01210	01250	E0040	E0000	E0210	E0320	F.0980	06603	E1155	E1155	£1240	E1403	E1750	E1900	E2030	

TODAYS DATE 03/02/76
OR INDEX(SQUARE) = 79.80
OR INDEX(CUBE) = 91.57
OR INDEX(TOTAL 1/E) = 89.31

### CONSTRAINED THE FOR UNIT MBAIS

#### H+HS. VACG

CURTATE TIE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED TZE 1S 5412-05 CU FT CONSTRAINED TO 85.0 PCT UR 4600.00 CU FT SQUARE OF PUBLISHED 1ZE 1S 7301.00 SO FT CONSTRAINED TO 85.0 PCT OR 6205.00 SO FT

9FF IC-	IF NO.Y																																		NOTE:		Unit = M8615	1000 - taisent	constraint = 30%		2.	•6		
*****REDUCED T/E***	cuar.	0.1	0.0	٠,	2.0		1.0	10.0	17.3	13.1		٠.	1.5	2.4	7.7	3.5	0.	3.7	1.0	۲.	74.4		0.	0.	٠.	3.4	12.0		0.0	1.0	3.4	21.0	25.0	5.0	24.0	24.0	1.0	*.	3.0	7.7	201.7	150.3	43.4	372.0
**RFDUCF	SOUNDE			141.6		20.0					156.9																																	
**	914		-	-	2.		-	•	. 4	2.	2.	2.	5.	5.	10.	5.	-	v.		2.		10		-		5.		2.	3.	2.	-		2.	200.	2.	2	-	2.	ė	-	0	24.	13.	
CRIT		4	•	2	α	2	2	2	~	2	2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2	-	-	-	-	-	-	-	-	-
TIE	717	-	-	-	~	1	-	4	4	2	~	2	5	2	10	S	-	2	r	2	2	10	2	-	2	r	9	~	3	^	-	r	~	500	~	2	-	2	2	-	5:	33	er -	*
1/6	WFIGHT	25.0	110.0	9525.0	232.0	6.000	23.0	532.0	392.0	200.0	6200.0	2.0	20.0	30.0	30.0	35.0	1.0	120.0	25.0	0.9	1240.0	10.0	3.0	1.0	10.0	10.0	300.0	10.01	120.0	20.0	52.0	245.0	129.0	200.0	400.0	408.0	6.0	0.4	80.0	40.0	3150.0	2803.0	120.0	1900.0
1/5	CUBE	1.0	4.0		2.0		1.0	19.0	17.3	13.1		0.	1.5	2.4	2.1	3.3	0.	3.7	1.0	·.	75.4		0.	6.		3.4	12.0	·.	0.3	1.0	3.4	51.0	22.0	2.0	26.0	24.0	1.4		3.3	7.7	315.0	210.5	63.4	
1/E	SOUARE			143.0		20.0					166.0																																	
ITEM	WEIGHT	25.0	110.0	9525.0	116.0	0.069	28.0	133.0	98.0	100.0	3100.0	1.0	4.0	0.9	3.0	7.0	0.1	0.05	2.0	3.0	620.0	1.0	1.0	1.0	2.0	2.0	20.0	4.0	40.0	10.0	52.0	53.0	0.09	1.0	50000	204.0	0.9	2.0	40.0	40.0	150.0	0.54	0.0	0.000
ITEM	CURE	1.0	0.4		1.0		1.0	4.8	4.3	6.5		0.	.3	6.		.3	0.	1.9	• 5	• 5	37.7	:	0.	0.	• 5	1.	5.0	•	3.3	5.	3.4	4.2	11.0	0.	13.0	15.0	1.0	.2	5.0	7.7	15.0	4.0	3.0	12%,0
ITEM	SOUARE			143.0		20.0					93.0																																	
	TAM	A2710	06006	96508	00515	32060	55128	92230	15500	42.390	92590	C5033	02010	02030	C2040	05023	65050	02020	C2080	00120	C2120	C2160	C2200	C2230	C2250	C2310	04010	02040	04040	C4140	04240	C4250	04340	04436	C4630	09940	04470	08440	06540	64790	02000	C4870	CARRO	00000

#### H+HS. MACG

DEFIC.

SQUARE

17%

C4050 C5020 CS100

. 4.

111.8 2.0.0

\*\*\*\*\*REDUCED T/E\*\*\*\*
OTY SOUARE CUSE CRIT CLATATE TZE FOR CLASS VII. CLASS II TAM ITEMS F 1 17E 5412.05 CU 4600.00 CU 7301.00 50 621.0 1127.0 1127.0 1277.0 12012.0 72012.0 7300.0 7 21.0 21.0 600.0 213.0 600.0 12888.0 4112.0 COUSE OF BURISHED TZE IS CONSTRAINED TO 85.0 PCT OR GOVAPE OF PUBLISHED TZE IS CONSTRAINED TO 85.0 PCT OF 31.0 714.0 12.6 3.0 158.2 12.5 58.7 114.9 66.0 SOUAPE NEIGHT LTEM

27.

31.0

193.0

143.0

153.0

30.0 197.0

30070

C6520 C6550 C6590

C6630

C6650 C6658 C6658 C6670 C6684

CS410 CS330 CS320 CS420 CS430 CC4130 CC4130 CC520 CC520 CC520 CC520 CC520 CC520 CC520 CC520 CC520 CC530 CC530 CC530 CC530 CC530 CC530 CC520 CC52

C5210 C5200 C5310 C5320 C5370 C5470

#### H+HS. MACG

SMALI	tt	<u> </u>
Y	53	SOS
ASS 11 T	5412.05	7301.00
5	1.5 0.8	15
CURTATE TZE FOR CLASS VIII. CLASS II TAM ITFWS	CURE OF PUBLISHED TZE IS 5412.05 CU FT CONSTRAINED TO 95.0 PCT OR 4600.00 CU FT	SQUARE OF PUBLISHED TZE IS 7301-00 SO FT CONSTRAINED TO 85.0 PCT OR 6205-00 SO FT
T/F FOR	OF PUBLI	OF PUHLI
CURTATE	CONSTR	SQUARE

	5855.0 1 2 10.0 1 2 16500.0 1 4 27000.0 2 2 35392.0 1 2 17772.0 1 2 18030.0 1 2	\$855.0 1 2 10.0 1 2 16500.0 1 4 27000.0 2 2 35392.0 1 2	<b>~</b>	119.0	119.0	119.0
0	10.0 1 2 16500.0 1 4 27000.0 2 2 35392.0 1 2 1772.0 1 2		∾.	6.		
1 2 4 8	16500.0 1 4 27000.0 2 2 35192.0 1 2 17772.0 1 2	16500.0 1 4 27000.0 2 2 35342.0 1 2 18030.0 1 2				.2 10.0
2 2	27000.0 2 2 35352.0 1 2 17772.0 1 2	35392.0 2 2 35392.0 1 2 2 1 7 2 0 1 1 2 2 1 2 2 1 2 2 1 2 2 1 2 2 1 2		331.0	331.0	16550.0 331.0
	35392.0 1 2 17772.0 1 2 18030.0 1 2	35392.0 1 2 17772.0 1 2		458.0	458.0	13500.0 458.0
1 2	18030.0 1 2	17772.0 1 2		364.0	364.0	35392.0 364.0
1 2	18030.0 1 2	18030.0		182.0	182.0	17772.0 182.0
1 2		7 . 0.0000.	182.0 18030.0 1 2		182.0	18030.0 182.0
1 2	70.0 1 2	.9 70.0 1 2			40.0	40.0
1 2	11.0 1 2			•	11.0	11.0
1 2	30.0 1 2			4.	30.0	30.0
1 2	1.0 1 2	.1 1.0 1 2		•	1.0	1.0
1 2	650.0 1 2			28.0	450.0 28.0	450.0 28.0
1 2	495.0 1 2	28.0 495.0 1 2		28.0	495.0	495.0
1 8	1250.0 1 8	87.0 1250.0 1 8		87.0	1250.0 87.0	1250.0 87.0
1 2	1.0 1 2			0.	1.0	1.0
1 5	1890.0 1 2		2.06	1.06	1,900.0	7.06 0.000 0.000
4 .	2280.0 4 4	2280.0 4 4		184.0	184.0	570.0 184.0
8 .			10840.0	372.0	372.0	2710.0 372.0 10840.0
8			109280.0	1498.0	1408.0	0 0000
2 2						0.0001
80			43962.0	380.0	380.0 43962.0	21981.0 380.0 43962.0
•	0	v 80	43962.0 2 2 29940.0 2 8	370.0 29940.0 2 8	380.0 43962.0 2 2 3 370.0 29940.0 2 8	15050.0 1405.0 10050.0 8 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
,	c	v 6: 6	43962+0 2 2 29940+0 2 8 29500+0 2 8	340.0 43962.0 2 2 3 370.0 29940.0 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	380.0 43962.0 2 2 370.0 29940.0 2 8	217830*0 1495*0 107250*0 8 4 21781*0 380*0 43962*0 2 14970*0 370*0 29940*0 2 14750*0 358
	0 60	N & &	43962.0 2 2 29940.0 2 8 29500.0 2 9	370.0 29940.0 2 3 3 3 3 3 3 5 9 9 9 9 9 9 9 9 9 9 9 9 9	380.0 43962.0 2 2 3 370.0 2 2 2 3 370.0 2 8 358.0 27500.0 2 8	21981-0 380-0 43962-0 2 2 2 14970-0 370-0 29940-0 2 8
6	0	v 60	43962.0 2 2 29940.0 2 8	370.0 29940.0 2 8	380.0 43962.0 2 2 370.0 29940.0 2 8	21981-0 380-0 43962-0 2 2 14970-0 370-0 2 2 8
	v	v ~:	43962.0 2 29940.0 2	370.0 29940.0 2	390.0 43962.0 2 370.0 29940.0 2	21981-0 380-0 43962-0 2 14970-0 370-0 29940-0 2
	44000		2289.0 10840.0 109289.0	372.0 10840.0 1499.0 109289.0	372.0 10840.0 1498.0 109280.0	372.0 10840.0
		1000 1000 1000 1000 1000 1000 1000 100	17772.0 18030.0 -9 70.0 -0 11.0 28.0 650.0 28.0 650.0 28.0 1250.0 0.0 1250.0 1.0 90.7 1890.0 10840.0	182.0 17772.0 18030.0 182.0	18772.0 182.0 17772.0 18030.0 18030.0 170.0 18030.0 17	18030.0 182.0 17772.0 18030.0 17772.0 18030.0 182.0 18030.0 18
	70.0 30.0 30.0 11.0 650.0 495.0 1250.0 1890.0 10880.0 10880.0	6 4 4 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	28.0 9.0 28.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9	182.0 182.0 182.0 180.0	3539220 35440 353 177720 1820 177720 180300 1820 1870 170 7000 1820 170 1100 -9 170 3000 -9 170 495.0 280.0 4 1250.0 1840 22 2710.0 1893.0 1092	3539000 45300 6570 6570 6570 6570 6570 6570 6570 65

TODAYS DATE 03/03/76
OR INDEX(SOUARE) = 87.62
OR INDEX(CUBE) = 91.59
OR INDEX(IOTAL I/E) = 90.86

#### H+HS. MACG

CURTATE TZE FOR CLASS VII, CLASS II TAM ITFMS

CUME OF PUBLISHED TZE IS 5412.05 CU FT CONSTRAINED TO 77.5 PCT OP 4194.00 CU FT

SQUARE OF PURLISHED TZE 15 7301.00 SO FT CONSTRAINED TO 77.5 PCT OR 5658.00 SO FT

																																				513	2	1t = 85%						
- LEELIC-	IENCY																																	NOTE:		Thit = M8615	2110	Constraint			٠,	. 4.		
1/: ***	CUBE	1.0	0.4		6.2		1.0	10.0	17.3	13.1		0.	1.5	2.4	2.0	3.8	c.	7.5	1.0	£.	75.4		0.	c.	۵.	3.4	12.0		9.8	1.0	4.6	21.0	22.0	2.0	26.0	24.0	4.1	•	C. E.	7.7	257.7	123.3	53.0	3.5.0
******EDJCF0 T/	SOJARE			125.4		20.0					143.8																																	
****	710	:	1.	:	2.	:	:	4	. 4	5.		5.	5.	5.	10.	5.	:-	5.	ľ	2.	5.	10.	3.	:	5.	٠ د	• 9	2.	3.	2.		5.	2.	200.	5.	2.	:	٠.	2.	:	15.	10.	15.	
CRIT		4	4	2	8	. 2	N	~	2	2	2	-	-	-	-	1	-	-	1	-	1	-	-	-	-	-	1	-	-	-		-		-	2	-	1	-	-	-	-	-	-	-
1/5	710	-	-	-	2	-	-	4	4	2	2	8	c	S	0.1	S	-	2	2	2	^	10	2	-	2	r	9	2	n	2	-	S	2	200	2	2	-	C1	~		51	33		•
1/E	WE I GHT	25.0	110.0	9525.0	232.0	0.069	28.0	532.0	392.0	200.0	6200.0	2.0	20.0	30.0	30.0	35.0	1.0	120.0	25.0	0.9	1240.0	10.0	3.0	1.0	10.0	10.0	300.0	10.0	120.0	20.0	52.0	255.0	128.0	200.0	400.0	408.0	0.9	4.0	80.0	0.04	3150.0	2805.0	120.0	0.1001
1/5	CUBE	1.0	4.0		2.0		1.0	19.0	17.3	13.1		0.	1.5	2.4	2.7	3.8	0.	3.7	1.0	•3	75.4		0.	· ·		3.4	15.0	•5	8.6	1.0	3.4	21.0	22.0	2.0	26.0	24.0	1.4	7.	3.9	7.7	315.0	210.2	53.4	37.4.0
1/5	SQUARE			143.0		20.0					166.0																																	
ITEM	WEIGHT	25.0	110.0	9525.0	116.0	0.069	28.0	133.0	0.86	100.0	3100.0	1.0	4.0	0.9	3.0	7.0	1.0	0.09	2.0	3.0	620.0	1.0	1.0			N		S	40.0	10.0	52.0		64.0		200.0		0.4	2.0	40.0	40.0	0.051	85.0	9.0	60000
1 TEM	CUBE	1.0	4.0		1.0		1.0	4.8	4.3	6.5		•	.3	• 5	•3	8.	•	1.9	.2	•2	37.7	•	0.	•	• 5	.7	2.0	:	3.3	• 5	3.4	4.2	11.0	0.	13.0	12.0	1.4	.2	2.0	7.7	15.0	6.4	3.6	124.0
ITEM	SOUARE			143.0		20.0					83.0																																	
	144	A2710	05006	90390	31540	65055	42155	92280	35290	92 190	92680	00020	01023	C2030	C2040	05020	09023	C2070	C2080	C2100	C2120	C2160	C2200	C2230	C2250	C2310	C4010	C4020	C4040	C4140	C4240	C4250	C4 340	C4436	C4630	C4560	C4670	C4680	56693	C4790	07-10	C4810	C4800	64000

#### H+HS. MACG

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CONSTRAINED TO 77.5 PCT OR 4194.00 CU FT

SQUARE OF PUBLISHED T/F IS 7301.00 SQ FT CONSTRAINED TO 77.5 PCT OR 5658.00 SQ FT

DEFIC-					15.		20.		18.																		38.		ď														
1/E****	11.8	0.0	2.7	26.6	95.2	66.0	207.3	145.0	150.2	54.0	1.8	4.3	38.0	22.0	22.1	2.0	:	12.6	3.0	164.2	96.0	2.1		12.6	58.7	114.0	647.0	714.0	20.4	· ·	٠.	31.0	6.0	100.0	α.	.2	4.7	0.	0.	a . c.		20.0	
*****FEDUCED																																									76.0		193.0
****	3.	3.	-	10.	25.	:	25.	-	24.	.9	2.	-	-:	2.	8	:	:	2.	•	2.	• 9	:		2.	10.	16.	37.	• 9	20.	:	:	-	3.	2.	15.	4.	5.	•06	:	2.	5 .	:	:
CRIT	-	-	-		. 1		-	-	1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1		-	-	-	-			1	-	2	4	2	α
1/E	•	3	-	10	40	-	45	-	42	9	2	-	-	2	60	-	-	2	9	2	9	-	9	2	01	16	75	9	28	-	-		3	2	15	4	5	06	-	~	c	-	-
T/E WE IGHT	285.0	621.0	127.0	140.0	160.0	1012.0	7290.0	2375.0	6300.0	786.0	20.0	39.0	642.0	1840.0	800.0	25.0	3.0	492.0	30.0	2508.0	0.006	144.0	24.0	214.0	1400.0	4112.0	24750.0	12888.0	1736.0	35.0	21.0	60009	213.0	0.009	15.0	4.0	0.06	0.06	1.0	26.0	2104.0	163.0	16956.0
TZE	11.8	0.0	2.7	56.6	151.2	66.0	367.2	145.0	292.3	24.0	1.8	4.3	38.0	22.0	22.1	2.0	-	12.6	3.0	168.2	66.0	2.1		12.6	58.7	114.9	1350.0	714.0	45.0	6.	• 5	31.0	0.9	100.0	. 3	.2	4.7	6.	0.	2.8		20.0	
SOUARE																																									76.0		1.43.0
WEIGHT	95.0	207.0	127.0	14.0	4.0	1012.0	152.0	2375.0	150.0	131.0.	10.0	38.0	642.0	920.0	100.0	25.0	3.0	246.0	2.0	1254.0	150.0	144.0	4.0	107.0	140.0	257.0	330.0	2148.0	62.0	35.0	21.0	600.0	71.0	300.0	1.0	1.0	18.0	1.0	1.0	28.0	1054.0	163.0	16455.0
CUBE	3.9	3.0	2.7	2.7	3.8	0.99	8.2	145.0	7.0	0.6	0.	4.3	38.0	11.0	2.8	2.0	:	6.3	• 5	84.1	11.0	2.1		6.3	5.9	7.2	18.0	119.0	1.5	•	• 5	3:00	2.0	20.0	:	:	6.	0.	0.	1.4		20.0	
SGUARE																																									38.0		183.0
TAN	09000	02050	00160	C3110	C5200	C5310	C5320	C5370	C5400	C5410	C5930	C5870	00653	CS420	C2430	C5940	C60 30	C61.30	C6220	C6230	C6260	C6280	C6290	C6370	C6388	C6 190	C6410	C6420	06490	C6520	05593	00290	C6630	05993	55993	66658	02990	C5534	50000	02000	00000	00100	00100

#### CONSTRAINED THE FOR JULT MBS15

H+HS. MACG

CURTATE TZE FUR CLASS VII. CLASS II TAM ITEMS

CONSTRAINED TO 77.5 PCT UR 4194.00 CU FT CONSTRAINED TO 77.5 PCT UR 4194.00 CU FT SQUARE OF PUBLISHED TZF IS 7301.00 SO FT CONSTRAINED TO 77.5 PCT UR 5658.00 SO FT

TENIX.					:													:		3.				:	3.	:	:			
*****/									0.	••	4.	••	28.0	28.0	97.0	٠.	2.00											1.2	6.4	3
**************************************		109.7		240.2	330.5	242.0	150.4	150.4										155.4	372.0	972.1	245.2	370.0	358.0	381.2	333.3	378.9	341.6			
017		:	:	1:	1:	:	:	1.	:-	:	:	:	:	-1	::		:	3.		5.	. 2	2.	2.	2.	5.	3.	:	3.	20.	:
CRIT		2	8	4	2	. 2	2	2	2	2	2	2	2	2	80	2	2	4	æ	4	2	<b>c</b> c	8	2	4	4	2	1	2	N
777		-	-	-	2	-	-	-	-	-	-	-	-	-	-	-	-	•	4	60	2	2	^	•	8	4	2	3	50	-
T/C WEIGHT	,	5855.0	10.0	16500.0	27000.0	35392.0	17772.0	18030.0	20.07	11.0	30.0	1.0	650.0	495.0	1250.0	1.0	1890.0	2280.0	10840.0	109280.0	43962.0	29940.0	29500.0	52230.0	19200.0	21840.0	68500.0	21.0	160.0	39.0
CUBE	,								0.	6.	4.	-	28.0	28.0	87.0	0.	400											1.2	6.4	::
SQUARE		119.0		331.0	458.0	364.0	182.0	182.0										184.0	372.0	1408.0	380.0	370.0	358.0	543.0	448.0	496.0	478.0			
NE 1GHT		5855.0	10.0	16500.0	13500.0	35392.0	17772.0	18030.0	20.07	11.0	30.0	1.0	650.0	495.0	1250.0	0.1	1890.0	570.0	2710.0	13660.0	21931.0	14970.0	14750.0	17410.0	2400.0	2460.0	34250.0	7.0	8.0	39.0
L TEM	,		.2						6.	6.	4.	•	28.0	28.0	87.0	0.	2.06											**	•3	:
SOUASE	!	119.0		331.0	229.0	364.0	182.0	132.0										46.0	93.0	176.0	190.0	185.0	179.0	181.0	61.0	124.0	239.0			
1.41		06166	01200	06200	99259	00310	00350	00330	00450	00470	00500	00575	00590	00900	00400	00694	02200	09800	09860	01030	01010	01110	01120	01130	01110	91116	01210	60003	61750	E2030

TODAYS DATE 03/02/76
09 INDEX(SQUARE) = 82.91.
0R INDEX(CUBE) = 87.43
0R INDEX(TOTAL T/E) = 86.59

5658.0 4194.0

793.

7301.0 5412.0 634748.0 922

GRAND TOTALS

#### H+HS. MACG

CUNTATE THE FOR CLASS VIL. CLASS II FAM ITEMS

CONSTRAINED TO 62-5 PCT OR 3343-00 CU FT SQUARE OF PUBLISHED TZE IS 7301-00 SQ FT CONSTRAINED TO 62-5 PCT OR 4563-00 SQ FT

DEFIC-	LENCA																																THOIR .	NOIE:		Unit = M8615	Constraint = 75%				•	12.		2.
	CUBE	0.:	0.4		2.0		1.0	10.0	17.3	13.1		c.	1.5	2.4	20.7	N. C	0.	3.7	1.0		75.4	.7	0.	0.	α.	3.4	12.0	.2	9.6	1.0	3.4	0.10	22.0	5.0	26.0	20.0	4.1	4.	0. 5.	7.7	223.9	130.9	53.4	2.10
****** T GEORGED 1/6****	SOUARE			86.3		20.0					116.6																																	
****	710	:	1.	-	. 2	:	:	• •	. 4	5.	:	2.	٠.	5.	10.	5.	-	2.	5.	5.	5.	10.	3.	-	5.	. 2.	٠	2.	3.	2.	:	5.	2.	5000	2.	2.	:			:	15.	21.	15.	<u>:</u>
CPIT		•	4	2	8	. 2	2	2	2	2	2	-	-	-	1	-	-	-	-	-	-		-	-	-	1		-	-	-	-	-	1	-	2	-		-	-	-		-	-	
1/5	27.0	-	-	-	~	-	-	4	4	2	2	2	2	5	10	2	-	2	2	2	2	10	3	-	2	S.	9	2	3	2	-	2	~	500	2	2	-	2	N	-	2.1	33	5:	*1
17E	WE I GHT	25.0	110.0	9525.0	232.0	0.069	28.0	532.0	392.0	200.0	6200.0	2.0	50.0	30.0	30.0	35.0	1.0	120.0	25.0	6.0	1240.0	10.0	3.0	1.0	10.0	10.0	300.0	10.0	150.0	20.0	52.0	265.0	128.0	200.0	400.0	408.0	0.9	4.0	80.0	0.00	3150.0	2805.0	120.0	1300.0
178	CUBE	1.0	4.0		2.0		1.0	19.0	17.3	13.1		0.	1.5	2.4	2.7	3.8	0.	3.7	1.0	•3	75.4		0.	0.	.8	3.4	15.0	.2	6.6	1.0	3.4	21.0	22.0	2.0	56.0	24.0	1.4		3.3	1.1	315.0	210.2	53.4	377.0
17.5	SOUARE			143.0		20.0					166.0																																	
ITEN	WEIGHT	25.0	110.0	9525.0	116.0	0.069	28.0	133.0	0.66	100.0	3100.0	1.0	0.4	0.9	3.0	7.0	1.0	60.09	2.0	3.0	620.0	1.0	1.0	1.0	2.0	2.0	20.0	2.0	40.0	10.0	52.0	53.0	0.49	1.0	200.0	204.0	0.9	2.0	40.0	40.0	150.0	85.0	0.8	60000
1 TEM	CUBE	1.0	4.0		1.0		1.0	4.8	4.3	6.5		••	.3	• 5	•3	8.	0.	1.9	.2	.2	37.7	-	0.	•	•5		2.0	••	3.3	.5	3.4	4.2	11.0	0.	13.0	15.0	1.4	• 5	2.0	7.7	15.0	6.4	3.6	154.0
1 1 5 4	SQUARE			143.0		20.0					83.0																																	
	14%	A2713	CEUCH	90109	H1540	95060	85158	92280	92290	95390	92630	00073	C2010	C2030	C2040	C2050	C2050	62070	C2080	C2100	C2120	C2150	00223	C2230	C2250	C2310	C4010	C4020	04040	04140	04240	C4250	C4340	C4436	64630	09940	C4670	CARBO	64690	05200	C4 320	C4870	CARAG	(4400

#### H+HS. MACG

CURTATE TIE FOR CLASS VII. CLASS II TAM ITEMS

tt	11
55	SO
5412.05	7301.00
15 08	15 08
COUST OF PURLISHED TXE IS 5412,05 CU FT CONSTRAINED TO 62.5 PCT OR 3383,00 CU FT	SQUARE OF PURLISHED TZE 15 7301.00 S9 FT CONSTRAINED TO 62.5 PCT OR 4563.00 S0 FT

PFF1C-	TENCY					14.		18.	1.	16.																		35.	4															
******/	CUBF	11.8	0.0	7.7	56.6	100.0	0.79	221.4	25.1	190.0	54.0	1.8	4.3	38.0	22.0	22.1	2.0		12.6	3.0	158.2	0.99	2.1	.7	12.6	40.45	114.7	717.9	216.8	30.4	0.	٠.	31.0	0.9	100.0	٠.	.2	4.7	6.		2.8		50.0	
*REDUCED	SQUARE																																									63.7		183.0
****	917	3.	3.	:	10.	26.	.1	27.	• 0	26.	• 9	2.	:-	:	2.	•	:	:	2.	.9	2.	• 9	:	.9	2.	10.	15.	40.	2.	20.	:	:	1:	3.	2.	15.	4.	2.	.00	:	2.	.5.	-	:
CRIT		-	-	-	-		1	-	-	1		1	-	-	1	1	-	1	-	-	-	1	-	1	-			-	1		-	-	-	-	1		-	-	-	-	٥.	4	2	۳.
1/6	017	3	٣	-	10	40	-	45	-	42	9	2	-	-	~	8	-	-	2	9	2	9	-	9	2	10	16	75	ç	28	-	-	-	3	2	15	4	r	05	-	2	2	••	-
1/6	WE IGHT	235.0	621.0	127.0	140.0	160.0	1012.0	7299.0	2375.0	6300.0	785.0	20.0	38.0	642.0	1840.0	800.0	25.0	3.0	492.0	30.0	2503.0	0.006	144.0	24.0	214.0	1400.0	4112.0	24753.0	12888.0	1736.0	35.0	21.0	0.009	213.0	0.009	15.0	6.4	0.00	0.06	1.0	50.0	2103.0	153.9	15053
1/E	CUBE	11.8	0.6	2.7	56.6	151.2	6.99	367.2	145.0	292.3	54.0	1.8	4.3	38.0	22.0	22.1	2.0	-:	12.6	3.0	168.2	0.99	2.1		12.6	58.7	114.9	1350.0	7:4.0	42.0	0,	·.	31.0	0.9	100.0	8.	۷.	4.7	0.	0.	2.8		20.0	
1/E	SQUARE																																									16.0		193.0
MELL	WEIGHT	95.0	207.0	127.0	14.0	4.0	1012.0	162.0	2375.0	150.0	131.0	10.0	38.0	642.0	920.0	100.0	25.0	3.0	246.0	5.0	1254.0	150.0	144.0	4.0	107.0	140.0	257.0	330.0	2148.0	62.0	35.0	51.0	0.009	71.0	300.0	1.0	0.1	18.0	1.0	1.0	28.0	1054.0	163.0	1.6000.0
1 TEM	CUBE	3.9	3.0	2.7	2.7	3.8	0.99	8.2	145.0	7.0	0.6	6.	4.3	38.0	11.0	2.8	2.0	7.	6.3	••	84.1	11.0	2.1		6.3	6.5	7.2	18.0	119.0	1.5	6.	.5.	31.0	2.0	20.0	:	-:	6.	0.	0.	1.4		20.0	
1.1EM	SQUARE																																									38.0		183.7
	747	09640	02050	C5100	C5110	00200	01250	CS320	C5370	00450	65410	C5830	CSA 70	00650	C5920	C5930	C5340	C6030	C6130	02290	C5250	09293	C6230	06290	C6.370	C6388	663390	C6410	C6420	06490	C6520	C0250	06593	C6630	05490	55993	ChrsB	62000	66684	56993	02000	00000	00100	901.40

#### H+HS. MACG

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CURTAIN TZE FUR CLASS VII. CLASS II TAM ITEMS	
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TO CONTRACT OF THE PARTY OF THE	The state of the s	SOUNRE OF PURITSHED THE 1S 7301.00 SOFT	CONSTRAINED TO 62.5 PCT 09 4563.00 SO FT
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7E****		•2							0.	4.	:	28.0	28.0	87.0	0.	96.7											1.2	6.4	::	3383.0
*****REDUCED TZE***	78.9		137.6	232.2	124.3	02.60	92.9										138.9	349.7	771.5	204.1	315.3	335.3	235.7	304.8	327.4	237.5				4563.0 3383.0
¥***	-	:	:	:-	•		:	1:	:	:	1.	1.	:	:	:	:	3.	. 4	. 4	:-	2.	2.	2.	ů.	3.	1:	3.	20.	:	788.
CRIT	2	2	4	2	. 2	2	2	2	2	2	2	N	2	œ	2	2	4	89	4	2	80	8	2	4	4	2	1	8	2	
1/E	-	-	-	~	-	-	-	-	-	-	-	-	-	-	-	-	4	4	60	2	2	2	3	80	4	2	n	50	-	922
T/E WEIGHT	5855.0	10.0	16500.0	27000.0	35392.0	17772.0	18030.0	70.0	11.0	30.0	1.0	650.0	495.0	1250.0	1.0	1890.0	2280.0	10840.0	109280.0	43962.0	29940.0	29500.0	52230.0	19200.0	21840.0	68500.0	21.0	160.0	39.0	634748.0
T/E CUBE		01						0.		4.	:	28.0	28.0	87.0	0.	4.06											1.2	6.4	::	5412.0
SQUARE	119.0		331.0	458.0	364.0	182.0	142.0										184.0	372.0	1408.0	380.0	370.0	358.0	543.0	498.0	406.0	479.0				7301.0
NEIGHT	5855.0	10.0	16500.0	13400.0	35302.0	17772.0	18030.0	20.07	11.0	30.0	1.0	0.059	495.0	1250.0	1.0	1890.0	6.075	2710.0	13660.0	21981.0	14970.0	14750.0	17410.0	2400.0	5460.0	34250.0	7.0	8.0	39.0	
CUBE		.2						6.	6.	4.	:	28.0	28.0	87.0	••	2.06											4.	•3	:	STALS
SQUARE	119.0		331.0	229.0	364.0	132.0	182.0										46.0	93.0	176.0	190.0	165.0	179.0	181.0	61.0	124.0	239.0				GRAND TOT
1 44	20100	01250	20230	00200	20310	02800	20330	03400	02430	03560	92590	06500	00900	00400	96900	02700	00440	ровно	01030	01010	01110	01110	01130	09110	01186	01210	E0090	E1760	E2030	

TODAYS DATE 03/02/76
0R INDEX(SQUARE) = 73.33
0R INDEX(CUBE) = 87.65
0R INDEX(TOTAL T/E) = 85.00

#### H+MS. [MAG VH! MAN. FUF

# CURTATE TIE FOR CLASS VII, CLASS II TAN ITEMS

CONSTRAINED TO 85.0 PCT OR 3298.00 CU FT CONSTRAINED TO 85.0 PCT OR 3298.00 CU FT SOUARE OF PUBLISHED TZ 85.0 PCT OR 2583.00 SO FT CONSTRAINED TO 85.0 PCT OR 2583.00 SO FT

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	53.0 195.0 212.0 750.9 4 1 0.0 0.0 0.0 13 1 72.0 0.56.0 72.0 918.0 1 2 3.0 65.0 3.0 85.0 1 1 12.6 204.0 24.0 24.0 1.4 1.4 6.0 1.1

#### H+45. (MAG VH) MAW. FINF

CURTAIN TAE FUR CLASS VII. CLASS II TAM ITEMS
CUSE OF PUBLISHED TAE IS 3880.49 CU FT
CUNSTRAINED TO 85.0 PCT OR 32994.00 CU FT

SQUAPE OF PUBLISHED TZE IS 3045.00 SO FT CONSTRAINED TO 85.0 PCT OR 2589.00 SO FT

-31-30	11 404				3.						15.	10.															21.																	
1/5***	CUBE	g.	104.6	15.4	253.3	25.5	42.7	140.0	30.0	23.9	125.5	140.0	6.6	69.6	0.0	100.0	1.8	4.3	11.0	-:	6.3	1.5	8.3	4.2	31.5	70.4	492.5	505.0	4.5	6.0	50.0	2.3	r.	٠.	0.	1.0		40.0	.5	1.4	۴.		0.	156.0
RREDUCED	SOUAPE																																				125.0							
****	V 10	3.	. 2 .		17.	•	12.	10.	2.	•	33.	17.	:	10.	:	• •		:	•	:	:	3.	۸.	84.	٠,	12.	27.	5.	3.	:	:	45.	5.	.09	:-	:	:	2.	:	:	<u>:</u>	:		:
CRIT		-		-	-	. 1	-	-	1	1	-	-	-	-		-		-	1	-		1	-	-	1	1	-	-	-	-	-	-	-		-	2	4	2	2	2	2	2	N	6.
1/5	710	2	~	2	20	4	12	10	2	0	48	27	-	01	-	•	~	-	•	-	-	r	4	84	c	12	4	S		-	-	45	S	20	-	-	-	2	-	-	-	-	-	-
1/5	WEIGHT	120.0	1266.0	RO.0	3000.0	340.0	0.96	1500.0	200.0	126.0	192.0	4374.0	86.0	1500.0	131.0	1412.0	20.0	39.0	400.0	3.0	246.0	15.0	576.0	0.48	535.0	1680.0	15840.0	10740.0	186.0	0.06	300.0	45.0	2.0	0.09	0.1	23.0	2650.0	326.0	16.0	21.3	16.0	11.0	1.0	1872.0
1/E	CUDE	5.3	106.6	15.4	300.0	25.5	42.7	140.0	30.0	23.9	181.4	220.3	9.9	9.69	0.0	100.0	1.8	4.3	11.0		6.3	1.5	8.3	4.2	31.5	70.4	864.0	595.0	4.5	6.9	20.0	2.3	•3	••	0.	1.4		40.0	• 5	1.4	r.			127.0
1/5	SOUARE																																				125.0							
ITEM	WEIGHT	40.0	633.0	40.0	150.0	95.0	8.0	150.0	250.0	14.0	4.0	152.0	86.0	150.0	131.0	35.3.0	10.0	38.0	100.0	3.0	246.0	2.0	144.0	1.0	107.0	140.0	330.0	2148.0	52.0	0.06	300.0	1.0	1.0	1.0	1.0	28.0	2650.0	153.0	16.0	21.0	16.0	11.0	1.0	1932.0
ITEM	CUBE	2.0	53.3	7.7	15.0	4.9	3.6	14.0	15.0	2.7	3.8	8.2	9.9	2.0	0.6	55.0	·•	4.3	2.8	-:	K	· 5	2.1	-	6.3	5.0	18.0	119.0	1.5	6.9	20.0	-		0.	0.	1.4		20.0	5.	1.4	5.		0.	125.0
:TEM	SQUARE																																				125.0							

C5330 C5400 C5410

C3320

C5820

04740 04740 04740

TAM

C4820

C4840 C4980 C5080 C5110 C5700 C5930 C6030 C6130 C6220 C6280

C6370 C6388 C6410

C6420 C5430 C6510

C6345

C6650 C6655 C6658 C6684

C56495 000070 000100 00330 00330

H+MS. (MAG VH) MAN. FMF

CURTATE TZE FOR CLASS VII. CLASS II TAM ITFMS

tu	+ u
55	80
3489.49	3045.00
COURT OF PUBLISHED TZE 18 3440.449 CU FT CONSTRAINED TO 85.0 PCT UR 3204.00 CU FT	SQUARE OF PUBLISHED TVE IS 3045.00 SO FT CONSTRAINED TO 35.0 PCT OR 2589.00 SO FT

	ITEM	ITEM	ITEM	1/F	TZE	17E	TIF	CRIT	****	PEDUCED T	/F****	DEFIC-
TAM	SOUARE	CUBE	WEIGHT	SQUARE	CUBE	WE IGHT	410	710	710	OTY SOUARE CUBE	CUBF	TENCY
00740		35.8	710.0		35.9	710.0	-	~	:		3. 25	
02200		4.06	1390.0		2.06	1890.0	-	2	-1		4006	
93849	46.0		570.0	138.0		1710.0	m	4	3.	133.0		
008800	93.0		2710.0	186.0		5420.0	2	4	.2.	186.0		
20985	61.0		20000	122.0		1000.0	~	. 4	2.	122.0		
01030	176.0		13660.0	704.0		54640.0	4	4	3.	557.5		
01116	61.0		2400.0	498.0		19200.0	œ	4	.6	353.7		2.
98110	124.0	٠	5450.0	496.0		21840.0	4	4	3.	404.5		:
E2030		::	39.0			39.0	-	8	:		::	
	GRAND TOTALS	TOTALS		3046.0	3880.5	3880.5 255202.0 994	906		913.	2589-0 3298-0	3238.0	

TODAYS DATE 03/03/76
DR INDEX(SOUARE) = 84.85
OR INDEX(CUBE) = 92.15
OP INDEX(TOTAL I/E) = 91.41

#### H+MS. (MAG VH) MAW. FMF

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS
CUME OF PUBLISHED TZE IS JAMO.49 CU FT
CONSTRAINED TO 77.5 PCT OR 3007.00 CU FT

SQUARE OF PUBLISHED TZE IS 3045.00 SO FT CONSTRAINED TO 77.5 PCT OR 2351.00 SO FT

																																		NOTE:		Ilnit =		Constra						
	19 10 4							-																32.								-:-		1		-		_						
	CUBE			-		1.4			0.	1.5	2.4	7.7	3.8	c.	7.5	3.1		75.4	.7	0.	0.	α.	3.4	95.1	12.6	2.0		3.3	5.4	1.0	• 5	5.5	1.3	42.0	22.0	7.7	1.3	212.0	0.0	72.0	3.0	24.0	1.4	
	**************************************	123.2	54.0		74.2		44.4	287.4																																				
	******	:		:	1.	1.	:	. 2	1.	5.	5.	10.	5.	:	2.	15.	2.	٠.	10.	3.	:	. 5	2.	.96	2.	:	٠.		5.	2.	4.	1001	2.	10.	2.		128.	. 4	13.	:	:-	. 2 .	:	:
	CRIT	2	2	~	2	. 2	(1	2	-	-	-	-	-	-	1	1	-	-	1	-	1	-	-	-	-	-	-	-	1	-		-	-		-	1	1		-	2	-	-	-	-
!	1/E 01Y	-	-	-	-	-	-	3	-	ıc	2	10	S	-	2	15	2	2	10	3	-	2	S	128	2	-	2	-	S	2	4	120	2	10	~	1	128	٧	19	-		5	-	-
	WE I GHT	20709.0	2641.0	2.0	2680.0	82.0	3375.0	55500.0	1.0	20.0	30.0	30.0	35.0	1.0	120.0	75.0	0.9	1240.0	10.0	3.0	1.0	10.0	10.0	2043.0	160.0	50.0	10.0	40.0	20.0	20.0	200.0	6.0009	0.06	530.0	128.0	60.0	128.0	760.0	0.0	914.0	85.0	403.0	0.9	C + c.
	CUBE			-		1.4			0.	1.5	2.4	2.7	3.8	0.	3.7	3.1	£.	75.4		0.	0.	.8	3.4	126.7	12.6	5.0	2.	3.3	5.4	1.0	٠.	0.9	1.3	45.0	22.0	7.7	1.3	212.0	0.0	72.0	3.0	24.0	1.4	•
	SQUARE	156.0	54.0		16.0		0.96	405.0																																				
	WEIGHT	20700.0	2641.0	2.0	2680.0	32.0	3375.0	18500.0	1.0	4.0	0.9	3.0	7.0	1.0	0.09	5.0	3.0	620.0	1.0	1.0	1.0	2.0	2.0	16.0	80.0	20.0	2.0	40.0	10.0	10.0	20.0	20.0	45.0	53.0	64.0	0.09	0.1	190.0	0.0	918.0	95.0	204.0	6.0	5.0
	CUBE			:		1.4			0.	• 3	• 5	.3	8.	0.	1.9	• 5	•2	37.7	:	0.	0.	• 2	.7	1.0	6.3	2.0	:	3.3	1:1	.5	•	:		4.2	11.0	7.7	0.	53.0	0.0	72.0	3.0	12.0	1.4	2.
	SQUARE	150.0	54.0		76.0		0.96	135.0																																				
	TAM	90440	99469	90510	90630	92070	32550	0520	00023	22010	620.10	05000	C2050	62050	C2070	C2030	65100	C2120	C2160	62230	C2230	62220	C2.310	C3020	00000	04010	54020	04040	C4110	64140	54205	24208	06245	04250	C4.340	C4390	C4436	64450	C4555	64640	64450	09983	01900	04660

: M8914 aint = 85%

#### H+MS. (MAG VH) MAW. FMF

CURTATE TZE FOR CLASS VII. CLASS II TAM ITFWS

CONSTRAINED TO 77.5 PCT UR 3007.00 CU FT SQUARE OF PUBLISHED TZE IS 3046.00 SO FT CONSTRAINED TO 77.5 PCT OR 2361.00 SO FT

			3.	1							-
TAM SOUARE	CUBE	WEIGHT	SQUARE	CUBE	WEIGHT	OTY		710	SOUARE	CUBE	TENCY
0690	2.0	40.0		5.8	120.0	n	-	3.		5.8	
094 50	53.3	633.0		106.6	1266.0	2	1	2.		106.6	
06140	7.7	40.0		15.4	80.0	2	1	. 2		15.4	
C4820	15.0	150.0		30000	3000.0	50	-	15.		225.3	
C4870	6.4	85.0		25.5	340.0	4	1	4		25.5	
C4880	3.6	8.0		42.7	0.96	12	-	.12.		42.7	
C4480	14.0	150.0		140.0	1500.0	01		10.		140.0	
C5080	15.0	250.0		30.0	200.0	8	-	2.		20.0	
C5110	2.7	14.0		23.9	126.0	6	-	•		23.9	
C5200	3.8	4.0		181.4	192.0	48	-	32.		120.4	16.
C5320	8.2	162.0		220.3	4374.0	27	-	16.		133.3	11.
CS330	9.9	86.0		6.9	86.0	-	-	:-		9.9	
C5400	7.0	150.0		9.69	1500.0	10	-	10.		60.09	
C5410	0.6	131.0		0.6	131.0	-	-	:-		0.0	
C5820	25.0	353.0		100.0	1412.0	4	-	4		100.0	
C5830	6.	10.0		1.8	20.0	2		2.		1.8	
C5870	4.3	38.0		4.3	38.0	-	1	:		4.3	
C5930	2.8	100.0		11.0	400.0	*	-	4		11.0	
C6630	•	3.0			3.0	-	-	:		:	
C5130	6.3	246.0		6.3	245.0	-	-	:		6.3	
C6220	• •	2.0		1.5	15.0	٦	-	3.		1.5	
C6280	2.1	144.0		8.3	276.0	4	-	•		8.3	
C6.145	•	1.0		4.2	84.0	84	-	77.		3.8	7.
C6370	6.3	107.0		31.5	535.0	S	-	5.		31.5	
C6.388	5.9	140.0		70.4	1680.0	12	-	12.		70.4	
C6410	18.0	330.0		864.0	15840.0	48	-	26.		462.0	22.
C6420	119.0	2148.0		695.0	10740.0	r	-	3.		379.0	
C6490	1.5	62.0		4.5	186.0	n	-	3.		4.5	
C6510	6.9	0.06		6.9	0.06	-		:		0.1	
C6650	20.0	300.0		20.0	300.0	-	-	:		50.0	
C6655	•	1.0		2.3	45.0	45	-	41.		2.1	
C6658	:	1.0		r.	0.0	S	-	5.		. e.	
C6684	0.	1.0		9.	0.09	9	-	•09		٠.	
56995	•	1.0		0.	1.0	7		:-		0.	
	1.4	28.0		1.4	28.0	-	8	1.		1.4	
D00000 125.0		2650.0	125.0		2650.0	-	4	:	125.0		
00100	20.0	163.9		40.0	326.0	2	8	2.		40.0	
00380	• 5	16.0		.5	16.0	-	~	:		·.	
00340	1.4	21.0		1.4	21.0	-	2	:		1.4	
00400	\$.	16.0		• 5	16.0	-	2	:		۲.	
00420		11.0		.7	11.0	-	2				
00694	0.	0.1		0.	1.0	-	~	:		0.	
20124	0 000	1420.0		136.0	1.0 40.0						

#### CONSTRAINED TIE FOR UNIT MAGIC

#### H+MS. (MAG VH) MAW. FMF

CURTATE TZE FOR CLASS VII. CLASS 11 TAM ITEMS

FT	FT
3	3
3830.49	3007.00
15	ac
3/1	PCT
CUBE OF PUBLISHED I	CONSTRAINED TO 77.5

SQUAPE OF PUBLISHED TZE IS 3046.00 SO FT CONSTRAINED TO 77.5 PCT 08 2361.00 SO FT

TZE TZE CRIT ****PEDUCED TZE****  710.0 1 2 1. 35.8 1890.0 1 2 1. 90.7 5420.0 2 4 2. 171.4 1900.0 2 4 2. 171.4 1900.0 8 4 5. 321.0 39.0 1 2 1. 2 1. 184.0 24.0 2 1. 171.4 25450.0 4 4 3. 40.8.2 21840.0 6 4 4 3. 40.8.2 21840.0 7 1 2 1. 181.0			:	3.	:						I F NC Y	-31 azu
7.7. 0.00000000000000000000000000000000	2351.0 3007.0	:							40.7	9.55	CURT	//E***
7.7. 00 00 00 00 00 00 00 00 00 00 00 00 00	2351.0		367.7	321.0	4.38.2	118.7	171.4	124.0			SOUARE	REDUCED :
00000000	978.	:	3.	۶.	3.	2.	2.	3.	:	:	410	****
00000000		~	4	4	4	4	4	•	2	~		CPIT
77E 710.0 710.0 11890.0 1700.0 54640.0 19200.0 21840.0	466	-	•	00	4	2	~	3	-	-	914	1/6
	255202.0	30.0	21840.0	19200.0	54640.0	100000	5420.0	1710.0	1890.0	710.0	WEIGHT	TVE
17.E CUBE 35.8 90.7	3880.5	:							2.06	35.9	CUNE	1/5
17/E S3UARE 138.0 186.0 704.0 499.0	3046.0		406.0	483.0	704.0	122.0	186.0	138.0			SOUARE	1/1
710.0 1840.0 570.0 570.0 2710.0 13660.0 5460.0		39.0	2460.0	2400.0	13660.0	200.0	2710.0	820.0	18.30.0	710.0	WFIGHT	1154
17EM CUBE 35-3 90-7	DTALS	:							2.06	35.3	CUBE	LTEM
17EN SQUARE 93.0 61.0 124.0	GRAND TOT		124.0	61.0	176.0	61.0	93.0	46.0			SOUARE	1104
7AM 000740 000770 000780 01080 01100 01186												

TGDAYS DATE 03/02/76

GR INDEX(SQUARE) = 78-14

GR INDEX(CUBE) = 88-77

GR INDEX(TGTAL T/E) = 87-70

#### H+MS. (MAG VH) MAW. FMF

CURTATE TZE FUR CLASS VII. CLASS II TAM ITEMS

CUHE OF PUBLISHED TZE IS 3880-49 CU FT CONSTRAINED TO 62-5 PCT OR 2425-00 CU FT

SQUARE OF PURLISHED TVF IS 3045.00 SQ FT CONSTRAINED TO 62.5 PCT OR 1904.00 SO FT

DEFIC- IENCY							•																41.								17.		NOTE.		Init - Men	חוור - נוספו	1. Constraint						
T/Esses C			:		1.4			0.	1.5	5.4	7.4	3.8	0.	3.7	3.1	F.	75.4	1:		0.	6.	3.4	85.4	12.6	2.0	٠.	3.3	5.4	1.0		5.1	1.3	42.0	22.0	7.7	1.3	182.4	0.0	72.0	3.0	24.0	1.4	
*****REDUCED T	82.9	44.0		25.6		64.5	219.4																																				
710	:	:	:	:	••	:		:		2.	10.	5.	:	. 2.	15.	2.	5.	10.	3.	:	5.	5.	87.	. 2	:	2.	:	·	2.		103.	2.	10.	2.	:	128.	3.	. 18.	:		2.	:-	:
CRIT	8	~	~	~	2	2	~	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2	-	-	-	••
17E	-	-	-	-	-	-	3	-	y,	S	10	S	-	~	1.5	8	2	01	3	-	ດ	S	128	~	-	cı	-	r	2	4	120	2	10	~	-	128	4	18	-	-	2	-	
T/E WEIGHT	20700.0	2641.0	2.0	2680.0	85.0	3375.0	25500.0	1.0	20.0	30.0	30.0	35.0	1.0	120.0	75.0	0.9	1240.0	10.0	3.0	1.0	10.0	10.0	2043.0	160.0	20.0	10.0	40.0	20.0	20.0	200.0	600000	0.06	530.0	128.0	60.09	128.0	760.0	0.0	918.0	85.0	403.0	0.0	3.0
TVE			•		1.4			••	1.5	2.4	2.7	3.8	0.	3.7	3.1		75.4		0.	••	€.	3.4	126.7	12.6	2.0	.2	3.3	5.4	1.0		0.9	1.3	45.0	22.0	7.7	1.3	212.0	0.0	72.0	3.0	54.0	1.4	.2
SQUARE	156.0	64.0		76.0		0.96	405.0																				A Company																
ITEM WEIGHT	20700.0	2641.0	5.0	2580.0	82.0	3375.0	18200.0	1.0	0.4	0.9	3.0	7.0	1.0	0.09	5.0	3.0	620.0	1.0	1.0	1.0	2.0	2.0		80.0	20.0	2.0	0.04	10.0	10.0	20.0	20.0	45.0	53.0	0.49	0.09	. 1.0	190.0	0.0	618.0	85.0	204.0	0.9	5.0
11EM CUBE			:		1.4			••	.3	· .	€.	89.	••	1.9	.2	•5	37.7	:	•	••	2.		1.0	6.3	2.0	-	3.3	:	• •	7.	-		4.2	11.0	7.7	•	53.0	0.0	72.0	3.0	12.0	1.4	• 5
SQUARE	156.0	54.0		70.0		0.96	135.0																																				
NA.	30440	30465	90510	80630	92070	82550	82550	00020	C2310	C2030	C2040	C2050	C2060	C2070	C2080	C2100	C2120	C2160	C2200	C2230	C2250	C2310	C3020	C4000	C4010	C4020	C4040	C4110	C4140	C4205	C4208	C4230	C4250	C4 340	C4 390	C4436	C4450	C4555	04940	C4450	C4660	C4570	05.463

CRIMIC IN CLASS VIII CLASS II IAM IIIAS	30.49 CU FT 25.00 CU FT	3046.00 SO FT
VIII	CUBE OF PUBLISHED TZE 1S 3830.49 CU FT CONSTRAINED TO 62.5 PCT OR 2425.00 CU FT	
E FUN CLASS	PUBLISHED	SQUARE OF PUBLISHED T/E 1S CONSTRAINED TO 62.5 PCT OR
	CONSTRAIL	SQUARE OF

** DEFIC-	ш	5.8	9.	.4	.0 0.		.7	0.	0.		.8 21.		4.	٧.	0.	0.	.8	.3	0.		6.3	1.5	P.3	3.6 12.	٠.	••		.7 5.		6.4	0.	.2 0.	r.	4.	0.	. 4.		0.	٧.	4.	.5	.7	0	
**** 0.		· C	106.6	15.4	180.0	24.5	42.7	140.0	30.0	23.9	103.8	109.7	9.9	69.6	0.0	100.0	1.8	4	11.0		9	-	a	m	31.5	70.4	335.4	400		·	20.0	-				-	97.5	40.0		-				
*PEDUCFD	SOUARE																																				.6							
****	710	3.	2.	2.	12.	4	12.	10.	2.	•	27.	13.	-	10.	:	. 4	2.	-	•	1.	:	3.	*	72.	5.	12.	19.	0	3.	:	-	38.	2.	.09	:	:	-	2.	-	<i>-</i>	:	-	:	
CRIT		-	-	-	-	-	-	-	-	-	-	1	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	8	4	2	2	2	2	2	2	
TVE	0TY	n	2	8	20	4	12	10	8	6	48	27	-	10	-	4	2	-	4	-	-	9	4	84	2	12	48	S	3	-	-	45	2	9	-	-	-	2	-	1	-	-	-	
1/5	WE IGHT	120.0	1266.0	80.0	3000.0	340.0	0.96	1500.0	200.0	126.0	192.0	4374.0	86.0	1500.0	131.0	1412.0	20.0	38.0	400.0	3.0	246.0	15.0	576.0	84.0	535.0	1680.0	15840.0	10740.0	186.0	0.06	300.0	45.0	2.0	0.09	1.0	28.0	2650.0	326.0	16.0	21.0	16.0	11.0	1.0	
176	CUBE	5.8	106.6	15.4	300.0	25.5	42.7	140.0	30.0	23.9	181.4	220.3	9.9	9.69	0.6	100.0	1.8	4.3	11.0	:	6.3	1.5	8.3	4.2	31.5	4.07	864.0	295.0	4.5	6.9	20.0	2.3	.3	9.	0.	1.4		40.0	5.	1.4	6.		0.	
1/1	SQUARE																																				125.0							
ITEM	WEIGHT	40.0	633.0	40.0	150.0	85.0	8.0	150.0	250.0	14.0	4.0	162.0	86.0	150.0	131.0	353.0	10.0	38.0	100.0	3.0	246.0	2.0	144.0	1.0	107.0	140.0	330.0	2148.0	62.0	0.06	300.0	1.0	0.1	1.0	1.0	28.0	5650.0	163.0	16.0	21.0	16.0	11.0	1.0	
ITEM	CUBE	2.0	53.3	7.7	15.0	4.9	3.6	14.0	15.0	2.7	3.8	8.2	9.9	7.0	0.6	25.0	6.	4.3	2.8		6.3	• •	2.1		6.3	5.9	18.0	119.0	1.5	6.9	20.0	:	:	0.	0.	1.4		20.0	.5	1.4	• 5	.7	0.	0 30
ITEM	SGUAPE																																				125.0							
	TAM	C4590	C4 760	C4790	C4820	54870	C4880	C4480	C5080	C5110	C5200	C5320	C5330	65400	C5410	C5420	C5430	C5870	C2630	65030	C6130	C6220	C6280	C6345	64379	C6238	56410	C6420	C6430	C6510	05990	68982	66658	C6684	56993	02000	00000	00100	00330	003390	00400	02450	00691	20100

#### H+MS. (MAG VH) MAW, FMF

# CURTATE TZE FUR CLASS VII. CLASS II TAM ITEMS

FT	4	
S	5	
3880.49 CU FT	2425.00 CU FT	
	CR	
TIE	PCT	
CHED	62 . PCT UR	
CURE OF PUBLISHED TIE IS	FO TO	
J.C	VIV	
CURE	CONSTRAÍNED TO	

FT	FT
80	80
3046.00	1904.00
15	OR
1/E	PCT
ISHED	TO 62.5
OF PUR	AINED
SQUARE	CONSTRAINED

	OTY SOUARE CUBE TENCY	35.8	4006		1.8	100.8	3.4	1.4	5.9	=	
******	OTY SOUA	:	:			2. 10				:	
CRIT		8	~	4	4	4	4	4	•	~	
T/E	410	-	-	3	~	8	*	80	4	-	
TZE	WEIGHT	710.0	1890.0	1710.0	5420.0	1000.0	54640.0	19200.0	21840.0	39.0	
1/E	CUBE	35.8	2.06							:	
176	SOUARE			138.0	186.0	122.0	704.0	488.0	496.0		
ITEM	WEIGHT	710.0	1830.0	570.0	2710.0	20000	13660.0	2400.0	5460.0	39.0	
ITEN	CUBE	35.8	1.00							=	
ITEN	SOUARE			0.94	93.0	61.0	176.0	61.0	124.0		
	144	00740	02100	00440	06800	00485	01030	09110	98116	E2030	

TODAYS DATE 03/02/76

OR INDEX(SQUARE) = 64.94

OR INDEX(CUBE) = 94.24

OR INDEX(TOTAL T/E) = 82.29

## MARINE AIR TRAFFIC CONTROL UNIT. MAG

CUBE OF PUBLISHED TVE IS 873.09 CU FT CONSTRAINED TO 85.0 PCT OR 742.00 CU FT SQUARE OF PUBLISHED TVE IS 772.00 SO FT CONSTRAINED TO 85.0 PCT OR 656.00 SO FT

	•														•																						Ε:		Unit = M8821		Constraint = 90%			
DEFIC	IONCA																																				NOTE:		Uni		Con			
DUCFD T/F***		0.1	63.0	-	2.4	1.1	3.8	1.9	4.	-5		6.	α.	3.4	61.1	2.0	2.2	.5	•		11.0	.2	15.0	106.6	c.	7.7	15.0	12.7	10.7	62.8	3.0	7.7	8.0	30.0	6.9	20.00	4.3		۲.	6.3	0.4	7.2	144.0	60.3
******	9 710	:	-	-	5.	5.	5.	:	2.	:-	10.	:	5.	٠,	62.	•	. 2.	:	1.	12.	:	24.	:	2.	*	:	-1	2.	3.	:	:	:	3.	.6	-:	3.	:	:	12.	:	:		3.	:
CRIT		4	4	~	-		-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	1	-	-	1	-	-	-	7	-	-	1	-	-		1	1	-	-	1	1	1
1/5	410	-	-	-	S	S	r	-	2	-	01	-	5	S	7.3	-	2	-	-	12	-	24	-	2	4	-	-	2	3	-	7	-	3	o	-	3	-	-	12	-	-	-	α	~
1/E	WE TGHT	42.0	145.0	2.0	30.0	15.0	35.0	0.09	10.0	3.0	10.0	1.0	10.0	10.0	1168.0	20.0	20.0	10.0	20.0	0.009	64.0	24.0	204.0	1266.0	4.0	40.0	150.0	170.0	54.0	0.009	0.50	127.0	45.0	32.0	152.0	450.0	38.0	5.0	12.0	107.0	140.0	257.0	2640.0	2140.0
TZE	CURE	1.0	53.0	:	2.4	1.3	3.8	1.3	4.	.2	1.	0.		3.4	72.3	2.0	2.2	5.	7	9.	11.0		12.0	106.6	c.	7.7	15.0	12.7	10.7	124.0	3.9	2.7	8.0	30.2	8.2	50.0	4.3	5.	٠.	6.3	5.9	7.2	144.0	:17.0
TVF	SOUARE																																											
ITEM	WEIGHT	42.0	145.0	2.0	6.0	3.0	7.0	60.0	5.0	3.0	1.0	1.0	2.0	5.0	16.0	20.0	10.0	10.0	20.0	20.0	64.0	0:1	204.0	633.0	1.0	0.04	150.0	85.0	8.0	0.009	0.56	127.0	14.0	4.0	152.0	150.0	38.0	5.0	1.0	107.0	140.0	257.0	330.0	2144.3
ITEM	CUBE	1.0	53.0			£.	æ.	1.9	.2	• 5		0.	.2		1.0	2.0	1:1	.5	~	:	11.0	0.	12.0	53.3	••	7.7	15.0	6.4	3.6	124.0	3.9	2.7	2.7	3.8	8.2	7.0	4.3	••	-:	6.3	6.5	7.2	19.0	0.611
ITEM	SOUARE																																											
	144	AC912	42510	90510	C2030	C2040	C2050	02023	C2030	C2100	62160	62230	02220	CZ 310	C3050	01000	01110	CALAD	C4205	C4208	C4340	C4436	09940	092 43	C4 765	064 40	C4820	C4870	C4480	00643	09640	C2100	C2110	C5200	C5350	C2400	65870	02293	66345	C6370	66 339	60100	24	01833

CONSTRAINED THE FOR UNIT MARRI

## MARINE AIR TRAFFIC CONTROL UNIT. MAG

CUSTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

U FT	U FT	1 4 0	TT O
873.09 CU FT	742.00 CU FT	772.00 SO FT	ASSESSO SO FT
CURE OF PUBLISHED TIE IS	CONSTRAINED TO 85.0 PCT OR	SOUARE OF PUBLISHED TIE IS	CONSTRAINED TO AS O DCT OR

	ITEN	ITEM	MELI	1/F	1/6	1/F	1/5	CRIT	****		1/F ****	DEFIC
TAM	SOUARE	CURE	WEIGHT	SOUARE	CUBE	WEIGHT	710		017	SOUASE	CUBE	IFNCY
C6430		1.5	62.0		4.5	186.0	£	•	3.		4.5	
56513		6.9	0.06		6.9	0.00	-		:		6.4	
06553		31.0	0.009		31.0	6.009	-	-	-:		31.0	
55493		-:	1.0		••	1.0	-	-			:	
C6684		•	0.1		:	10.0	01	-	10.		••	
20070		1.4	28.0		1.4	29.0	-	8	:		1.4	
00100		20.0	163.0		20.0	163.0	-	8	:		20.0	
00800	46.0		570.0	46.0		570.0	-	8	:	44.3		
09800	0.96		2750.0	0.96		2750.0	-	2	:	83.0		
06800	93.0		2710.0	93.0		2710.0	-	8	:	80.3		
01030	176.0		13660.0	352.0		27320.0	~	2	2.	267.3		
011160	61.0		2400.0	61.0		2400.0	-	8	:	54.5		
01186	124.0		5460.0	124.0		5460.0	-	89	:	124.0		
0600B		4.	7.0		1.2	21.0	٣	-	3.		1.2	
	GRAND TO	OTALS		772.0	873.1	53381.0	244		231.	656.0	742.0	

TODAYS DATE 03/03/76
OR INDEX(SQUARE) = 91.43
OR INDEX(CUBE) = 95.00
OR INDEX(TOTAL T/E) = 94.73

CCNSTRAINED TIE FOR UNIT MBB21

MARINE AIR TRAFFIC CONTROL UNIT, MAS

13		
CURTATE TIE FOR CLASS VIII. CLASS II TAM ITEMS	873.09 CU FT	772.00 SQ FT 598.00 SQ FT
-	77	CC
Σ	55	S
-	000	00
-	• •	• •
-	7.7	72
55	æ &	- 6
LA		
C	50	SOR
-		
-	CONST OF OUBLISHED TZE 15 CONSTRAINED TO 77.5 PCT 09	SQUARE OF PUBLISHED TZE IS CONSTRAINED TO 77.5 PCT OR
	- 10	- 10
ć	c·	0 .
2	. IL	H
0	- 0	- 0
Č	B -	9 -
1	200	D O
4	Z	Z
-	Ç 4	CK
10	IJ L	W -
4	5 Z	A Z
a	0 0	000
2		S

																						1																							
DFFIC-	AUNUL														17.															1.				NOTE:		Unit = M8821		Constraint = 85%						:	
1/E****	CURE	1.0	53.0	-	2.4	1.3	3.6	1.9	4.	.2		· ·	α.	3.4	55.5	2.0	2.2			9.	11.0	.2	12.0	106.6	0.	7.7	15.0	12.7	10.7	32.5	3.9	2.7	A.0	30.5	8.2	50.0	4.3	٠.	••	6.3	0.0	7.2	144.0	31.2	
**BEDUCED	SOJACE																																												
*	919	-	-	-	5.	5.	5	-	2		10.		5.	'n	-95	-	2.	-	-	12.		24.	-	2	4	-	-	2	3	•	-	-	'n	8	-	'n	-	-	12.	-	-	-	00	c	
CRIT		4	4	8	1	-			-		1			1	1	1	1	-	-		-			-	-		1	-	~		-	-	-	-	-		-		-	1				-	
1/E	017	-	-	-	2	S	S	-	8	-	10	-	S	S	73	-	8	-	-	12	-	24	-	8	4	-	-	8	m	-	-	-	•	80	-	n	-	-	12	-	-	-	8	-	
1/6	WEIGHT	42.0	145.0	2.0	30.0	15.0	35.0	0.09	10.0	3.0	10.0	1.0	10.0	10.0	1168.0	20.0	20.0	10.0	20.0	0.009	64.0	24.0	204.0	1266.0	4.0	0.04	150.0	170.0	24.0	0.009	0.56	127.0	45.0	32.0	162.0	450.0	38.0	2.0	12.0	107.0	140.0	257.0	2640.0	2143.0	
1/E	COUR	1.0	53.0	:	5.4	1.3	3.8	1.9	4.	.2		0.		3.4	72.3	2.0	2.2	• 5	1.	9.	11.0	.2	12.0	106.6	0.	7.7	15.0	12.7	10.7	124.0	3.9	2.1	8.0	30.2	8.2	65000	4.3	• 5	9.	6.3	5.9	7.2	144.0	110.0	
1/6	SQUARE																																												
ITEM	WE IGHT	42.0	145.0	2.0	0.9	3.0	7.0	0.09	2.0	3.0	1.0	1.0	2.0	2.0	16.0	20.0	10.0	10.0	20.0	20.0	64.0	1.0	204.0	633.0	1.0	40.0	150.0	85.0	8.0	0.009	0.56	127.0	14.0	4.0	162.0	150.0	34.0	2.0	1.0	107.0	140.0	257.0	330.0	2148.0	
LTEM	CUBE	1.0	53.0	-		£.	. 8	1.9	• 5	• 5	••	••	• 5		1.0	2.0	::	• 5	:		11.0	0.	12.0	53.3	•	7.7	15.0	6.4	3.6	124.0	3.9	2.7	2.1	3.8	8.2	7.0	4.3	.5	-	6.3	2.0	7.2	18.0	110.0	
ITEN	SOUARE																																												
		A0912	A2510	80510	05020	C2040	C2050	C2070	C2080	C2100	C2150	52230	C2250	C2310	C3020	01000	01143	C4140	C4205	C4208	C4340	C4436	09940	C4750	64 765	C4 790	C4820	C4870	C4880	00643	C4 960	C2100	62110	C2500	CS320	C5400	C5870	C6220	66.345	C6370	C6 188	00890	01000	C1420	

CONSTRAINED TIE FOR UNIT MR921

## MARINE AIR TRAFFIC CONTROL UNIT, MAG

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

J FT		D FT	D FT
0	5	3, 2	S
873.09 CU FT	0.	772.00 'SO FT	598.00 SO FT
15	ž	1.5	OR.
CUBE OF PUBLISHED TVE IS	CONSTRAINED TO COS PCT OR	SQUARE OF PUBLISHED TIE 15	MAINED TO 77.5 PCT
CUBE	CONSTR	SQUARE	CCNSTR

DFF1C.	IENCY											-				
/F****	CUBE	4.8	6.9	31.0	:	:	1.4	20.0							1.2	598-0 A77-0
PEDUCED 1	OTY SOJARE								43.4	76.5	74.8	224.9	54.3	124.0		0.802
****	410	3.	-1	:		10.	:-	1.	1.		:	:	:	:	3.	224.
CRIT		-	-	-	-	-	2	2	2	2	2	2	2	80	-	
T/E CRIT	OTY	6	-		-		-	-	-	-	-	8	-	-	6	244
TZE	WE IGHT	185.0	0.06	0.009	1.0	10.0	28.0	163.0	570.0	2750.0	2710.0	27320.0	2400.0	5460.0	21.0	53381.0 244
1/E	CUBE	4.5	6.9	31.0	-	•	1.4	20.0							1.2	873.1
TZE	SQUARE								46.0	0.96	93.0	352.0	61.0	124.0		772.0
ITEM	WEIGHT	62.0	0.06	0.009	1.0	1.0	28.0	163.0	570.0	2750.0	2710.0	13650.0	2400.0	5460.0	7.0	
ITEM	CUBE	1.5	6.9	31.0	•	••	1.4	20.0							4.	OTALS
TEM	SCUARE								46.0	0.96	93.0	176.0	61.0	124.0		GRAND TOTALS
	TAM	06490	01593	06590	C6655	C6584	02000	00100	00800	09800	90880	01030	01110	98110	E0090	

TODAYS DATE 03/02/76
UR INDEX(SQUARE) = 87.14
UR INDEX(CUBE) = 92.53
UR INDEX(TOTAL T/E) = 92.12

## MARINE AIR TRAFFIC CONTROL UNIT, MAG

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS CURE OF PUBLISHED TZE IS 873.09 CU FT

FF	11
3 3	50
546.00 CU FT	772.00 SQ FT
CORE OF PUBLISHED TZE IS CONSTRAINED TO 62.5 PCT OR	SQUARE OF PUBLISHED TZE IS CONSTRAINED TO 62.6 PCT OR

, DEFE	1 P N O V														24.									2.							NOTE.	MOIE.	Hait wood	Unit = M8821	Constraint = 75%									•	
1/F****	CUBE	1.0	53.0	:	2.4	1.3	3.0	1.0	4.		.,	0.		3.4	40.8	2.0	2.2	٠.	:	٧.	11.0		12.0	14.0	0.	7.7	15.0	12.7	10.7	16.3	3.9	2.7	8.0	30.2	8.2	50.0	4.3		٠.	F. 3	0.5	7.2	144.0	15.7	
*****																																													
****	717	:	:	-	5.	. S.	5.		2.	1:	10.	1:	5.	5.	40.	1.	2.	1:		12.	:	24.	1:	• 0	4	:	•	2.	3.	0	:	:	3.	· œ	:	3.	:	1.	12.	-	:	1:	8		
CRIT		4	4	2	-	1	-	1	1	-	-	-	-	-	-	1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			-	-	-	
1/5	710	-	-	-	c	S	2	-	2	-	10	-	c	S	7.3	-	2	-	-	12	-	24	-	2	4	-	-	2	6		-	-	m	8	-	n	-	-	12	-	-	-	œ	-	
17.5	WE IGHT	42.0	145.0	2.0	30.0	15.0	35.0	0.09	10.0	3.0	10.0	1.0	10.0	10.0	1168.0	20.0	20.0	10.0	20.0	60000	64.0	24.0	204.0	1266.0	4.0	40.0	150.0	170.0	24.0	0.009	0.56	127.0	42.0	32.0	162.0	450.0	38.0	2.0	12.0	107.0	140.0	257.0	2640.0	2:48.0	
1/6	CUBE	1.0	53.0	•	5.4	1.3	3.8	1.9	•	.2		0.	8.	3.4	72.3	2.0	2.2	5.	•	9.	11.0	.2	12.0	106.6	0.	7.7	15.0	12.7	10.7	124.0	3.9	2.7	8.0	30.2	8.2	50.9	4.3	• 5	9.	6.3	6.5	7.2	144.0	113.0	
17.6	SOUARE																																												
ITEM	WEIGHT	42.0	145.0	5.0	0.9	3.0	7.0	0.09	2.0	3.0	1.0	1.0	2.0	2.0	16.0	20.0	10.0	10.0	20.0	20.0	64.0	1.0	204.0	633.0	1.0	40.0	150.0	85.0	8.0	0.009	0.56	127.0	14.0	4.0	162.0	150.0	38.0	2.0	1.0	107.0	140.0	257.0	330.0	2144.0	
ITEM	CUBE	0.1	53.0		· •	.3	.8	1.9	• 5	•5	-	0.	• 5		1.0	2.0	1:1	• 5	-	-	11.0	0.	15.0	53.3	0.	7.7	15.0	6.4	3.6	124.0	3.9	2.1	2.7	3.8	8.2	7.0	4.3	• 5	-:	6.3	5.9	7.2	18.0	113.0	
1 TEN	SOUNAE																																												
	TAN	2160A	A2510	01509	52030	52040	05020	12070	CZCHO	65100	C2160	C2230	C2250	C2310	C3050	01040	C4110	C4140	C4205	C4208	C4340	C4436	C4660	C4760	C4766	04740	C4 820	C4870	C4880	00640	C4 360	C2100	C3110	C2500	C5320	C2400	C5870	C6220	66345	C6370	C6388	06290	C6410	07410	

CONSTRAINED TZE FOR UNIT 48921

## MARINE AIR TRAFFIC CONTROL UNIT. MAG

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

11 11	1 1
55	50
873.09 CU FT	772.00 SQ FT
5 9	72.
Ø, T	- 4
20	80
-	= _
CUBE OF PUBLISHED TVE IS	PC PC
_ 0	. 0
HED 62.	HE 0
20	1 5
# F	સ ►
P.	D C C
OF A	OF
F	W F
D Z	₹ Z
0 3	SOUARE OF PUBLISHED TZE IS CONSTRAINED TO 62.6 PCT OR

ITEM	ITEM	ITEN	1/E	1/5	1/E	1/E	CRIT	****	*********	1/E***	DEFIC-
GUARE	CUBE	WEIGHT	SQUARE	CUBE	WE IGHT	710		710	SQUARE	CUME	IENCY
	1.5	62.0		4.5	186.0	<b>E</b>	-	3.		A.5	
	6.9	0.06		6.9	0.06	-	1	:		6.9	
	31.0	0.009		31.0	0.009	-		:		31.0	
	:	1.0		-:	1.0	-	-			:	
	0.	1.0			10.0	10	1	10.		:	
	1.4	28.0		1.4	28.0	-	2			1.4	
	20.0	163.0		20.0	163.0	-	8	:		20.0	
46.0		570.0	46.0		570.0	-	2	:	36.5		
0.96		2750.0	0.96		2750.0	-	8	:	58.4		
93.0		2710.0	03.0		2710.0	-	~	1.	57.4		
176.0		13660.0	352.0		27320.0	8	8	:	162.4		:
61.0		2400.0	61.0		2400.0	-	~	:	44.3		
124.0		2460.0	124.0		5460.0	-	60	1.	124.0		
	•	7.0		1.2	21.0	n	-	3.		1.2	
CRAND T	OTAL S		772.0	1.174	0.19552	440		• • •		0 545	

TODAYS DATE 03/02/76
OR INDEX(SQUARE) = 76.68
OR INDEX(CUBE) = 88.94
OR INDEX(TOTAL T/E) = 88.02

WAPINE HELICOPTER ATTACK SQUADSON(HMA)

CURTAIN TZE NON CLASS VIII. CLASS II TAM ITMAS

CONSTRAINED TO 95.0 PCT OP 1405.00 CU FT CONSTRAINED TO 95.0 PCT OP 1405.00 CU FT SQUARE OF PUBLISHED TZE IS 2245.00 SO FT CONSTRAINED TO 95.0 PCT OR 2133.00 SO FT

9cF1C-	>0241																						17.			30.		Nome	NOIE:		Unit = M8970	Constraint = 90%												
****	COURT	7.0	0.:		1.0	13.0	173.0	26.5	5.1.		0.	1.5	2.4	2.7	3.8	0.	3.7	• 3	15.4		0.	0.	25.5	.8	3.4	97.5	12.6	2.0	•5	3.3	4.3	1.0	4.2	22.0	7.7	6.	1.4	.2	0.0	7.7	51.0	30.0	10.6	11.3
*************************	SOUARE			16.0																																								
:	410	:	-	-	:	-	:	23.	-	-	:	5.	ď	10.	· v	-	5.	5.	2.	.01	٠,	-	87.	٠,	5.	98.		-	2.	-	*	2.	:	2.	:	93.	-	-	-	-	8	5.		
CRIT		~	2	2	2	2	2	2	2	2	1	-		-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1/E	710		-	-	-	-	-	30	-	-	-	ıc.	2	10	S	-	01	2	2	10	2	-	104	S	2	128	2	-	~	-	4	2	-	2	-	63	-	-	-	-	œ	2	•	•
1/E	WE I GHT	182.0	28.0	2680.0	116.0	355.0	0.096	2520.0	145.0	82.0	1.0	20.0	30.0	30.0	35.0	1.0	120.0	6.0	1240.0	10.0	2.0	1.0	728.0	10.0	10.0	2048.0	160.0	50.0	10.0	40.0	40.0	50.0	53.0	128.0	60.09	03.0	6.9	2.0	0.04	40.0	680.0	6.000	55.0	12.0
1/5	CUBE	7.0	1.0		1.0	13.0	173.0	74.4	5.1	£.	0.	1.5	2.4	2.7	3.8	0.	3.7	•3	75.4	.7	c.	0.	30.2	. 3	3.4	126.7	12.5	5.0		3.3	4.3	1.0	4.2	22.0	7.7		1.4	• 5	2.0	7.7	51.0	30.0	10.6	11.3
TVE	SQUARE			76.0																																								
N S L I	WEIGHT	132.0	28.0	2680.0	116.0	355.0	0.056	84.0	145.0	82.0	1.0	4.0	0.9	3.0	7.0	1.0	0.09	3.0	620.0	1.0	1.0	1.0	7.0	2.0	2.0	16.0	80.0	20.0	2.0	40.0	10.0	10.0	53.0	64.0	0.09	1.0	6.0	2.0	40.0	40.0	95.0	250.0		0.0
1 154	CUBE	7.0	1.0		1.0	13.0	173.0	2.5	5.1.	8.	0.	.3	5.	•3	. 8	0.	1.9	• 5	37.7	-:	0.	0.	r.	• 5		1.0	6.3	2.0	-	3.3	1:1	• 5	4.2	11.0	7.7	0.	1.4	.2	5.0	7.7	6.4	15.0	2.7	o. r.
ITEN	SOUARE			76.0																																								
	4 4 4	A0970	A2480	30530	11540	31650	06916	92030	01220	32240	65065	C2010	C2030	02040	C2050	62060	02020	C2100	C2120	C2160	C2200	\$22.30	C2235	C2250	C2310	C3020	C4000	C4010	C4020	C4040	C4110	C4140	04250	C4340	C4390	C4136	C4670	C4460	C4690	062 00	C4870	08050	02110	00.650

## MARINE HELICOPTER ATTACK SQUADRON(HWA)

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

11	-		1
3	00	50	50
1478.50	1405.00	2245.00	2133.00
CUSE OF PUBLISHED T/F 15 1478.50 CU FT	CJNSTRAINED TO 95.0 PCT UR 1405.00 CU FT	SQUARE OF PUBLISHED T/F IS 2245.00 SQ FT	CONSTRAINED TO 95.0 PCT OR 2133.00 SO FT

TODAYS DATE 03/03/76
OR INDEX(SOURE) = 95.82
OR INDEX(CUBE) = 89.98
OR INDEX(CUBE) = 60.93

# MARINE MELICOPTER ATTACK SQUADRON(HMA)

CURTATE T/E FOR CLASS VII. CLASS II TAM ITEMS CUBE OF PUBLISHED TZE 1S 1478-50 CU FT CONSTRAINED TO 92-5 PCT OR 1369-00 CU FT 2245.00 SO FT CONSTRAINED TO 92.5 PCT OR

																						1																	85%					
																																					8970	•	nt =					
																																			 		Thit = M8970		Constraint					
	. >																																		NOTE:		Ilni		Con					
31330	12.50							0															22.			37.																		
	CUBE	7.0	1.0		1.0	13.0	173.0	51.5	5.1	80.	c.	1.5	2.4	2.7	3.5	0.	3.7	۳.	75.6	1.	c.	0.	23.7		3.4	80.0	12.6	2.0	2.	3.3	4.3	1.0	4.2	22.0	7.7	0.	1.4		2.0	7.7	51.0	30.0	10.6	11.3
0401040****				76.0																																								
****	710		:-	1.	:	:	:	21.		:	::	5.	5.	10.	5.	:	2.	2.	2.	10.	2.	-:	82.	5.	5.	91.	2.	1:	2.	:	•	5.	:	2.	:-	93.	:	1:	:	:-	8.	2.	٠,	÷
7197		2	N	8	2	~	0	2	2	0		-	1	1	1	1	-	1	1	1	1		1			1	-		-	-	-	1	-		1		1	1	1	1	1	-		-
1/5	017	-	-	-	-	-	-	30	-	-	-	2	r	10	5	-	~	2	8	01	2	-	104	S	2	128	2	-	2	-	4	2	-	2	-	66	-	-	-	-	60	2	4	۳.
1/5	WEIGHT	182.0	28.0	2680.0	116.0	355.0	0.096	2520.0	145.0	82.0	1.0	20.0	30.0	30.0	35.0	1.0	120.0	0.9	1240.0	10.0	2.0	1.0	728.0	10.0	10.0	2048.0	160.0	20.0	10.0	40.0	40.0	20.0	53.0	128.0	0.09	93.0	0.9	2.0	0.00	40.0	680.0	0.005	84.0	12.0
1/5	CUBE	7.0	1.0		1.0	13.0	173.0	74.4	5.1	8.	0.	1.5	2.4	2.1	3.8	0.	3.7	.3	75.4	.7	0.	0.	30.2	. 9	3.4	126.7	12.6	2.0	.2	3.3	4.3	1.0	4.2	22.0	7.7	0.	1.4	• 5	2.0	7.7	51.0	30.0	10.6	11.3
TVE	SQUARE			16.0																																								
ITEM	WEIGHT	182.0	28.0	2680.0	116.0	355.0	0.096	84.0	145.0	82.0	1.0	4.0	0.9	3.0	7.0	1.0	0.09	3.0	620.0	1.0	1.0	1.0	7.0	2.0	5.0	16.0	80.0	20.0	2.0	40.0	10.0	10.0	53.0	64.0	0.09	1.0	0.9	2.0	40.0	40.0	85.0	250.0	14.0	۷٠٥
ITEM	CUBE	7.0	1.0		1.0	13.0	173.0	2.5	5.1	. 8	0.	•3	• 5	£.	8.	•	1.9	• 5	37.7	:	0.	0.	•3	• 5		0	6.3	2.0	•	3.3	-:-	• • •	4.5	11.0	7.7	0.	1.4	.2	5.0	7.7	4.0	15.0	2.7	3.0
TEN	SQUARE			16.0																																								
	TAM	A0370	A2480	69630	91510	81650	91690	82030	82210	92240	C2000	01023	02030	C2040	05020	55000	02020	00123	C2120	09173	C2200	C2230	C2235	C2250	C2310	C3020	00040	01040	C4020	C4040	C4110	64140	C4250	C4340	C4390	C4436	02900	C4680	00950	C4 796	C4870	CS080 .	C.110	66290

# MARINE HELICOPTER ATTACK SQUADRON(HMA)

. CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUBE OF PUBLISHED T/E IS 1478-60 CU FT CONSTRAINED TO 92-5 PCT OR 1368-00 CU FT

SQUARE OF PUBLISHED T/E IS 2245.00 SO FT CONSTRAINED TO 92.5 PCT OR 2077.00 SO FT

DEF 1C-	15 NCY											2.																					:				
T/E***	CUBE	4.0.8	50.0	0.6	٠.	4.3	5.5	1.0	11.0	20.4	111.7	243.5	4.5	20.0	3.2	· •	0.	1.4		20.0	.5	1.4	• 5	ç.		125.0	35.8	.3	4006						0.	:	2077.0 1368.0
**********	SOUARE																		125.0											46.0	273.1	733.6	597.1	226.2			2077.0
*****	410	5.	3.	:	8	:	2.	2.		8.	2.	14.	3.		:	53.	:	1:	:	:	:	:		:	:		:	1:	:	1:	3.	3.	3.	. 4	:	:	521.
CRIT		-	-	-	-						-	-	-	-	-	-	-	2	2	2	~	2	2	2	2	2	2	2	2	2	2	4	~	2	-	2	
1/E	710	S		-	80	-	2	2	-	80	8	16	E	-	-	53	-	-	-	-	-	7	-	-	-	-	-	-	-	-	3	3	4	4	-	-	593
17.6	WE IGHT	810.0	450.0	131.0	8.0	38.0	200.0	10.0	150.0	856.0	280.0	5280.0	186.0	300.0	30.0	53.0	1.0	28.0	2650.0	163.0	16.0	21.0	16.0	16.0	11.0	1832.0	710.0	8.0	1890.0	570.0	8130.0	57780.0	24640.0	0.0096	2.0	39.0	160255.0
1/E	CUBE	40.8	50.9	0.6	.5	4.3	5.5	1.0	11.0	50.4	11.7	288.0	4.5	20.0	3.2	\$.	0.	1.4		20.0	• 5	1.4		٠٠		125.0	35.8	.3	4.06				,		0.	Ξ	1478.6
17.5	SOUARE																		125.0											46.0	279.0	771.0	704.0	244.0			2245.0
ITEM	WEIGHT	162.0	150.0	131.0	1.0	38.0	100.0	2.0	150.0	107.0	140.0	330.0	62.0	300.0	30.0	0.1	1.0	28.0	2650.0	163.0	16.0	21.0	16.0	16.0	11.0	1832.0	710.0	0.8	1890.0	220.0	2710.0	19260.0	13650.0	2400.0	2.0	39.0	
ITEM	CUBE	8.2	7.0	0.6		4.3	2.8	• 5	11.0	6.3	5.9	18.0	1.5	20.0	3.2	•	•	1.4		20.0	5.	1.4	5.	9.		125.0	35.8	• 3	2.06						0.	:	OTALS
ITEM	SQUARE																		125.0											46.0	93.0	257.0	176.0	0.19			GRAND TO
	TAM	02833	C5400	01153	CSHSO	C5870	08653	C6220	C6260	02893	C6 388	C6410	Cha 30	05950	05450	56684	56992	02000	06000	00100	00380	00390	00400	00410	00450	00725	00700	00100	00110	00840	00880	00488	01030	01160	01250	E2030	

TODAYS DATE 03/02/76

OP INDEX(SQUARE) = 93.73

OR INDEX(CUEE) = 87.16

DH 2001X(TOTAL 17) = H7.50

CONSTRAINED TZE FOR UNIT M8970

MARINE HELICOPTER ATTACK SQUADRON(HMA)

CUBE OF PUBLISHED TVE IS 1478-50 CU FT CONSTRAINED TO 87.5 PCT OR 1294-00 CU FT

SQUARE OF PURLISHED TZE 1S 2245.00 SO FT CONSTRAINED TO 87.5 PCT OR 1964.00 SO FT

																																		-	NOTE:		Unit =	2000	Justi					
PEFIC	1ENCY						:	.,																		23.									N		Ur	c	3					
T/F***	CUBE	7.0	1.0		1.0	13.0	84.5	60.3	5.1	۴.	0.	1.5	2.4	2.7	3.8	0.	2.7	۳.	75.6		0.	0.	26.1	.8	3.4	103.9	12.6	2.0		3.3	4.3	1.0	4.2	22.0	7.7	6.	1.4		2.0	7.7	11.0	30.0	10.6	11.3
****				76.0																																								
****	710	:	1.	:	:	:	•0	24.	:	:	:	5.	2.	10.	2.	1.	2.	2.	2.	10.	5.		•06	·	۶.	105.	2.	:-		-	•	2.	-	2.	:	93.	-	:	:	:	8.	2.		3.
CRIT	;	8	2	2	2	2	2	2	2	2	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
TVE	710	-	-	-	-	-	-	30	-	-	-	S	S	10	S	-	2	2	8	10	8	-	104	S	S	128	8	-	~	-	4	~	-	2	-	63	-	-		-	80	EV.	4	m
1/6	WEIGHT	182.0	28.0	2680.0	116.0	355.0	0.096	2520.0	145.0	82.0	1.0	20.0	30.0	30.0	35.0	1.0	120.0	0.9	1240.0	10.0	2.0	1.0	728.0	10.0	10.0	2048.0	150.0	20.0	10.0	40.0	40.0	20.0	53.0	128.0	0.09	93.0	0.9	2.0	40.0	40.0	680.0	20000	20.0	12.0
TVF	CUBE	7.0	1.0		1.0	13.0	173.0	74.4	5.1	. 8	0.	1.5	2.4	2.7	3.8	0.	3.7	.3	75.4		0.	0.	30.2	€.	3.4	126.7	12.6	2.0	.2	3.3	4.3	1.0	4.2	22.0	7.7	6.	1.4		5.0	7.7	21.0	30.0	10.6	
1/5	SQUARE			16.0																																								
FTF	WEIGHT	182.0	28.0	2680.0	116.0	355.0	0.096	84.0	145.0	82.0	1.0	4.0	0.9	3.0	7.0	1.0	0.09	3.0	620.0	1.0	0.1	0.1	7.0	2.0	2.0	16.0	80.0	20.0	2.0	40.0	10.0	10.0	53.0	64.0	0.09	1.0	0.9	2.0	40.0	40.0	85.0	250.0	14.0	٥.٧
Mali	CUBE	7.0	1.0		1.0	13.0	173.0	5.5	5.1	8.	0.	.3	• 5	.3	8.	0.	1.9	• 5	37.7	:	0.	0.	۲.	.2		1.0	6.3	2.0	-	3.3		• •	4.2	11.0	7.7	0.	1.4	• 5	2.0	7.7	6.4	15.0	2.1	3.8
NAT -	SQUARE			75.0																																								
	MA.	40870	42430	90630	91540	31650	91440	92030	01220	32240	C 2000	01020	05023	C2040	C2050	C2050	C2070	C2100	C2120	C2160	C2200	C2230	C2235	C2250	C2310	C3020	C4000	01010	C4020	C4040	01110	C4140	C4250	C4340	C4390	64436	C4670	C4680	C4690	C4 790	C4870	C5080	0:190	00250

= M8970 raint = 75%

## CONSTRAINED THE FOR UNIT MASTO

# MARINE HELICOPTER ATTACK SQUADRON(HMA)

CURTATE TZE FUR CLASS VII. CLASS II TAM ITEMS

CONSTRAINED TO 87.5 PCT OR 1234.00 CU FT

SQUARE OF PUBLISHED TZE IS 2245.00 SO FT CONSTRAINED TO 87.5 PCT OR 1964.00 SO FT

DEFTC-											3.																					:			
	9.04	50.02	0.6	•	4.3	5.5	1.0	11.0	50.4	11.7	232.8	4.5	20.0	3.2	r.	0.	1.4		20.0	.5	1.4	••	9.		125.0	35.8	•3	2000						0.	:
******REDUCFD T/E****																		125.0											46.0	252.9	6.049	569.6	214.5		
,	5.	3.	:	. 8		2.	2.	:	.8	2.	13.	3.	:	:	53.		:	:	:	:	:	:	:	:	:	:	:	:	:	3.	3.	3.		:	:
CRIT	-	-	1		-	-	-	-	-		1	-	-	-	-	-	8	2	2	2	2	2	2	8	2	~	2	2	2	2	4	~	2	-	~
17E	r	3	-	œ	-	2	~	-	80	8	91	3	-	-	53	-	-	-	-	-	-	-	-	-	-	-	-	-	-	n	m	4	4	-	-
T/E WEIGHT	810.0	450.0	131.0	8.0	38.0	200.0	10.0	150.0	856.0	280.0	5280.0	186.0	300.0	30.0	53.0	1.0	28.0	2650.0	163.0	16.0	21.0	16.0	16.0	11.0	1832.0	710.0	8.0	1890.0	570.0	8130.0	57783.0	54640.0	0.0096	2.0	39.0
TVE	40.8	50.0	0.6	c.	4.3	5.5	1.0	11.0	50.4	11.7	288.0	4.5	20.0	3.2	6.	••	1.4		20.0	.5	1.4	s.	9.		125.0	35.8	•3	2.06						0.	:
TZE																		125.0											46.0	279.0	771.0	704.0	244.0		
WEIGHT	162.0	150.0	131.0	1.0	38.0	100.0	2.0	150.0	107.0	140.0	330.0	955.0	300.0	30.0	1.0	1.0	28.0	2650.0	163.0	16.0	21.0	16.0	16.0	11.0	1832.0	710.0	8.0	1890.0	570.0	2710.0	19260.0	13660.0	2400.0	5.0	39.0
LTEM	8.2	7.0	0.6	:	4.3	2.8	• 5	11.0	6.3	8.9	18.0	1.5	20.0	3.2	••	••	1.4		20.0	5.	1.4	• 5	9.		125.0	35.8	.3	2.06						0.	3
SOUARE																		125.0											46.0	93.0	257.0	176.0	61.0		
7 4	05320	C5400	C5410	C5850	C5870	C5930	C6220	66260	C5370	C6 188	66410	26432	C6650	56995	C6664	56493	00000	08000	00100	00380	00390	00400	00410	00450	00725	00740	00120	00110	00840	00880	00988	01030	0110	01250	E2030

TODAYS DATE 03/02/76

DR INDEX(SOUARE) = 88.82

OR INDEX(CUBE) = 91.61

OP INDEX(TOTAL 1/5) = 91.44

545. 1964.0 1294.0

2245.0 1478.6 160255.0 593

GRAND TOTALS

CONSTRAÍNED TZE FOR UNIT M8937

MARINE MEDIUM HELICOPTER SOUADRONTHMM)

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS	11
Σ	23
+	00
-	
ASS	284
บ	80
-	- +
>	7 0
LASS	CURE OF PUBLISHED TZE IS 2847.91 CU FT CONSTRAINED TO 95.0 PCT OR 2706.00 CU FT
2	110
10	90
1/6	AINE
FATE	CURE
CUB	0 8

14 80 2339.00 CONSTRAINED TO 90.9 PCT OR

																																					0						
DFF IC-																						20.											NOTE:		Unit = M8937	Continue - 00%	constraint = 30%						
	0	0		0	6	0			7	α	c	1	1	3	4	~	0	0	a	α	•			~	2	•	0	-	0	7	<b>a</b>	c	,	2	0	c	c	4	2	0	1		1
7/E**** CUBE	7.	1.0		1.0	65.0	•	1.5	2.	2.	3.8		3.	3.1	•	75.4	•	0.	0.	27.8	α.	3.4	121.1	18.	•	3.	5.4	1.0	•	1.9	•	16.8	22.0	:.	1.5	0.0	÷	15.	1.4		2.0	7.	105.0	13.
#####FDUCED TZE####			76.0																																								
***	1:	-	-1	-	25.	:	5.	5.	10.	.5	:	. 2	15.	2.	2.	10.	5.		.96	5.	5.	122.	3.	2.	-	5.	2.	:	38.	<u>:</u>	•	5.	•	118.	•	:		-	-	-	-	7.	.01
CRIT	8	2	2	2	8	-	-	-	1	-	-	-	1	-	1	-	-	1	-	-	-	-	-	-	-	-	-	-	-	-	-			~ .		-	-		-	-	-	-	-
17E	-	-	-	-	30	-	2	S	10	S.	-	2	15	2	2	10	2	-	96	S	S	142	E	2	-	r	~	-	38	-	4	۸.		21.3	•	_	-	-	-	-	-	^	1.0
T/E WEIGHT	182.0	28.0	2680.0	116.0	2520.0	1.0	20.0	30.0	30.0	35.0	1.0	120.0	75.0	6.0	1240.0	10.0	2.0	1.0	672.0	10.0	10.0	2272.0	240.0	10.0	40.0	20.0	20.0	0.1	38.0	45.0	212.0	129.0	0.00	1.18.0	0.0	82.0	204.0	0.5	5.0	40.0	40.0	10601	0.000
CUBE	7.0	1.0		1.0	74.4	0.	1.5	2.4	2.7	3.8	0.	3.7	3.1	• 3	75.4		c.	0.	27.8	8.	3.4	140.6	:8.3	• 5	3.3	5.4	1.0		1.9		10.8	22.0		7.1	0.0	0.5	12.0	1.4	• 5	5.0	7.7	101.3	6.1.7
SQUARE			76.0																																								
WEIGHT	182.0	28.0	2680.0	116.0	84.0	1.0	4.0	0.9	3.0	7.0	1.0	0.09	5.0	3.0	620.0	1.0	1.0	1.0	7.0	2.0	2.0	16.0	80.0	2.0	40.0	10.0	10.0	1.0	1.0	45.0	53.0	0.40	0.00	0.0	0.00	0.00	204.0	6.0	2.0	40.0	40.0	130.0	0.4.
CUBE	7.0	1.0		1.0	2.5	0.	.3	\$.	.3	8.	••	1.9	• 5	• 5	37.7	-	••	0.	.3	•5		1.0	6.3	:	3.3	-:	.5	•	-		2.6	11.0		•	0.0	0.0	15.0	1.4	• 5	2.0	7.7	15.0	6.9
SOUARE			26.0																																								
TAM	40470	A2460	80630	91540	92030	00023	01020	C2030	05070	62050	50,769	07020	08023	C2100	C2120	09120	C2200	C2230	C2235	C2220	C2310	C3020	C4000	04020	C4040	01110	04140	C4205	C4208	54230	64250	04340	24.000	200	(4555	00000	64460	64670	C4480	06940	06280	64820	04:170

### CONSTRAINED TZE FOR UNIT M9937

## MARINE MEDIUM HELICOPTER SQUADRON(HMM)

# CURTATE TAF FOR CLASS VIII. CLASS II TAM ITFWS

E	-	FT	FT
3	2	80	20
CUBE OF PUBLISHED TZE 15 2867.91 CU FT	CONSTRAINED IN SECTION 2 705.03 CO FT	SQUARE OF PUBLISHED TYF IS 2339.00 SQ FT	CONSTRAINED TO 90.9 PCT DR 2127.00 SO FT
1.5	260	5	20
1/1	-	1/5	000
SHED	5	SHED	000
UBL I	-	UISL I	07 0
OF P	Ž	0F P	AINF
CUBE		SOUARE	CONSTR

DEFIC- TENCY																	•																										
CURE	42.7	0.96	30.0	18.6	87.6	40.0	13.0	125.0	1.4	4.3	5.5	.2	1.0	1.5	69.3	11.7	364.0	357.0	4.5	20.0	4.	:	0.0		0.	1.4	499.0	20.0	1.4	5.	4.		0.	125.0	35.8	r.	400						
**************************************																																						92.0	183.5	122.0	678.8	325.5	214.2
• VTO	12.	7.	2.	7.	23.	.,	2.	٠,	24.	:-	2.	:	2.	30.		2.	20.	3.	3.	:	13.	3.	:	72.	:	:	-	:	-	:	:	:	:	:	:	:	1.	5.	2.	2.	3.	2.	•
11 00	-	-	-	-	-	-	1		1	-		1	-	-	1		-	-		-	-	1	-		-	8	2	8	2	2	2	8	8	8	N	2	8	8	2	4	4	٨	2
17E	12	1	8	1	52	9	2	S	24	-	~	1	8	30	11	~	56	3	3	-	13	۳	-	72	-	1	-	-	-	-	-	-	-	-	-	-	-	2	8	2	<b>m</b>	2	•
T/E WE IGHT	0.96	1050.0	20000	98.0	100.0	972.0	300.0	1765.0	24.0	38.0	200.0	7.0	10.0	30.0	1177.0	280.0	8580.0	6444.0	186.0	300.0	13.0	3.0	0.0	72.0	1.0	28.0	2650.0	163.0	21.0	16.0	16.0	11.0	1.0	1832.0	710.0	9.0	1890.0	1140.0	5420.0	1000.0	67780.0	27323.0	0.0000
CUBF	42.7	0.80	30.0	18.6	5.46	49.0	13.9	125.0	1.4	4.3	5.5	.2	1.0	1.5	69.3	11.7	458.0	357.0	4.3	20.0	••		0.0		0.	1.4	499.0	20.0	1.4	•5	9.		c.	125.0	35.9		2.06						
SOUARE																																						92.0	186.0	122.0	771.0	352.0	544.0
MEITEM	9.0	150.0	250.0	14.0	4.0	162.0	150.0	353.0	1.0	38.0	100.0	7.0	2.0	1.0	107.0	140.0	330.0	2148.0	62.0	300.0	1.0	1.0	0.0	1.0	1.0	28.0	2650.0	163.0	21.0	14.0	16.0	11.0	1.0	1832.0	710.0	0.0	1890.0	570.0	2710.0	200.0	19250.0	13660.0	2430.0
CUBE	3.6	14.0	15.0	2.7	3.8	8.2	7.0	25.0	-	4.3	2.8	• 5	• 5	:	6.3	5.9	18.0	119.0	1.5	20.0	:		0.0	0.	0.	1.4	499.0	20.0	1.4	5.	9.		••	125.0	35.8	.3	2.06						
SQUARE																																						46.0	93.0	61.0	257.0	176.0	61.0
TAM	06143	04040	08050	C5110	00250	C5320	00050	C5820	C5850	C5870	C5930	C0:40	02250	26345	C6 370	C6388	C6410	C6420	C6490	C6650	55993	66658	26995	C6684	56493	02000	00000	00100	00100	00400	00410	20420	00634	00725	00740	00100	02100	00440	00880	99385	99896	01030	91160

CONSTRAINED TZE FOR UNIT M9937

# MARINE WEDIUM HELICOPTER SQUADRON(HWW)

CURTATE TZE FOR CLASS VII. CLASS II TAM !TEMS

FT	FT	F
2	5	20
2847.31	2704.00	2339.00
51	90	15
1/5	PCT	3/1
CUBE OF PUBLISHED TYE IS 2847.91 CU FT	CONSTRAINED TO 95.0 PCT OR 2706.00 CU FT	SQUARE OF PURLISHED THE 15 2339.00 SO FT
c	4	OF
CUBE	CONSTE	SOUARF

	*****REDUCED T/E**** DEFIC- OTY SOUARE CUGE TENCY	15.0	809. 2127.0 2706.0
	*****REDUC	4. 415.0	809. 212
<b>.</b>	CRIT	<b>*</b> ~	
0 83	1/E	•-	842
CONSTRAINED TO 90.9 PCT OR 2127.00 SQ FT	TZE TZE CRIT	21840.0 4 4	2339.0 2847.9 157031.0 842
10.0 PCT	TVE	3	2847.9
ATNED TO	TZE	406.0	2339.0
CONSTR	ITEM	39.0	
	I TEM CUSE	3	OTALS
	SOUARE	124.0	GRAND TOTALS
	7 44	D1196 E2030	

TODAYS DATE 03/03/76
OR INDEX(SOUARE) = 91.93
OP INDEX(CUBE) = 95.79
OR INDEX(TOTAL T/E) = 95.54

CONSTRAINED THE FOR UNIT MB937

## MARINE MEDIUM HELICOPTER SOUADRON(HMM)

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUNSTRAINED TO 92.5 PCT OR 2634.00 CU FT SQUARE OF PUBLISHED TZE IS 2339.00 SQ FT CONSTRAINED TO 88.5 PCT OR 2071.00 SQ FT

DEFIC-	TE NCY					.9														13.			29.										NOTE.	MOLE:		Unit = M893/	Constraint = 85%							
/E****	CUBE	7.0	1.0		1.0	58.3	••	1.5	5.4	7.2	3.8	c.	3.7	3.1		75.4		0.	0.	24.5		3.4	1111.7	18.9	.2	3.3	5.4	1.0	-			16.8	22.0	7.7	1.2	0.0	3.0	12.0	1.4		4.0	7.7	105.0	43.7
*****REDUCED T/E***	SOJAPE			76.0																																								
****	710	:	:	:	:	24.	:	5.	8.	10.	5.	:	2.	15.	2.	5.	10.	2.		83.	5.	5.	113.	3.	2.	:	3.	5.	:	38.	<u>:</u>	;	5.	:	118.	•	:	:	:	-	-	-	7.	10.
CPIT		8	2	2	~	2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	_	-	-	-	-	-	-	-	-	-	-
1/6	710	-	-	-	-	30	-	2		10	S	-		15	2	8	01			96	S	2	-	3	~	-	r	8		38	-	4	2	-	118	4	-	-	-	-	-	-		01
1/E	WE I GHT	182.0	28.0	2680.0	116.0	2520.0	1.0	20.0	30.0	30.0	35.0	1.0	120.0	75.0	6.0	1240.0	10.0	2.0	1.0	672.0	10.0	10.0	2272.0	240.0	10.0	40.0	20.0	20.0	1.0	38.0	45.0	212.0	128.0	0.09	118.0	0.0	85.0	204.0	0.9	2.0	40.0	47.3	1050.0	870.0
1/E	CUBE	7.0	1.0		1.0	74.4	0.	1.5	2.4	2.7	3.8	0.	3.7	3.1	.3	75.4		c.	0.	27.8	.8	3.4	140.5	18.9		3.3	5.4	1.0	•	1.0		16.8	55.0	7.7	1.2	0.0	3.0	12.0	1.4	. 2	2.0	7.7	105.0	61.7
1/6	SQUAPE			76.0																																								
ITEM	WE IGHT	182.0	28.0	2680.0	116.0	84.0	1.0	0.4	0.9	3.0	7.0	1.0	0.09	2.0	3.0	620.0	1.0	1.0	1.0	7.0	2.0	2.0	16.0	80.0	2.0	40.0	10.0	10.0	0:-	1.0	45.0	53.0	0.49	90.09	0.1	0.0	85.0	204.0	0.9	2.0	40.0	40.0	150.0	95.0
I TEM	CUBE	7.0	1.0		1.0	5.5	•		••	£.		••	1.0	• 5	.2	37.7	-	••	•	•3	.2		1.0	6.3	-	3.3	==	••	:	-		4.2	11.0	1.7	0.	0.0	3.0	15.0	1.4	• 5	2.0	7.7	15.0	0.0
ITEN	SOUARE			76.0																																								
	7 A 4	ACRTC	A2480	90430	31540	350 30	C2000	C2010	C2030	C2040	62050	C2060	C2070	C2030	C2100	C2120	C2150	C2200	C2230	C2235	C2250	C2 110	C3020	C4000	C4020	04040	C4110	C4140	C4205	C4208	C4230	C4250	C4 340	06280	C44.35	C4555	C4650	64660	01915	Co 630	CARSO	00293	02850	04+40

### CONSTRAINED TIE FOR UNIT M8937

### MARINE MEDIUM HELICOPTER SQUADRON(HMM)

ITEMS	F F	11
Z	33	800
ASS 11 TA	2634.00	2339.00 SO FT
VII. C.	ZE IS PCT OR	7F 15
CURTATE TZE FUR CLASS VIII. CLASS II TAM ITFWS	COME OF PUBLISHED TZE IS 2847.91 CU FT CONSTRAINED TO 92.5 PCT OR 2634.00 CU FT	SQUARE OF BURLISHED TZF IS CONSTRAINED TO 88.5 PCT OR
17	OF	MAIN
CURTATE	CONST	SQUARE

	N I I	E 22 -	1/5		14.						
SOUARE	CUBE	WEIGHT	SOUARE	CUBE	WE IGHT	017		017	SOUARE	CURE	IENCA
	3.6	8.0		42.7	94.0	12	-	12.		42.7	
	14.0	150.0		0.86	1050.0	^	-			0.80	
	15.0	250.0		30.0	20000	2	-	2.		30.0	
	2.7	14.0		18.6	98.0	~	-			18.6	
	3.8	4.0		94.5	100.0	25	-	21.		70.A	
	8.2	162.0		49.0	972.0	•	-	• 9		40.0	
	7.0	150.0		13.9	300.0	2	-	2.		13.0	
	25.0	353.0		125.0	1755.0	r	-	5.		125.0	
	•	1.0		1.4	24.0	24	-	24.		1.4	
	4.3	38.0		4.3	38.0	-	-	-		4.3	
	2.8	100.0		5.5	200.0	2	-	2.		5.5	
	.2	7.0		.2	7.0	-	1	-		.2	
	••	5.0		1.0	10.0	2	-	2.		1.0	
		1.0		1.5	30.0	30	1	30.		1.5	
	6.3	107.0		69.3	1177.0	=	-	::		59.3	
	6.5	140.0		11.7	280.0	~	1	2.		11.7	
	18.0	330.0		468.0	8580.0	56	-	18.		317.3	8.
	119.0	2148.0		357.0	6444.0	m	-	3.		357.0	
	1.5	62.0		4.5	186.0	٣	-	3.		4.5	
	20.0	300.0		20.0	300.0	-	-	<u>:</u>		20.0	
	•	1.0			13.0	13	-	13.		4.	
	• 1	1.0		:	3.0	e	-	3.		-	
	0.0	0.0		0.0	0.0	-	-	-		0.0	
	0.	1.0			72.0	72	-	72.			
	0.	1.0		0.	1.0	-	-	-		0.	
	1.4	28.0		1.4	28.0	-	2	:		1.4	
	499.0	2650.0		499.0	2650.0	-	2	:		490.0	
	20.0	163.0		20.0	163.0	-	2	-		20.0	
	1.4	21.0		1.4	21.0	-	2	:		1.4	
	• 5	16.0		• 5	16.0	-	2	:		v.	
	9.	16.0		9.	16.0	-	2	:		9.	
	.7	11.0		2.	11.0	-	2	:			
	0.	1.0		0.	1.0	-	8	-1		0.	
	125.0	1832.0		125.0	1832.0	-	2	:		125.0	
	35.8	710.0		35.8	710.0	-	2	1.		35.8	
	•3	0 · d		•3	8.0	-	2	:			
	2.06	1890.0		2006	1890.0	-	2	1:		4006	
46.0		270.0	92.0		1140.0	~	2	2.	92.0		
93.0		2710.0	186.0		5420.0	~	2	2.	182.9		
0.19		20000	122.0		1000.0	2		2.	122.0		
257.0		19260.0	77:00		57780.0		4	3.	654.5		
176.0		13660.0	352.0		27320.0	^	2	2.	318.5		
0.1.		0000									

CONSTRAINED TZE FOR UNIT M8937

### MARINE MEDIUM HELICOPTER SOUADRON(HMM)

CURTATE T/E FOR CLASS VII. CLASS II TAM ITFWS

CUBE OF PUBLISHED T/E IS 2847.91 CU FT CONSTRAINED TO 92.5 PCT OR 2634.00 CU FT

\*\*\*\*REDUCED T/F\*\*\* DEFIC-OTY SOUAPE CUBE TENCY CRIT SQUARE OF PUBLISHED TZE IS 2339.00 SO FT CONSTRAINED TO 88.5 PCT OR 2071.00 SO FT T/E WE IGHT I TEM WEIGHT

-

414.9

3.

4 0

39.0

--

496.0

39.0

1:1

124.0

51186 E2030

GRAND TOTALS

21840.0

17E

T/E CUBE

SQUARE

CUBE

SOUARE

2071.0 2634.0

780.

2847.9 167031.0 842

2339.0

TODAYS DATE 03/02/76
OR INDEX(SQUARE) = 89.68
OR INDEX(CUBE) = 92.30
OR INDEX(TOTAL T/E) = 92.13

### CONSTRAINED TZE FOR UNIT M8937

## MARINE MEDIUM HELICOPTER SQUADGON(HMM)

CONTAIL THE FOR CLASS VII. CLASS II TAM ITEMS 2402.00 CU FT 2339.00 SO FT 1959.00 SO FT CUBE OF PUBLISHED TZE IS CUNSTRAINED TO 87.5 PCT OR SQUARE OF PURLISHED TZF IS CONSTRAINED TO 83.8 PCT OR

				1							
SOUARE	CUBE	WEIGHT	SOUARE	CUBE	WE I GHT	770		914	SOJARE	CUPE	1 = 11C ×
	7.0	182.0		1.0	182.0	-	~	:		7.0	
	0.1	28.0		1.0	28.0	-	2			1.0	
15.0		26.90.0	16.0		2680.0	-	2	1.	76.0		
	1.0	116.0		1.0	116.0	-	~	-		1.0	
	2.5	84.0		74.4	2520.0	30	2	26.		64.7	•
	••	0.1		••	1.0	-	-	:		c.	
	.3	4.0		1.5	20.0	S	-	5.		1.5	
	.5	6.0		2.4	30.0	S	1	۶.		2.4	
	7.	3.0		2.7	30.0	10	1	10.		7.7	
	. 8	7.0		3.8	35.0	S	-			3.6	
	••	1.0		0.	1.0	-	-	:			
	1.9	0.09		3.7	120.0	8	-	2.		3.7	
	.2	5.0		3.1	75.0	15	-				
	• 5	3.0		•3	9.0	~	-	. 2			
	37.7	620.0		75.4	1240.0	^				75.4	
	:	1.0			10.0	10	-	10.			
	••	0.1		••	2.0	2	-	2.		0.	
	0.	1.0		0.	1.0	-	-	-1			
	.3	7.0		27.8	672.0	96	-	88.		25.4	
	•2	2.0			10.0	S	-	5.			
		2.0		3.4	10.0	S	-	5.		3.4	
	1.0	16.0		140.6	2272.0	142	-	125.		123.3	17.
	6.3	80.0		18.9	240.0	2	-	3.		18.9	
	-	2.0		•2	10.0	8	-	2.		.2	
	3.3	40.0		3.3	40.0	-	-	:		3.3	
	:	10.0		5.4	20.0	S	-	5.		5.4	
	\$.	10.0		1.0	20.0	2	-	5.		1.0	
	:	1.0		-:	1.0	-	-	:		•	
	•	1.0		1.9	38.0	38	-	38.		1.9	
	.7	45.0			45.0	-	-	:		2.	
	4.2	53.0		16.9	212.0	4	-	4		16.8	
	11.0	64.0		22.0	128.0	~	1	2.		22.0	
	7.7	0.09		7.7	0.09	-	-			7.7	NOTE:
	0.	1.0		1.2	118.0	118	-	118.		1.2	
	0.0	0.0		0.0	0.0	4	-	4		0.0	Ilnit = M8937
	3.0	85.0		3.0	85.0	-	-	:		3.0	
	12.0	204.0		12.0	204.0	-	-	:		12.0	Constraint = 7
	1.4	0.9		1.4	0.9	-	1	:		1.4	
	.2	2.0			2.0	-	-	:		2.	
	2.0	40.0		2.0	40.0	-	-	:		5.0	
	7.7	40.0		7.7	40.0	-	-	:		7.7	
	15.0	150.0		105.0	1050.0	1	-	7.		105.0	
	6.4	0.82		67.7	6.00.0						

int = 75%

### CONSTRAINED T/E FUR UNIT M8937

# MARINE MEDIUM HELICOPTER SQUADBON(HMM)

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CU FT CU FT	S0 FT S0 FT
2847.91 CU FT 2492.00 CU FT	2339.00
CONSTRAINED TO 87.5 PCT OR 2492.00 CU FT	SQUARE OF PUBLISHED T/E IS 2339.00 SO FT CONSTRAINED TO 83.8 PCT OR 1959.00 SO FT

DEFIC-	LE NC A					3.												5.																								:		1.
1/E****	CUBE	42.7	98.0	30.0	18.6	84.3	0.64	13.0	125.0	1.4	4.3	5.5	2.	1.0	1.5	69.3	11.7	375.5	357.0	4.5	20.0	٠.	-	0.0		0.	1.4	275.2	20.0	1.4	•5	٠.		0.	125.0	35.8	.3	4.00						
	SOUADE																																						92.0	171.2	122.0	6111.5	293.7	195.5
****	914	12.	7.	2.	. 7.	22.	٠,	2.	.0	24.	:	2.	:	2.	30.		2.	21.	3.	3.	:	13.	3.	:	72.	:	:	:	:	-	:	:	:	:	:	:	:	-	2.	8	۶.		8.	3.
CRIT		-	-	-	-	-	-		1		1	-		-	-	1	1	-	-		-	-	-	1		-	8	2	2	2	2	2	8	8	2	2	2	8	2	2	4	4	2	2
1/E	710	12	1	8	1	25	9	8	S	24	-	2	-	~	30	11	2	52	6	e	-	13	3	-	72	1	-	1	-	-	-	-	-	-	-	-	-	-	~	7	~	3	~	4
1/E	WEIGHT	0.96	1050.0	20000	98.0	100.0	972.0	300.0	1765.0	24.0	38.0	20000	7.0	10.0	30.0	1177.0	280.0	8580.0	6444.0	186.0	300.0	13.0	3.0	0.0	72.0	1.0	28.0	2650.0	163.0	21.0	16.0	16.0	11.0	1.0	1832.0	710.0	8.0	1890.0	1140.0	5420.0	1000.0	57780.0	27320.0	0.0090
1/6	CUBE	42.7	98.0	30.0	18.6	94.5	49.0	13.9	125.0	1.4	4.3	5.5	• 2	1.0	1.5	69.3	11.7	468.0	357.0	4.5	20.0	9.		0.0		0.	1.4	499.0	20.0	1.4	• 5	ç.	.7	0.	125.0	35.8	•3	2.06						
1/E	SOUARE																																						95.0	186.0	122.0	771.0	352.0	244.0
ITEM	WEIGHT	8.0	150.0	250.0	14.0	4.0	162.0	150.0	353.0	1.0	38.0	100.0	7.0	5.0	1.0	107.0	140.0	330.0	2148.0	62.0	300.0	1.0	1.0	0.0	1.0	1.0	28.0	2650.0	163.0	21.0	16.0	16.0	11.0	1.0	1832.0	710.0	8.0	1890.0	570.0	2710.0	200.0	19260.0	13560.9	2400.0
ITEM	CUBE	3.6	14.0	15.0	2.7	3.8	8.2	7.0	25.0	-	4.3	2.8	•2	• 5	-:	6.3	5.9	18.0	119.0	1.5	20.0	:	••	0.0	•	•	1.4	499.0	20.0	1:4	· •	9.		•	125.0	35.8	.3	2.06						
ITEN	SOUARE																																						46.0	93.0	61.0	257.0	176.0	611.0
	144	C4880	C4980	65080	C2110	C5200	C5320	C5400	C5820	C5850	C5870	68930	Ce140	C6220	C6.345	C6370	68193	C6410	C6420	06490	C6650	66655	66658	C6682	C6684	26993	02000	00000	00100	00330	00400	00410	00450	00694	90725	00740	00100	00110	00840	DORRO	58+00	D0448	01030	01160

CONSTRAINED TIE FOR UNIT M8937

## MARINE MEDIUM HELICOPTER SOUADRON(HMM)

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

11	11
55	80
2492.00	2339.00
CONSTRAINED TO 87.5 PCT OR 2492.00 CU FT	SQUARE OF PUBLISHED TZE 15 2339.00 SQ FT CONSTRAINED TO 83.8 PCT OR 1959.00 SQ FT

- 2	:	
DEFIC- IFNCY	:	
CUBE	:	2492.0
**************************************	397.0	1959.0 2492.0
y 10	. :	801.
CRIT	4-	
17.6	٠-	842
TZE TZE CRIT WEIGHT OTY	21840.0	2339.0 2847.9 167031.0 842
T/E CUBE	:	2847.9
SQUARE	4 96.0	2339.0
ITEN	5460.0	
LITEM	3	TOTALS
SQUARE	124.0	GRAND TO
144	62030	

TODAYS DATE 03/02/76
OR INDEX(SQUARE) = 85.79
G9 INDEX(CUBE) = 95.12
G9 INDEX(TOTAL T/E) = 94.53

#### CONSTRAINED TZE FOR UNIT M8625

## FORWARD AIR DEFENSE BATTERY, MACG, MAW

CUSTATE TZE FOR CLASS VII. CLASS I! TAM ITEMS

CUBE OF PUBLISHED TZE 1S 3280.58 CU FT CONSTRAINED TO 90.0 PCT D2 2953.00 CU FT SQUARE OF PUBLISHED TZE 1S 4311.00 SQ FT CONSTRAINED TO 90.0 PCT DR 3880.00 SQ FT

Seric-	15 NC																							41.										NOIE:		Unit = $M8625$	, oct + 1 000%							
T/E****	CUBE	0.6	23.0	1.0	15.0		330.0	184.0	0.00			c.	9.1	2.7	3.8	0.	3.7			0.	0.	æ.	3.4	236.5	12.6	5.0	-	3.3	6.5	·.	B. A.	165.0	11.0	7.7	0.	0.9	12.0	1.4	4.	2.0	7.7	61.0	a .0 *	٠.
	SOUARE					70.0							£1.																															
****	VT0	3.	23.		15.	:	:	23.	.06	:	2.	1.	5.	10.	5.	1.	2.	:	10.	3.	:	٠.	20	239.	2.	:	:	:	•	:	2.	15.	-:		•06	2	:	:	2.	1:	-	* a	14.	:
CAIT		4	4	4	4	4	4	4	•	4	~	-	1	1	-	1	1	-	-	-	-	-	-	-	-	-	1	-	-	-	1	-	-	-	1	-	1	1	1	-	-	1	-	-
1/E	710	m	23	-	1.5	-	-	23	06	-	2	-	2	10	2	-	2	-	10	3	-	r	2	280	~	-	-	-	9	-	~	15	-	-	06	2	-		N		-	8	14	-
1/E	WE I GHT	141.0	460.0	10.0	330.0	4190.0	2575.0	3197.0	1800.0	28.0	164.0	1.0	20.0	30.0	35.0	1.0	120.0	3.0	10.0	3.0	1.0	10.0	10.0	4480.0	160.0	20.0	2.0	40.0	20.0	10.0	106.0	2700.0	64.0	20.0	0.06	170.0	204.0	6.0	4.0	40.0	40.0	6.80.0	112.0	13.0
1/E	CUBE	0.6	23.0	1.0	15.0		350.0	184.0	0.06	1.0	9.1	0.	1.5	2.7	3.3	0.	3.7	~.		· ·	0.	. 9	3.4	277.2	12.6	2.0	:	3.3	6.5	.5	8.4	165.0	11.0	7.7	6.	6.0	12.0	1.4	4.	5.0	7.7	51.0	69.3	
1/1	SQUAPE					70.0																																						
ITEM	WF IGHT	47.0	20.0	10.0	22.0	4190.0	2575.0	139.0	20.0	28.0	82.0	1.0	4.0	3.0	7.0	1.0	0.09	3.0	0.1	1.0	1.0	2.0	2.0	16.0	80.0	20.0	2.0	40.0	10.0	10.0	53.0	180.0	0.49	0.09	1.0	85.0	204.0	0.9	2.0	40.0	40.0	85.0	A.0	15.0
ITEM	CUBE	0.5	1.0	1.0	1.0		350.0	8.0	1.0	1.0	.8	0.	.3	٤.	.8	•	1.9	•2		••	••	•5		1.0	6.3	2.0	:	3.3		••	4.2	11.0	11.0	7.7	••	3.0	12.0	1.4	.2	2.0	7.7	6.4	3.6	
ITEM	SOUARE					70.0																																						
	T 4M	A0000	A0320	A1250	A1730	41000	A1940	A2020	42050	A2430	92240	60062	01022	C2040	05020	05020	C2070	C2:00	C2160	C2200	C2230	C2250	01122	63020	00000	C4010	C4020	C4040	C4110	C4140	C4250	C4290	C4340	C4390	C4436	05940	C4660	C4670	CARRO	06940	C4 700	04840	C143C	06000

#### CONSTRAINED TZE FOR UNIT M8625

## FORMARD AIR DEFENSE BATTERY, MACG. MAN

SWJI		
2	55	20
CURTAIN IZE FOR CLASS VIII. CLASS II TAM ITEMS	3280.58 CU FT 2953.00 CU FT	SOUARE OF PUBLISHED TZF 15 . 4311.00 SO FT CONSTRAINED TO 90.0 PCT OR 3380.00 SO FT
. CL	51 00	15 08
-	177	17F
CL. A55	CURE OF PUBLISHED TZE IS	1 90.0
100	PUBL 1	PUBL.
3	NIA.	DE
CUSTALE	CONSTRAINED TO 90.0 PCT OP	SOUAFF

	I TEN	LTEM	FFGM	1/5	TVE	1/E	TIE	CRIT	****	SEDUCED TYEARS	21 30 44	-31
744	SOUARE	CUBE	WEIGHT	SGUARE	CUBE	WE I GHT	710		410	SOUATE CURF	BE TENCY	4CY
06040		14.0	150.0		10.01	750.0	S	-	5.	20	20.07	
08030		15.0	250.0		15.0	250.0	-	-	1:	15	15.0	
うかつとし		4.0	196.0		4.0	196.0	-	-	:	4	0.4	
02110		2.7	14.0		23.9	126.0	6	1	•	23	23.9	
C5200		3.8	4.0		3.8	0.4	-	-	-1	3	3.8	
C5320		8.2	152.0		65.3	1296.0	60	-	œ.	69	65.3	
C5400		7.0	150.0		13.9	300.0	~	1	2.	13	13.9	
C5410		0.6	131.0		3.0	131.0	1				6:0	
65920		25.0	353.0		100.0	1412.0	4	-	*	100.00	• •	
C5970		4.3	38.0		4.3	38.0	-	1	:	4	4.3	
C2930		2.8	100.0		2.8	100.0	-		:	2	2.8	
02190		6.3	245.0		6.3	246.0	-	-	1:	•	6.3	
26140		.2	7.0		.2	7.0	-	1			٠٠.	
02290		• 5	5.0		1.5	15.0	3	1	3.		1.5	
C6250		11.0	150.0		11.0	150.0	-	1	-1	11.0	0.	
08293		•	0.4		:	4.0	-		1.			
025.93		6.3	107.0		6.3	107.0	7	,	-1	•	6.3	
28132		6.5	140.0		11.7	280.0	2		2.	11.7	.7	
06290		7.2	257.0		57.4	2056.0	ď	-	8.	57.4	4.	
00490		126.0	2136.0		126.0	2136.0	-	2	-	126.0	••	
01490		18.0	330.0		0.00	1650.0	2	1	5.	0.06	. 0.	
06490		1.5	62.0		10.5	434.0	7		7.	10.5	۲.	
01590		6.9	0.00		6.9	0.00	-	-		•	6.9	
05490		20.0	300.0		20.0	300.0	-			50	20.0	
C6655		:	1.0		4.	8.0	80	1	8.			
C6658		:	1.0		•	1.0	1		:			
56684		0.	1.0		1.0	103.0	103	1	103.	-	0.	
02000		1.4	28.0		1.4	28.0	-	2	:		1.4	
06000	38.0		1054.0	38.0		1054.0	-	2	:	38.0		
00100		20.0	153.0		20.0	163.0	-	2	:	20	20.0	
00110		4.0	517.0		4.0	517.0	-	-	:	4	4.0	
00380		• 5	16.0		• 5	16.0	-	2	1.		• 5	
00390		1.4	21.0		1.4	21.0	-	2		-	1.4	
00400		• •	16.0		.5	16.0	-	N	:		.5	
00410		9.	16.0		••	16.0	-	2	:		٠.	
00725		125.0	1832.0		125.0	1832.0	-	2	:	125.0	0.	
00740		35.8	710.0		35.3	710.0	-	2		35	35.8	
00840	46.0		240.0	1196.0		14820.0	58	4	23.	1041.8		3.
00860	0.96		2750.0	0.96		2750.0	-	4	:	0.50		
00880	63.0		2710.0	184.0		5420.0	2	4	2.	186.0		
06600	71.0		2780.0	71.0		2780.0	-	N	1.	71.0		
02010	176.0		13660.0	528.0		40930.0	n	4	3.	521.R		
01110	18.0		0.000	546.0		27000.0	30	4	27.	0.504		:

CONSTRAINED TIE FOR UNIT M8625

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CURE OF PUBLISHED TZE IS 3280.58 CU FT CRNSTRAINED TO 90.0 PCT OR 2953.00 CU FT

SQUARE OF PUBLISHED TZE IS 4311.000 SO FT CONSTRAINED TO 90.0 PCT OR 3380.00 SO FT

	TENCY	:		8.		41.		
/E****	CUBE		c.	28.7	1.0	756.4	0.0	0 2953.0
PEDUCED T	OTY SOJARE CUBE	1353.4						3880.0
****	OTY	22.		74.	98.	100.	15.	1165.
CRIT		•	-	1	-	-	-	
1/1	710	52	-	82	66	150	15	1265
1/F	WE I GHT	62400.0	2.0	574.0	98.0 99	10650.0	0.0	206269.0 1265
1/E	CUBE		0.	32.0	1.0	1050.0	0.0	3280.6
17.6	SOUARE	1586.0						4311.0
ITEM	WEIGHT	2400.0	2.0	7.0	0.1	71.0	0.0	
ITEM	CUBE		••	*.	0.	7.0	0.0	DTALS .
TTEM	SOUARE	61.0						GRAND TOT
	MAT	01110	51250	E0390	F0210	E0590	£3195	

TODAYS DATE 03/03/76
OR INDEX(SQUARE) = 89.22
OR INDEX(CUBE) = 94.56
OP INDEX(TOTAL T/E) = 93.61

CONSTRAINED TIE FOR UNIT M8625

CUPTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CUNSTRAINED TO 85.0 PCT OR 2769.00 CU FT SOUARE OF PUBLISHED T/E IS 4311.00 SO FT CONSTRAINED TO 85.0 PCT OR 3664.00 SO FT

inger IC-	TENCY							.2.	14.															66.										NOTE.		That - 100.75	Unit = M0023	Constraint = 85%						
****3/1	CUPE	0.6	23.0	1.0	15.0		350.0	171.6	75.9	1.0	٠.:	c.	1.5	7.7	3.8	0.	3.7			0.	0.	٠.	3.4	211.7	12.6	2.0	-	3.3	6.9		4.6	155.0	0.11	7.7	•	0.9	12.0	1.4	4.	5.0	7.7	51.0	40.8	4.
****** CEDUCED I/E***	SOJARE					70.0																																						
****	710	3.	23.	-	15.	:	:	21.	76.	:	2.	-	·¢	10.	9.	:	2.	:	10.	3.	:	5.	5.	214.	2.	:	:	-		-	5	15.	:	-	.06	2.	:		2.	-	-	.6	14.	-
CRIT		4	4	•	4	•	4	4	4	4	~	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-	-
TZE	410	r	23	-	15	-	-	23	06	-	2	-	S	10	S	-	2	-	10	m	-	S	c	280	2	-	-	-	9	-	~	15	-	-	06	2	-	-	2	-	-	6	14	-
1/E	WE 1GHT	141.0	460.0	10.0	330.0	4190.0	2575.0	3197.0	1800.0	28.0	164.0	1.0	20.0	30.0	35.0	1.0	120.0	3.0	10.0	3.0	1.0	10.0	10.0	4480.0	160.0	20.0	2.0	40.0	0.09	10.0	105.0	2700.0	64.0	0.09	0.06	170.0	204.0	6.9	0.4	40.0	40.0	580.0	0.51.7	15.0
1/E	CUBE	0.6	23.0	1.0	15.0		350.0	184.0	0.06	1.0	1.6	0.	1.5	2.7	3.8	0.	3.7	.2		0.	0.	.8	3.4	277.2	12.6	2.0	:	3.3	6.5	• 5	8.4	165.0	11.0	7.7	6.	0.9	12.0	1.4	4.	6.0	7.7	51.0	49.8	4.
1/E	SQUARE					20.0																																						
ITEM	WEIGHT	47.0	20.0	10.0	22.0	4190.0	2575.0	139.0	20.0	28.0	82.0	1.0	4.0	3.0	7.0	1.0	0.09	3.0	1.0	0.1	1.0	2.0	2.0	16.0	80.0	20.0	2.0	40.0	10.0	10.0	53.0	180.0	0.49	0.09	1.0	85.0	204.0	0.9	2.0	40.0	0.04	95.0	8.0	15.0
ITEM	CUBE	3.0	1.0	1.0	1.0		350.0	8.0	1.0	1.0	.8	0.	.3	.3	.8	0.	1.9	•5	:	••	••	•5		1.0	6.3	5.0	-	3.3	1:1	• 5	4.2	11.0	11.0	7.7	0.	3.0	12.0	1.4	• 5	2.0	7.7	6.4	3.6	4.
ITEM	SOUARE					10.0																																						
	TAN	A0090	A0320	A1250	A1730	A1900	A1940	A2020	A2050	A2480	H2240	00000	07020	C2040	C2050	09020	62070	C2100	C2160	C2200	C2230	C2250	C2310	C3020	C4000	C4010	C4020	C4040	C4110	C4140	C4250	06240	C4340	C4330	C4436	C4550	C4660	C4670	C4630	06440	C4 7 30	04640	64880	64930

### CONSTRAINED TZE FOR UNIT M3625

FORWARD AIR DEFENSE SATTERY, MACG, MAW

3		
1	##	1. L
2	2.5	50
-	58	000
=	80.	11.
155	32	36
5		α
•	18	81
>	PC	PC.
5.5	6.	0
-	SHE	SHE
	120	170
CURTATE IZE FOR CLASS VII. CLASS II TAM ITEMS	CUBE OF PUBLISHED TZE IS 3280-58 CU FT CONSTRAINED TO 85-0 PCT OR 2788-00 CU FT	SQUARE OF PUBLISHED TZE IS 4311.00 SQ FT CONSTRAINED TO 85.0 PCT OR 3664.00 SQ FT
1/1	OF AIN	OF
	STR	STR
×13	ON	A O O
3		S

-01 4 30 15 NCV																																											
T/E****	70.0	15.0	4.0	23.0	3.8	65.3	13.0	0.0	100.0	4.3	2.6	6.3	.2	1.5	11.0	:	6.3	11.7	57.4	125.0	0000	10.5	6.9	20.0		-	0	1.4		20.0	4.0		1.4		٠.	125.0	35.8						
**************************************									•																				38.0									970.4	96.0	186.0	71.0	482.5	464.7
, , , ,	ů.	:	:	°	:-	8	2.	1:		:	:	:	1:	3.	:	:	-1	٠,	ъ. К	1.	5.	7.	1:	1:	8.		103.	1:		:	:	:	:	:	:	:	:	21.	:-	2.	1:-	3.	. 75.
CRIT	-	-	-	-	-	-	-	-	-	-	-	1	-	-	-	-	-	-	-	2	-	-	-	-	-	-	1	2	2	2	-	8	2	2	2	2	2	4	4	4	2	4	•
17E	r	-	-	6	-	œ	8	-	4	-	-	-	-	<b>6</b>	-	-	-	2	œ	-	S	1	-	-	20	-	103	-	-	-	-	-	-	-	-	-	-	56	-	2	-		30
T/E WEIGHT	750.0	250.0	196.0	156.0	4.0	1296.0	300.0	131.0	1412.0	38.0	100.0	246.0	7.0	15.0	150.0	4.0	107.0	280.0	2056.0	2136.0	1650.0	434.0	0.06	300.0	8.0	1.0	103.0	28.0	1054.0	163.0	517.0	16.0	21.0	16.0	16.0	1832.0	710.0	14820.0	2750.0	5420.0	2740.0	40030.0	57630.0
T/E CUBE	70.0	15.0	4.0	23.9	3.8	65.3	13.9	0.6	100.0	4.3	2.8	6.3	.2	1.5	11.0		5.3	11.7	57.4	126.0	0.06	10.5	6.9	50.0	*.	:	1.0	1.4		20.0	4.0	.5	1.4	٠.	9.	125.0	35.8						
TIE																													38.0									1196.0	0.96	186.0	71.0	528.0	540.0
NE IGHT	150.0	250.0	196.0	14.0	0.4	162.0	150.0	131.0	353.0	38.0	100.0	246.0	7.0	5.0	150.0	0.4	107.0	140.0	257.0	2136.0	330.0	62.0	0.06	300.0	1.0	1.0	1.0	28.0	1054.0	153.0	517.0	16.0	21.0	16.0	16.0	1832.0	710.0	270.0	2750.0	2710.0	2740.0	13060.0	0.000
CUBE	14.0	15.0	0.4	2.7	3.8	8.2	7.0	0.6	25.0	4.3	2.8	6.3	• 5	• 5	11.0	:	6.3	6.6	7.2	126.0	18.0	1.5	6.9	20.0	••	••	••	1.4		20.0	4.0	.5	1.4	5.	9.	125.0	35.8						
SQUARE																													38.0									46.0	0.96	93.0	71.0	176.0	13.0
747	C+ 0 + 0	C3090	06050	C5110	C5200	C5320	C5400	C5410	C5520	C2853	62330	C6130	06130	C6220	09290	66290	02893	C6 188	C6 390	C6400	C6410	06490	C6510	05490	C6655	C6658	66684	02000	06000	00100	00176	00180	00300	00400	00410	00725	00700	00000	09800	00880	06000	01030	01110

CONSTRAINED TZE FOR UNIT M9625

CURTATE THE FOR CLASS VII. CLASS II TAM ITEMS

CUBE UF PUBLISHED T/E IS 3280.58 CU FT CONSTRAINED TO 85.0 PCT DR 2788.00 CU FT

SQUARE OF PUBLISHED TZE IS 4311.00 SQ FT CONSTRAINED TO 85.0 PCT OR 3664.00 SQ FT

DEFIC-		5.		15.		56.		
T/E***	2005		••	26.3	1.0	655.1	0.0	0 2788.0
*****REDUCED T/E***	LENORE	1276.8						3564.0
****	;	21.	:	67.	.86	.46	15.	1098.
CRIT		*	-		-	-	-	
1/E	;	56	-	82	98	150	13	1265
1/5		0.00050	2.0	574.0	98.0	10650.0 150	0.0	206269.0 1265
1/E	1000		·	32.0	1.0	1050.0	0.0	3280.6
TVE		1536.0						4311.0
TTEM		2400.0	2.0	7.0	1.0	71.0	0.0	
ITEM	200		••	4.	0.	7.0	0.0	DTALS
LTEM	1	01.0						GRAND TOTALS
2		0110	01250	60003	60210	E0590	£3195	

TODAYS DATE 03/02/76
UR INDEX(SQUARE) = 84.17
QR INDEX(CURE) = 87.93
OR INDEX(TOTAL T/E) = 87.26

CONSTRAINED TZE FOR UNIT M8525

CUNTATE THE FOR CLASS VII. CLASS II TAM ITEMS

CUME OF PUBLISHED TZE IS 3280.58 CU FT CONSIBAIND TO 70.0 PCT OP 2440.00 CU FT

SQUAVE UF PUBLISHED TZE IS 4311.00 SO FT CUNSTRAINED TO 75.0 PCT OR 3233.00 SO FT

-5116-	TENCY						•	•	17.															73.								2.		NOTE:		Ilnit = M8675		Constraint = 75%						
	CURE	3.6	22.6	1.0	15.0		2.06	152.8	73.1	1.0	1.6	0.	1.5	2.7	3.8	••	3.7			0.	0.	٠.	3.4	204.8	12.6	2.0	:	3.3	6.5	v.	8.4	144.7	11.0	7.7	6.	6.0	12.0	1.4	4.	2.0	7.7	51.0	40.0	•
*****DEDUCED T/C.***	SOUASE					70.0																																						
****	710	*	23.	:	15,	:	•	19.	73.	:	2.	:	5.	10.		-		:	10.	3.	:	3.	2.	207.		:		:	•		2.	13.	:	:	•06	2.	-	:	2.	:	:	8.	14.	:
CRIT		•	•	4	•	•	•	•	•	•	8	-	-	-	-	-	.,	-	-	-	-	-	-	-	-	-	-	-	_	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1/E	017	•	53	-	13	-	-	23	00	-	2	-	c	0	S	-	~	-	10	•	-	S	•	280	N	-	-	-	•	-	N	2	-	-	06	~	-	-	2	-	-	<b>a</b>	14	-
17.6	WE I GHT	141.0	460.0	10.0	330.0	4190.0	2575.0	3197.0	1800.0	28.0	154.0	1.0	20.0	30.0	35.0	1.0	120.0	3.0	10.0	3.0	1.0	10.0	10.0	4480.0	160.0	20.0	2.0	40.0	0.09	10.0	106.0	2700.0	64.0	0.09	0.06	170.0	204.0	0.9	4.0	40.0	40.0	480.0	112.0	12.0
TZE	CVDE	0.6	23.0	1.0	15.0		350.0	184.0	0.06	1.0	1.6	•	1.5	2.7	3.8	•	3.7	.2	1.		0.	e.	3.4	277.2	12.6	2.0	:	3.3	6.5	5.	8.4	165.0	11.0	7.7	6.	6.0	12.0	1.4	4.	2.0	7.7	51.0	6.64	•
1/E	SOUARE					10.0																																						
ITEM	WEIGHT	47.0	20.0	10.0	22.0	4190.0	2575.0	139.0	20.0	28.0	82.0	1.0	0.0	3.0	7.0	1.0	0.09	3.0	1.0	1.0	1.0	2.0	2.0	16.0	80.0	20.0	2.0	0.04	10.0	10.0	53.0	0.081	64.0	0.09	1.0	85.0	204.0	0.9	2.0	0.04	40.0	95.0	8.0	15.0
ITEN	CUBE	3.0	1.0	1.0	1.0		350.0	8.0	0.1	0.1	8.	•	£.	.3		•	6.1	• •	:	•	•	•5		1.0	6.3	2.0	:	3.3	1:1	.5	4.2	11.0	0.11	7.7	•	3.0	12.0	1.4	• 5	2.0	7.7	6.4	3.6	*.
ITEN	SOUARE					10.0																																						
	144	A0090	40.420	41250	A: 730	A1900	04614	42020	42050	42430	82249	C2000	01000	05023	65023	62560	62023	C2100	C2150	C2200	C2230	C2250	62310	C3050	C4000	C4010	C+020	C4040	0110	C4140	C4250	C4290	C4340	C4390	64436	C4650	C4660	C4670	C4680	04940	00193	C4970	*	03 0 50

CONSTRAINED TZE FOR UNIT M8625

CURTATE TZE FOR CLASS VII. CLASS II TAM ITEMS

CONSTRAINED TO 75.0 PCT OR 2460.00 CU FT

SQUARE OF PUBLISHED TZE 15 4311.00 SO FT CONSTRAINED TO 75.0 PCT 09 3233.00 SO FT

** DEFIC-		0.07	15.0	0.4	6.	3.8	.3	13.9	0.0	0.	4.3	2.8	6.3	•2	1.5	0.		6.3		4.	0.	.0	10.5	6.9	20.0	4.		0.	1.4		20.0	4.0	.5	1.4	٠.	9.	0.	35.8	.6					7.
T/E***		70	u	4	23.9	3	65.3	13	C	100.0	4	2	9		•	11.0		•	11.7	4.72	126.0	0.06	01	•	20			-	1	0.	20	4		-			125.0	35		0.		6.		. 4.
*REDUCED	SQUARE																													38.0									847.6	0.40	179.7	71.0	424.2	414.4
****	¥ 10	5.	:		•6	1:	. 8	2.	1.	. 4	:		:	:		:	:	:1	2.	œ	:	.0.	7.	:	:	ď	-	103.	:	:	:	:	:	:	:	:	:	-	18.	<u>:</u>	2.	1.1	2	23.
CRIT		-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	2	-	-	-	-	-	-	-	2	2	2	-	2	2	~	2	2	~	4	*	4	2	4	
1/E	> TO	5	-	-	6	-	<b>6</b> C	~	-	4	-	-	-	-	۳	-	-	-	2	60	1	c	1	-	-	<b>c</b>	-	103	-	-	-	-	-	-	-	-	-	-	52	-	2	-		30
1/E	WEIGHT	750.0	250.0	196.0	126.0	4.0	1290.0	300.0	131.0	1412.0	38.0	100.0	246.0	7.0	15.0	150.0	4.0	107.0	280.0	2056.0	2135.0	1650.0	434.0	0.06	300.0	8.0	1.0	103.0	29.0	1054.0	163.0	517.0	16.0	21.0	16.0	16.0	1832.0	710.0	14820.0	2750.0	5420.0	2789.0	40980.0	0.00079
TVE	CUBE	70.0	15.0	0.4	23.9	3.8	65.3	13.9	0.6	100.0	4.3	2.8	6.3	.2	1.5	11.0	•	6.3	11.7	57.4	126.0	0.06	10.5	6.9	20.0	*•	-	1.0	1.4		20.0	4.0	5.	1.4	ç.	9.	125.0	35.8						
1/5	SQUARE																													38.0									1196.0	0.96	186.0	71.0	529.0	640.0
ITEM	WEIGHT	150.0	250.0	196.0	14.0	4.0	162.0	150.0	131.0	353.0	38.0	100.0	246.0	7.0	5.0	150.0	0.4	107.0	140.0	257.0	2136.0	330.0	62.0	0.06	300.0	1.0	1.0	1.0	28.0	1054.0	163.0	517.0	16.0	21.0	16.0	16.0	1832.0	710.0	570.0	2750.0	2710.0	2780.0	12560.0	0.000
ITEM	CUBE	14.0	15.0	4.0	2.7	3.8	8.2	7.0	0.6	25.0	4.3	2.8	6.3	•5	5.	11.0		6.3	5.9	7.2	126.0	18.0	1.5	6.9	20.0	-:	7.	0.	1.4		50.0	0.4	••	1.4	5.	9.	125.0	35.8						
ITEN	SQUARE																													38.0									46.0	0.96	63.0	7:-0	176.0	18.0
	XAT	C4090	C5030	06050	C5110	C5200	C5320	C5400	C5410	CSR20	C5870	02430	C6133	C6140	C6220	00293	C6290	C6370	C6.38d	C6390	C6400	C6410	C6490	C6510	05490	C6555	C6658	C6684	02000	06000	00100	00110	00380	00360	00400	01400	00725	09100	00000	00860	DGSBO	06890	5:033	01130

#### CONSTRAINED TIE FOR UNIT M8625

FORWARD AIR DEFENSE BATTERY, MACG, MAW

CURTAIL TZE FOR CLASS VIII. CLASS II TAM ITEMS

CUME OF PUBLISHED TZE IS. 3280-58 CU FT CONSTRAINED TO 75.0 PCT OR 2460-00 CU FT SQUARE OF PUBLISHED TZE 15 +311.00 SO FT CONSTRAINED TO 75.0 PCT OR 3233.00 SO FT

-31 J 16	:		17.		59.		
CURE		0.	25.2	1.0	637.2	0.0	0.2460.0
OTY SOJAPE CUEF	1992.1						3233.0
017	18.	:	65.	98.	.10	15.	1068.
CRIT		-	-	-	-	-	
17E	36	-	82	98	150	15	1265
T/C WE IGHT	62400.0	2.0 1					206287.0 1265
T/E CUBE		0.	32.0	1.0	1050.0	0.0	3280.6
TVE	1586.0						4311.0
MEIGHT	2400.0	2.0	1.0	1.0	71.0	0.0	
LTEN		0.	4.	0.	7.0	0.0	OTALS .
SQUARE	0.19						GRAND TOT
7.4.4	09110	01730	00003	601203	50590	E3145	

TODAYS DATE 03/02/76
OR INDEX(SQUARE) = 74.10
OR INDEX(CUBE) = 85.56
GR INDEX(TOTAL T/E) = 93.51

Appendix D

A MODEL TO COMPUTE AMPHIBIOUS LIFT FOR A VARIABLE DAY OF SUPPLY FROM THE F-2 JOPS CARD

#### Appendix D

A MODEL TO COMPUTE AMPHIBIOUS LIFT FOR A VARIABLE DAY OF SUPPLY FROM THE F-2 JOPS CARD

#### I INTRODUCTION

The automated output from the MAGTF Program is a card image file consisting of the JOPS formatted F-1, F-2, and F-3 cards. The MAGTF Program was written to include mountout cargo in certain of the F-2 cards as a function of the inputed days of supply (DOS). The term DOS is defined in the MAGTF System to be the days of supply for the MAGTF run under preparation. The MAGTF of MAF size is divided into the assault echelon (AE) and the assault follow-on echelon (AFOE). The term DOS applies to the AFOE allowing another parameter to designate AE days of supply. This parameter is called assault echelon days of supply (AEDOS), and its value may be less than equal to DOS (it is usually less than the DOS). The JCS specification for the F-2 card requires the mountout computation to be for a DOS value of 30 in all units of the MAF, and requires AEDOS to have the value 30 also. In an actual operation, AEDOS can be less than DOS, so the MAGTF Program permits the DOS parameter to be variable and therefore to take on a value assigned by the user. If the user plans to submit the JOPS cards from a MAGTF run, DOS must be set at 30. When the AEDOS is less than DOS, it becomes necessary to convert the mountout cargo on the F-2 cards for AE units from DOS to AEDOS. This conversion was necessary in order to utilize the existing automated output of the MAGTF System in the current study. In summary, a mathematical model was required to convert mountout cargo quantities, based on DOS, contained on the F-2 card to an amount based on AEDOS.

This model provides the conversion for bulk stowed cargo in units of the measurement ton and for square loaded cargo in units of square feet.

This appendix explains the model used in the TFEIN Program within CALAS in order to provide an understanding of the source of all data used in the study. The CALAS model is explained in Section VI.

#### II THE MODEL FOR BULK LOADING

The MAGTF System provides data by unit load and landing force supply for each unit in a MAGTF. The F-2 card of the JOPS Deck for mountout contains an amount specified for landing force supply only. The algorithm presented here pertains only to that portion of mountout contained in landing force supply.

Let:

T = The cube of mountout in landing force supply based on the value of DOS

d = The value of DOS.

If d is greater than 30,

 $T = T_1 + T_2$ 

where

 $T_1$  = Cube of materiel whose value is computed from the assault rate in the MAGTF Program for the first 30 days

T<sub>2</sub> = Cube of materiel whose value is computed from the sustained rate for DOS greater than 30, i.e., for (DOS - 30) days

 $\gamma$  = Proportion of mountout computed for the first 30 days.

Then:

 $T_1 = \gamma T$ 

 $T_2 = (1-Y)T.$ 

'If:

f(a<sub>k</sub>) = A function in the MAGTF Program computing the
 cube of mountout for the kth class of supply
 for the jth unit for d = 1

 $d_a$  = The DOS for the AEDOS ( $d_a \le 30$ )

d = The DOS for mountout

a = Allowance of ith TAM item of the jth unit

 $x_i$  = Cubic feet of the ith TAM item

s = Allowance of ith TAM item of the jth unit for square loaded items

 $z_{i}$  = Square feet of the ith TAM item,

then

$$T = \begin{cases} (30-d_a) \sum_{k=1}^{9} f(a_k) + (d-30) \sum_{k=1}^{9} f(a_k); d \ge 30 \\ d \sum_{k=1}^{9} f(a_k); d \le 30. \end{cases}$$
 (1)

Since T is known for the DOS minus the DOS carried in the unit load, it is necessary to find the mountout for the DOS in the landing force supply carried by the AE.

For certain items:

$$f'(a_k) = \sigma f(a_k) \tag{2}$$

when  $\sigma$  = .5. There are TAM items that do not have an assault rate different from the sustaining rate when  $\sigma$  = 1. The assumption is made that all items do have an assault rate when  $\sigma$  = .5. A slight error occurs from this assumption for those items that do not have an assault rate. Substituting equation (2) into (1) gives:

$$\sum_{k=1}^{9} f(a_k) = \frac{T}{(1-\sigma)(30-d_a)}$$
 (3)

the mountout for one DOS. Finally, the desired value for mountout contained in landing force supply for the AE at  $\begin{pmatrix} d & -d \\ a & u \end{pmatrix}$  DOS is given by:

$$T_1 = \frac{\gamma(d_1 - d_1)T}{(1 - \sigma)(30 - d_1)}.$$
 (4)

Certain classes of supply are not affected by an assault rate for which the first 30 days are greater than the second. For this materiel an expression to convert mountout computed from  $(d-d_u)$  DOS to  $(d_a-d_u)$  DOS carried in landing force supply is given by:

$$T_2 = \frac{(1-Y)(d_a - d_u)T}{(d-d_u)}$$
 (5)

Combining equations (4) and (5) an expression for  $\begin{pmatrix} d & -d \\ a & u \end{pmatrix}$  DOS carried in landing force supply in the AE for the jth unit is:

$$T'_{j} = (d_{a} - d_{u}) \frac{\gamma}{(1 - \sigma)(30 - d_{a})} + \frac{(1 - \sigma)}{(d_{a} - d_{u})} \sum_{\ell=1}^{p} T_{\ell},$$
 (6)

where P is the number of F-2 JOPS cards containing mountout data for the jth unit. Equation (6) is used in the TFEIN Program to convert mountout in the JOPS cards to the desired DOS.

The value for Y was obtained from the AE summary of the MAGTF listing by summing the cubic feet of materiel from supply classes having an assault rate and dividing by total mountout. Supply classes II, V, VII fall in this category.

#### III THE MODEL FOR SQUARE LOADING

Using exactly the same technique, mountout of square loaded items is converted to the desired DOS. Equations for this conversion are simplified by being involved with only supply class VIIW.

If  $S_{\ell}$  is the square feet of a group of square loaded items, mountout can be computed by:

$$s'_{j} = \frac{(d_{a}^{-d}u)}{(1-\sigma)(30-d_{a})} \sum_{\ell=1}^{p} s_{\ell}$$
 (7)

#### IV COMPUTING ALGORITHM

Now that the algorithm for computing mountout is available, the method used to obtain the lift expression for the AE and AFOE can be written by:

$$L_{A} = \sum_{j=1}^{M} \sum_{i=1}^{N} a_{ij} x_{i} + d_{u} \sum_{k=1}^{N} f(a_{k})_{j} + T'_{j}$$
 (8)

for bulk cargo in measurement tons

$$S_{A} = \sum_{j=1}^{M} s_{ij} z_{i} + d \sum_{u=1}^{N} c_{i} s_{ij} z_{i} + S'_{j}$$
(9)

for the AE, and

$$L_{F} = \sum_{j=1}^{M'} \sum_{i=1}^{N_{j}} a_{i} x_{i} + d_{i} \sum_{k=1}^{M} f(a_{k})_{j} + T_{j}$$
(10)

for bulk cargo, and

$$S_{F} = \sum_{j=1}^{M'} s_{ij} z_{i} + d_{u} \sum_{i=1}^{N'} c_{i} s_{ij} z_{i} + S_{j}$$
(11)

for the AFOE. It should be emphasized that  $T_j$  and  $S_j$  are summed values taken from the JOPS cards designated for landing force supply. This cargo is mountout for  $(d-d_u)$  DOS. These values are calculated by:

$$T_{j} = \sum_{\ell=1}^{P} T_{\ell}$$

$$S_{j} = \sum_{\ell=1}^{P} S_{\ell},$$
(12)

$$S_{j} = \sum_{\ell=1}^{P} S_{\ell},$$

where

P = Number of JOPS cards for landing force supply in the AFOE

= Number of units in the AE

Number of TAM items in the jth unit

N N' Number of square loaded TAM items on the jth unit.

#### V PROGRAM TFEIN

The TFEIN Program punches a card containing total personnel, barrels of bulk fuel,  $L_A$ ,  $S_A$ ,  $L_F$ , and  $S_F$ . The format of this card is the type 9 input of the TFE Program. This card is the movement requirement for the TFE Program. It is also used as one of the inputs to the Constrained Cargo Factoring Model. Appendix E explains this model and uses as its prime input the type 9 card. It is the values for  $L_{Aj}$  and  $S_{Aj}$  for each unit that must be factored into specific supply class categories before it is possible to apply constraints to unit cargo categories in a realistic manner. A description of Program TFEIN is given in the following paragraphs.

The initial design of Program TFEIN was to provide an interface between the JOPS card file containing the cargo requirements for individual units of the AE and AFOE and the additional data requirements for the transportation simulation provided by the TFE Program. Program TFEIN requires considerable data preparation for the transportation aspect of the output data and different data preparation necessary to modify JOPS data for the specific use of stating lift requirements for each unit. This program reads from card sources, accumulates lift requirements for the unit, performs the necessary modifications, combines all necessary data for the type 9 format, and punches and writes the type 9 output format for each unit. This program is included in CALAS as it currently exists. If a system such as CALAS is implemented, this program would be replaced by a similar program that prepared data obtained directly from Program MAGTF, thus providing all inputs to the Constrained Cargo Factoring Model without the manual interface required from the present programs that use JOPS card input.

Figure D-1 contains the flow chart for the TFEIN program. The following explanation refers to that figure. The program begins by initializing all parameters and reading all card input files. A value for unused mobile loading capacity is entered by card to provide the basis of reallocating a part of this unused capacity to all units of the AE. This calculation simulates the loading of all vehicles with mobile loaded cargo. A card deck is read providing the type 9 noncargo data elements. This information is placed in an array as a look-up table for use later in the program. An additional deck is read that provides unit mobile loaded cargo. This data is necessary because JOPS data includes cargo that would have been mobile loaded. The movement requirement, however, does not include mobile loaded cargo. The data source for this deck is the MAGTF listing for each unit of the AE.

When TFEIN is run for AE units, the conversion factor, explained earlier in this appendix, must be computed. This factor converts mount-out from 55 DOS to 10 DOS for AE units. The AFOE version of the program excludes this section of the code. The mobile loading reallocation factor is computed. This factor reduces the movement requirement uniformly among units of the AE.

The next section of code executes for each unit of the input JOPS file. The JOPS cards are read one at a time and processed before the next card is read. When all cards for one unit are processed, totals for bulk cargo, square loaded items, bulk fuel, and passengers are obtained. The output files are written for that unit, then the next unit's cards are processed. As each card is read, it is checked to determine if the last card image of the file has been read. If the last card has been processed, the program branches to 3. If not, the program determines if the card is F-1, F-2, or F-3 format and branches to the 5, 6, or 7 control points for further execution. The F-1 card provides the UTC for unit identification and the number of passengers. The program terminates reading JOPS cards

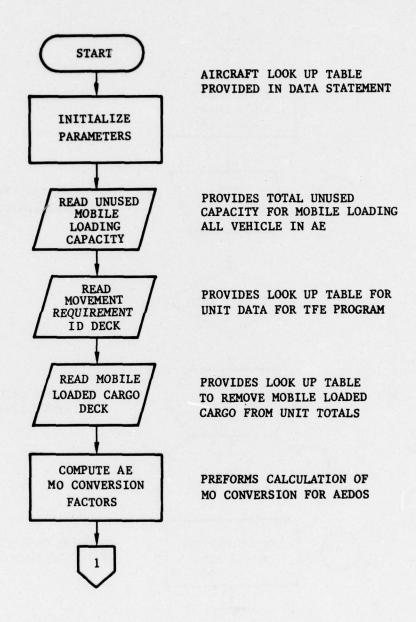
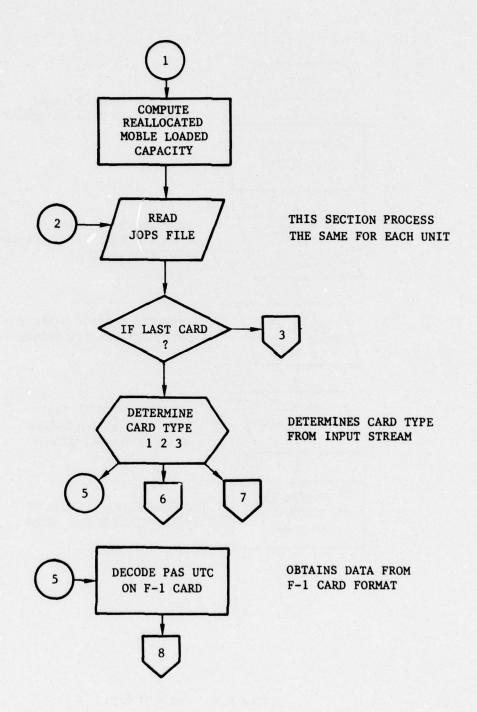
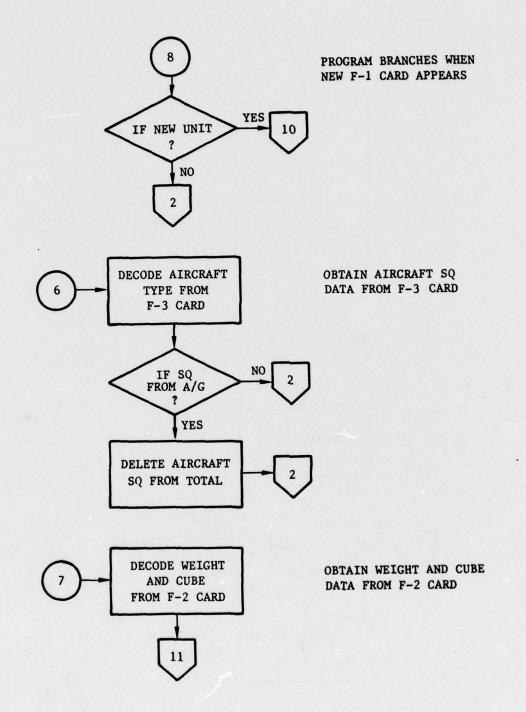
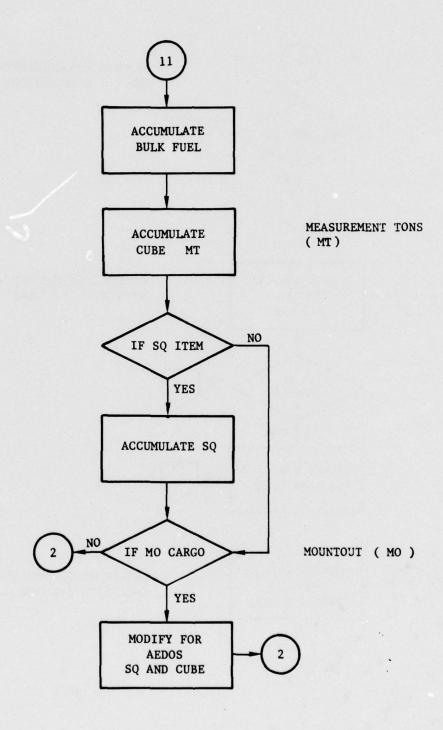
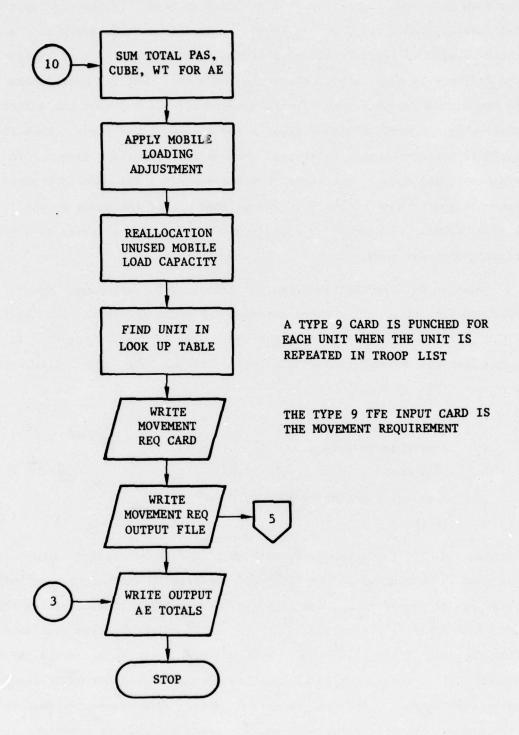


FIGURE D-1. PROGRAM TFEIN









for each unit when the next unit's F-1 card is read. If the next unit's F-1 card is read control passes to 10, otherwise control passes to 2 and the next card is read. Control is passed to 6 when an F-3 card is read. The F-3 card is used only to eliminate the square feet for helicopters in the square totals for helicopter squadrons. The F-3 card has a field containing the MAGTF system name of major square loaded items. When the field is compared with a helicopter look-up table provided from a DATA statement, the square feet added from the preceding F-2 card is removed when the system name on the F-3 card matches one of the names in the look-up table. After the F-3 card is processed, control passes to 2 for reading the next card.

When an F-2 card is read, control passes to 7. All cargo data is obtained from this card. There are many F-2 cards per unit. The CRCAT field of the F-2 card identifies the five cargo categories required to accomplish the accumulation of the totals for the unit. These categories are:

- a. Bulk cargo
- b. Square loaded cargo
- c. Bulk fuel
- d. Mountout (carried in landing force supply)
- e. Weight.

Category d is also composed of bulk cargo and square loaded cargo. After the data is obtained from the F-2 card, the program accumulates the bulk cargo square loaded cargo, and bulk fuel for the unit load according to the CRCAT field. Information on air transportability is also available from the CRCAT field if desired. When mountout cargo is processed, it is converted from the 55 DOS carried on the JOPS card from the MAGTF input parameters to the 10 DOS desired for AE units. This conversion feature is not used when processing AFOE units. After all data is processed from the F-2 card, control is passed back to 2 for reading the next JOPS card.

As previously stated, when the F-1 card for the next unit is read, control is passed to 10, where final processing for the current unit is accomplished. A total for the AE is obtained by adding unit totals together as they are computed. The mobile loaded cargo is subtracted, as well as the additional mobile loaded cargo capacity available to each unit from unit total bulk in measurement tons. The program then locates the current unit in the unit look-up table and combines cargo data with movement data required for the type 9 TFE input format. This format is then written to the output file and punched on cards for use as input to the TFE program and the AMPSF program, containing the Constrained Cargo Factoring Model of CALAS.

After the output statements have been executed, control passes to 5 and the F-1 card of the next unit just read is processed. If no further cards are contained in the file, control passes to 3 and the MAGTF totals are written to output and the program terminates.

Appendix E

CONSTRAINED CARGO FACTORING MODEL

## Appendix E

#### CONSTRAINED CARGO FACTORING MODEL

#### I INTRODUCTION

During the 1975-1980 time frame, the lift capacity of amphibious assault ships available to support a MAGTF of MAF size is expected to be less than the lift requirement of the assault echelon of the MAF. The extent of the amphibious lift short fall is presented in Section IV of this report. Section V provides an explanation of the nature and composition of landing force material. Familiarity with the information in Section V will be helpful in understanding the model presented in this appendix.

Each unit included in the troop list of the MAF has a lift requirement consisting of the nine classes of supply. This material is separated into the unit load and landing force supply. The unit load consists of the initial issue of supply classes II and VII, also known as the material specified by the table of equipment (T/E) and a specified number of days of supply (DOS) of all nine classes of supply called mountout. Therefore, the unit load consists of T/E, and for this project, five DOS of mountout. In addition, each unit generates a specified number of DOS of mountout to be included in landing force supply. The total mountout accompanying the AE is the 5 DOS in unit load and 10 DOS landing force supply, for a total of 15 DOS. The total DOS of mountout for the MAF is 60. The AFOE must also lift 45 DOS of mountout for the AE.

When the unit is prepared for loading it consists of four categories of requirements to be met by the amphibious assault ship capacity.

#### These are:

- (1) Personnel
- (2) Bulk fuel (barrels)
- (3) Bulk cargo (measurement tons, i.e., 40 cubic feet per measurement ton)
- (4) Square loaded cargo (square feet).

It has been determined during the course of this study that no constraint exists for either personnel or bulk fuel. These lift requirements are therefore excluded from the following analysis. The lift requirements of interest are bulk cargo and square loaded cargo. Based on ship loading techniques currently in effect, the Constrained Cargo Factoring Model loads bulk cargo and square loaded cargo separately into the spaces of assault shipping. The model permits loading of bulk cargo into square spaces by a conversion factor that assumes bulk cargo will be stowed two pallets high (or 80 inches). No square loaded items are loaded into spaces designated for bulk cargo. Broken stowage factors of .8 for bulk and .75 for square are assumed for the model. When preloading boats of the Assault Craft Unit, Naval Beach Group, with square loaded items, a broken stowage factor of .65 is assumed.

When considering a reduction of materiel from units, it is necessary to plan the reduction from precise cargo categories. Reductions must be made from bulk cargo separately, as distinguished from square loaded cargo, although these categories are not necessarily independent from the viewpoint of unit integrity. Variable parameters controlling model operation provide a means of interreacting the reductions of bulk and square loaded cargo. This effect will be explained later.

There are two methods of reducing unit lift requirements. These are a reduction in the unit T/E and the reduction of DOS determining mountout. It should be pointed out that these reduction methods assume

that the planning factors specifying mountout for 1 DOS will remain constant. Examining bulk cargo reveals that reductions will have to be made from supply classes II and VII nonsquare, which comprise the unit's T/E, and/or by reducing the DOS of nine classes of supply from 15 DOS of mountout. For square loaded cargo, reductions must occur for class VII square loaded T/E items and by reduction of DOS for mountout affecting only supply class VII square. The rationale for the procedure of employing this model is contained in Section VI of this report.

The Constrained Cargo Factoring Model is a simple mathematical procedure that uses lift data for individual units to factor the lift requirement provided as input into categories which represent the specific materiel that is logically reduced when a unit is not able to load all of its materiel into assigned assault shipping spaces. The model applies a specified constraint to the total cube of the unit's T/E, i.e., effects a percentage reduction, loads the ship with the reduced T/E requirement, reduces the DOS of bulk mountout (if specified), loads the mountout, repeats this process for each unit, determines if the assault shipping is available, and generates a short fall or an excess. The model also performs the same functions for square loaded cargo.

For each constraint, the model provides a list of all units containing the original bulk and square and the cargo values permitted under the active constraint. If the model determines that an excess of square storage space exists, it reallocates the excess square to bulk space and reloads the units.

This appendix provides a mathematical explanation of the model. It must be understood that the model is a subsystem of CALAS and does not function in isolation. It primarily provides the data for the Constrained T/E Embarkation Analysis Model, which determines the optimal mix of the T/E under constrained loading conditions.

#### II INPUT

There are three input sources for the Cargo Factoring Model. This paragraph presents an explanation and notation to be used in defining the model input. The principal input sources are:

- (1) The movement requirement comprised of bulk and square loaded cargo
- (2) Cargo factor file
- (3) Amphibious assault ship lift characteristics.

A variety of values for the constraints are required inputs, but are changed as desired by the user.

Appendix D provides an explanation of the source of the cargo movement requirement that are input to the Constrained Cargo Factoring Model. That input was defined for the AE to be:

$$L = \sum_{j=1}^{M} \sum_{i=1}^{N_{j}} a_{ij} x_{i} + d_{u} \sum_{k=1}^{q} f(a_{k}) j$$

$$+ (d_{a} - d_{u}) \left[ \frac{\gamma}{(1 - \sigma)(30 - d_{a})} + \frac{(1 - \sigma)}{(d_{a} - d_{u})} \right] \sum_{k=1}^{p} T_{k}$$
(1)

for bulk cargo, and

utier File :

$$S = \sum_{j=1}^{M} s_{ij} z_{i} + d_{u} \sum_{i=1}^{N_{j}} c_{i} s_{ij} z_{i}$$

$$+ \frac{(d_{a} - d_{u})}{(1 - \sigma)(30 - d_{a})} \sum_{\ell=1}^{P} s_{\ell}, \qquad (2)$$

 $f(a_k)_j$  = a function in the MAGTF Program computing the cube of mountout for the kth class of supply for the jth unit for d=1

 $d_a$  = the DOS for the AE

 $d_{u}$  = the DOS for mountout

a = allowance of 1th TAM item of the i unit

 $x_i$  = cubic feet of the ith TAM item

Y = proporation of mountout computed for the first 30 DOS

 $\sigma$  = adjusting factor for mountout computations for DOS  $\geq$  30

s = allowance of ith square loaded item
for jth unit.

Equations (1) and (2) show how the movement requirement is determined from the F-2 JOPS card. The values for L and S can be written:

$$S_{i}, L_{i} = (T/E \text{ equipment}) + d_{a} \text{ (mountout for 1 DOS)}$$

for the jth unit, or

$$L_{j} = \sum_{i=1}^{N_{j}} a_{ij} x_{i} + d_{i} \sum_{k=1}^{q} r(a_{k})_{j},$$
 (3)

and

$$S_{j} = \sum_{i=1}^{N'_{j}} s_{ij} z_{i} + \frac{d}{d} c_{i} s_{ij} z_{i}, \qquad (4)$$

where

c = combat active replacement factor
 for 30 DOS.

The movement requirement for each unit of the AE is available for input to the model by a card file in the format of the type 9 card used by the TFE Model. A description of this format can be found in the "FMF TFE Users Manual." The same card is used in both the TFE and Constrained Model's computer programs. The essential data elements are:

- (1) Bulk cargo in measurement tons
- (2) Square loaded items in square feet
- (3) Personnel
- (4) Bulk fuel in barrels carried in a miscellaneous cargo category field.

Only the bulk and square loaded cargo categories are used by the Constrained Model.

Since the automated data mode available to the model is in the configuration for loading of ships, i.e., bulk and square loaded cargo, it is necessary to factor the cargo requirements into other cargo categories, thus facilitating the systematic and logical reductions for each unit. Basically, the cargo must be factored into T/E and mountout, permitting the application of a constraint to the T/E and a reduction to the DOS for mountout. Additionally, it was necessary to have supply classes II and VII of mountout factored in order to permit an investigation of the effect on amphibious lift short fall of applying a different combat active replacement factor to mountout calculations. The following variables are provided by factor cards which are used to conduct factoring operations within the model:

t = T/E items in measurement tons (MT)

 $T_{m}$  = Mountout supply classes I, V, VI VII, IX in MT

L\_ = Total bulk cargo from MAGTF listing

t = Mountout supply classes IIW and VIIW in square feet

t = Initial issues, plus 90 days mountout supply class VIIA in square feet

t = Initial issues, plus 90 days mountout supply classes IIA and VIIA nonsquare in MT

b = Bulk fuel in cubic feet

L = Supply class IX part of unit materiel in MT

L = Supply class IX computer for equipment in the unit but carried by third and fourth echelon maintenance units.

A factor card is available for each complete unit in the AE. The card contains values for each factor shown above, obtained from MAGTF listings. It should be noted that the detailed application of constraints to unit cargoes would not be possible without the specific cargo categories provided by the MAGTF Program. It was assumed that detachments are prepared for deployment containing only essential equipment. No constraints are applied to these units and no factor cards were prepared.

The cargo capacity provided by the amphibious assault ships has been made available to the model by a card image file. There are two cards for each ship in the force designated to lift the AE of the MAF. The format of this card file is the type 8 input card of the TFE Program. These cards serve as input to both the TFE and Constrained Cargo Factoring Model's computer programs. The essential data elements on the cards required by the constrained model are:

- (1) Bulk capacity in measurement tons
- (2) Personnel capacity
- (3) Square loading capacity in square feet
- (4) A miscellaneous capacity that may be designated a lift capacity such as bulk fuel or containers.

A description of the card format can be found in the HQFMF Pac "FMF TFE Users Manual."

#### III CARGO FACTORING PROCEDURE

The procedure used in this study to factor unit cargo into categories in order to apply constraints would not be used in a permanent computer assisted decision aid interactive system. The specific cargo categories needed to factor the movement requirement are available in the MAGTF Program in automated form after a unit has been processed. These values are included in the current unit listing generated from the program. A program change would be required to generate an output file on tape, disk, or cards, as desired, for use in the Constrained Cargo Factoring Model. This modification would eliminate the manual interface with the CALAS system now required to factor the cargo data. This MAGTF modification requirement was not identified prior to the last processing of the MAF. The time delays and additional costs that would have been generated by the modification did not justify the effort for the current study.

The procedure used herein is based on calculating the proportionate parts, as factors, of both bulk cargo and square loaded cargo for each cargo category, and applying these factors to the movement requirements generated by the TFEIN program, as explained in Appendix D. The scheme used is to factor the cargo totals into their parts, apply the constraints, and sum the reduced parts—thus obtaining the reduced movement requirement. The following notation will be used in the computing relationships presented below.

Let:

L = Bulk cargo obtained from MAGTF listing corrected for supply class IX, supporting and cubic feet of bulk fuel  $T_{mc}$  = Proportion of bulk cargo pertaining to mountout

 $\tau$  = Proportion of supply class VIIA square used for IMA for the aviation unit

 $\sigma$  = An assigned constraint. The value is defined to be the proportion of the T/E to be loaded, i.e.,  $\sigma$  = 1. There is no reduction. If  $\sigma$  = .8, a 20% reduction occurs

 $\delta$  = Proportion of supply class IIA and VIIA nonsquare included on OMA for an aviation unit

Type = Proportion of supply class VIIW square contained in mountout

d = A variable DOS for reducing the mountout within a
 units material

 $\gamma$  = A corrective factor for adjusting the combat active replacement factor.

Then:

$$L_{mc} = L_{M} - L_{S} - b_{f}, \tag{5}$$

providing an adjusted total bulk cargo. The relationship for the factored bulk cargo then becomes:

$$L' = \left(\frac{Lt_{e}}{L_{mc}} - L_{s}\right)\sigma + \left[\frac{(T_{m}^{-L}s^{-b}f) + t_{s}Y}{\frac{d_{a}L_{mc}}{a_{mc}}}\right]Ld_{v}$$

$$+ \frac{\delta t_{e}L}{L_{mc}}.$$
(6)

The first term of equation (6) factors the T/E items of cargo from the total bulk cargo obtained from the TFEIN Program and applies the constraint  $\sigma$ . The second term factors mountout from the bulk cargo by first removing class IX cargo carried by third and fourth echelon maintenance units and cubic feet of bulk fuel. Then supply classes IIW and VIIW are factored separately in order to apply the adjusting quantity

for a new combat active replacement factor. The variable d<sub>V</sub> is also present to adjust the DOS for the AE if desired. The third term of equation (6) factors supply classes IIA and VIIA separately in order to remove from the AE IMA support from aviation units having aircraft. Also this portion of the cargo is unaffected by DOS. This procedure assumes IMA support will be provided by the LHA and LPH until arrival of the AFOE. The IMA factor can be set to one to include IMA with the AE if desired.

For square loaded items:

$$S' = \left[ (S-t_{as})(1-\Pi) \right] \sigma + \underbrace{(S-t_{as})}_{d} \Pi d_{u} + t_{as} \delta.$$
 (7)

In this equation the first term is the square loaded T/E items with the constraint  $\sigma$  applied. The second term is the portion of the total square contained in mountout. The value d provides the option of reducing the DOS for mountout of square loaded items. The third term adds the supply class VIIA square loaded items. The value for  $\gamma$  was obtained by sampling three aircraft squadrons to determine the porportion of class VIIA square that is IMA equipment. The sample revealed that  $\gamma$  was zero, indicating that all square loaded items are IMA and will not be included in the AE.

#### IV APPLICATION OF CONSTRAINTS

Having developed the cargo factoring procedure that permitted the application of constraints on the T/E, the model has been designed to weight the application of those constraints on the units of the AE. The weighted constraints are applied in a manner that indicates the sensitivity of the contribution of T/E items affected by the constraint to the accomplishment of the unit's mission and the mission of the AE of the MAF prior to arrival ashore of the AFOE about D+3 to D+7. Three different weights are applied. These different values for the constraints are computed as a function of one assigned value for the overall constraint. The weighted values are termed light, medium and heavy. The light constraint is defined to be one-half of the overall constraint; the medium constraint is equal to the overall constraint; and the heavy constraint is one and one-half times the overall constraint. Equations for these calculations are:

Light

$$\sigma' = .5(1 + \sigma) \tag{8}$$

Medium

$$\sigma' = \sigma$$
 (9)

Heavy

$$\sigma' = 1.5\sigma - .5.$$
 (10)

The assignment of weights to units can be found in Section VI.

Experience with this model gained from loading the AE of the MAF into the available shipping has revealed that, as a result of a smaller short fall of square loaded cargo than for bulk, a tradeoff exists

between the square and bulk cargo derived from obtaining additional bulk space by converting square space to bulk stowage resulting from applying constraints to square loaded items. The rationale for the application of this tradeoff is found in Appendix F. The model, therefore, provides a feature which converts unused square stowage space by the assumption of stacking bulk cargo two pallets high, computed by:

$$L_{cs} = \frac{80 f_{bb} S_{u}}{12 f_{bb}}, \qquad (11)$$

where

L = Converted square space to bulk

f = Broken stowage factor for bulk, i.e., .8

 $f_{bs}$  = Broken stowage for square, i.e., .75

S = Excess square space.

This procedure is commonly used by Marine Corps embarkation planners and can be found in FMFM 4-2. (This reference uses 72 inches for the planned conversion.)

The procedure for computing the percent short fall used in the graphs of Section VII is to obtain the difference between the ship capacity and the constrained cargo in measurement tons, divide by the constrained cargo, and multiply by 100. The graphs are plotted as a function of the weighted constraints.

Let

C = capacity of the ith ship in square

Cp; = capacity of the ith ship in bulk

 $B_i$  = bulk of the jth unit less T/E items

b = bulk T/E of the jth unit

S, = square cargo of the jth unit less the T/E

 $s_{+}$  = T/E square of the jth unit

σ = weighted constraint

v = conversion factor for square to bulk

m = number of units

n = number of assault ships

P<sub>SF</sub> = Percent short fall, then the percent short fall is computed by:

$$P_{SF} = \begin{cases} 100 \left[ \sum_{i=1}^{n} C_{Bi} + \left( \sum_{i=1}^{n} C_{si} - \sum_{j=1}^{m} S_{j} + \sigma S_{tj} \right) v - \sum_{j=1}^{m} B_{j} + \sigma b_{tj} \right] / \sum_{j=1}^{m} B_{j} + b_{tj} \\ ; \left( \sum_{i=1}^{n} C_{si} - \sum_{j=1}^{m} S_{j} + \sigma S_{ij} \right) \ge 0 \\ 100 \left[ \sum_{i=1}^{n} C_{Bi} - \sum_{j=1}^{m} B_{j} + \sigma b_{tj} \right]; \left( \sum_{i=1}^{n} C_{si} - \sum_{j=1}^{m} S_{j} + \sigma S_{tj} \right) \le 0 \end{cases}$$

$$(12)$$

The graphs are plotted with  $P_{SF}$  versus  $\sigma$  from equation (12).

#### V COMPUTER PROGRAM

A computer program was written to perform the cargo factoring operation, apply the constraints to the T/E (or change the DOS for mountout), and perform the ship loading operation. The same operations must be performed on each unit of the AE, after which amphibious lift status is available for the ships contained in the input deck. This program has been labeled AMPSF. It is part of CALAS, as presented in Section VI of this report. The present section presents an explanation of a generalized flow chart of Program AMPSF. As explained in Section VII-F, the form of the Constrained Cargo Factoring Model, as it would be implemented in the FMF of the 1980s, would be different from the version developed during this study. If implementation of CALAS is required, computer documentation would be prepared at that time, describing the final version of all computer programs within that system.

## A. Main Program

Figure E-1 is the generalized flow chart for Program AMPSF. The following explanation refers to the flow chart. The program consists of two routines: a main program AMPSF and the subroutine CONST. Routine AMPSF is programmed to execute once for each constraint planned for the analysis. A Do loop is set up to provide the continued execution. Values for the constraints are provided to the program in an array by Data Statement. In order to have the program execute exactly the same for each constraint, the input file, consisting of the card input decks, are written to the disk by control cards and then attached to the program before execution. Rewinding the disk file containing the input data decks alone after each execution of the program then becomes possible.

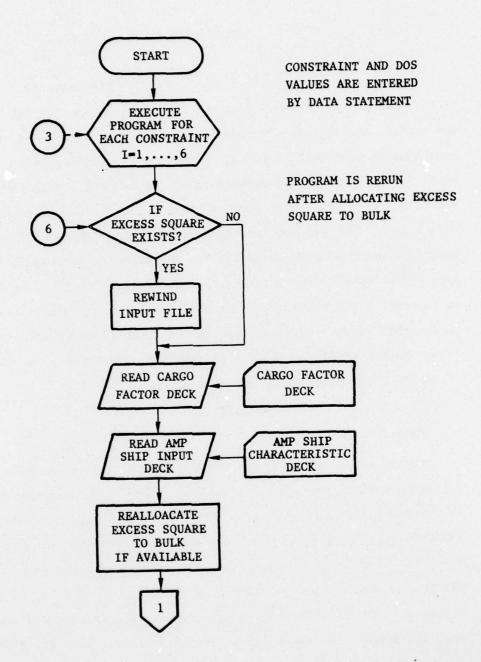
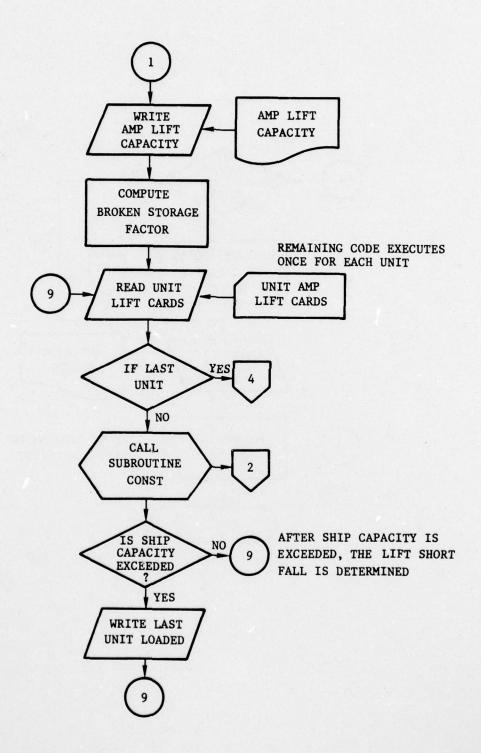
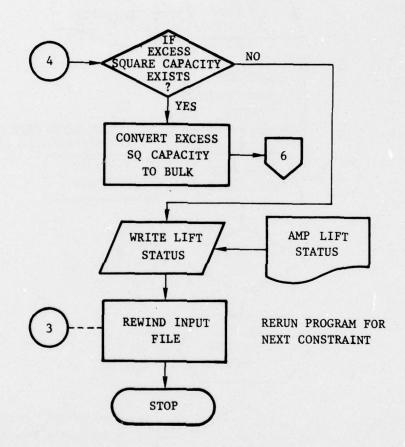


FIGURE E-1. PROGRAM AMPSF





STANFORD RESEARCH INST MENLO PARK CALIF NAVAL WARFAR--ETC F/G 15/5
MATERIEL WEIGHT AND CUBE CONTROL (1975-1980).(U)
MAR 76 T H ALLEN, R B RINGO N00014-75-C-0708 AD-A041 598 NL UNCLASSIFIED 6 OF 7

The program also reexecutes by rewinding the input data files after reallocating excess square cargo capacity to bulk while processing the same constraint. Control is passed to entry point 6 on the figure for this purpose.

The cargo factor deck is read into an array and placed in common, providing a look up table for each unit in the AE to Subroutine CONST. The Amphibious Ship Characteristic Deck is read by the program, permitting the bulk and square loading capacity totals to be obtained. These totals are modified on those runs where reallocation of square to bulk took place. The total square used becomes the square capacity, and the converted additional bulk space from the excess square is added to the previous total bulk. The lift capacity for each ship in the deck is written to output. The format for these cards and the data contained thereon are the input to the TFE Program. Only two of the many fields on this card are used by this program. The dual use of these cards, however, adds a greater dimension to the analytical effort. The broken stowage factor for bulk and square is then applied to the total lift capacity.

At this point the program reads the unit movement requirement deck and executes the next section of code, once for each unit. After processing each unit, control is passed to entry point 9 after completely processing each unit. Control is passed to entry point 4 after the last unit card is processed. When a unit card is read, Subroutine CONST is called passing control to the entry point on Figure E-2.

After each unit is loaded into the ships, a check is made to determine when the total ship capacity is exceeded. A message is written to output indicating which unit was the last to be loaded and the materiel of that unit not loaded, if any. If lift capacity is not exceeded for the unit being processed, control is passed to 9, and a new unit card is read for processing the next unit.

After the last unit is processed, control is passed to four, and a check is made to determine if excess square exists in ship capacity.

When this occurs, a conversion of the excess square to bulk takes place, and control passes to 6, where the program will be rerun entirely for the same constraint value after adjusting the lift capacity for the converted excess square. An excess square condition can occur only once for the same constraint. On the second pass through the program for the converted square, the program bypasses the conversion routine, writes the lift status, and rewinds the input disk file. At this point, control passes to 3 since the end of the Do loop is encountered. The program is ready to execute again for the next constraint. When the last constraint run is completed, program control passes out of the Do loop and processing terminates.

### B. Subroutine CONST

In Figure E-2, Subroutine CONST receives the bulk and square cargo requirements for the unit being processed from the parameter list. The cargo factor lookup table is provided by common storage arrays. An additional array is provided to CONST, permitting the recalculation of supply classes IIW and VIIW mountout from a modification factor for the combat active replacement factor (CARF) used in mountout calculations. This data is provided by a DATA Statement. When a modified CARF is desired, a flag is set, permitting a change in mountout for classes IIW and VII as each unit's data is processed.

The first operation is to find the unit pasced to the subroutine in the cargo factor lookup table. When the unit is found, a code is obtained identifying the unit as a detachment or a complete unit. The cargo for the detachment is not constrained, so the program conducts the loading calculation and returns control to MAIN.

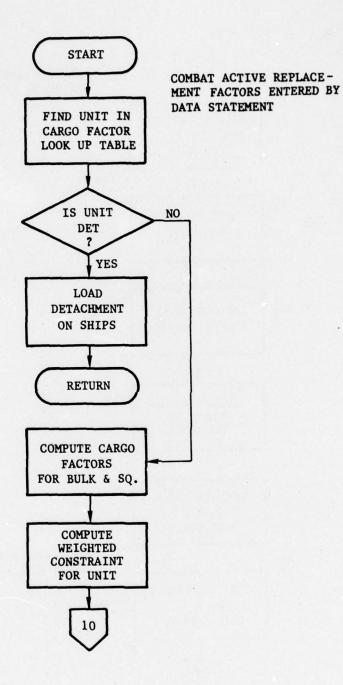
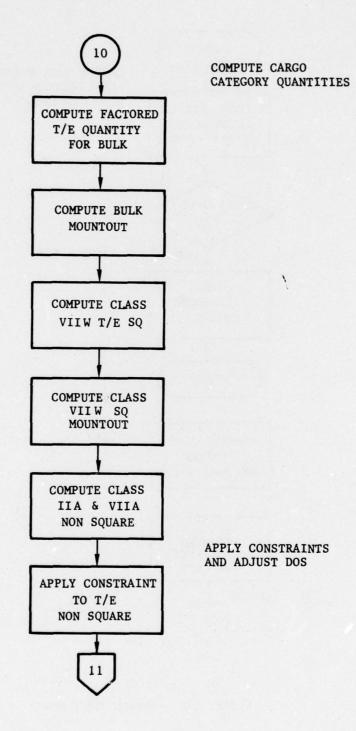
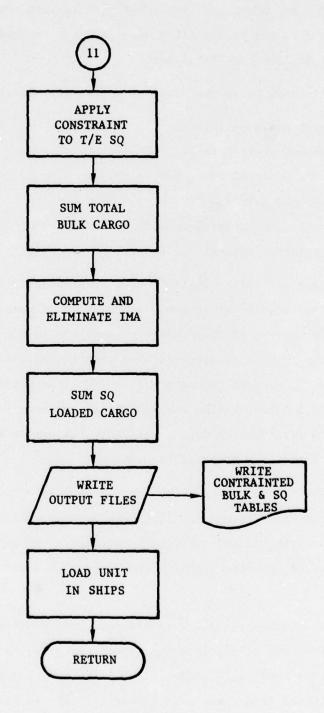


FIGURE E-2. SUBROUTINE CONST





For complete units, the cargo factors are computed for bulk and square, T/E, and mountout. The constraint is then computed, based on a code found in the lookup table providing the assigned weight to the constraint for the particular unit.

The factored cargo quantities are then calculated for:

- (1) T/E materiel in bulk
- (2) Mountout in bulk
- (3) T/E materiel in square
- (4) Mountout in square
- (5) Aviation materiel in bulk
- (6) Aviation materiel in square.

With the factored cargo available, the constraint is then applied to T/E materiel in bulk and square. A provision is made in this routine to limit the amount of the constraint applied to T/E square loaded items. This feature is required when interfacing the square feet of the unit's T/E reduced to the specific TAM items eliminated by the Constrained T/E Embarkation Analysis Model of Appendix F. When processing a troop list through CALAS, the limit feature on applying constraints to square loaded T/E materiel is frequently used.

The DOS for mountout may be changed as well by entering a different value in the DATA Statement of the main program. This value is passed to the subroutine in the parameter statement. Unless a new value for DOS is entered, mountout remains unchanged in the processing within the subroutine.

Supply classes IIA and VIIA nonsquare are modified to factor IMA materiel from the totals in these categories. The amount to be included in the unit's total bulk cargo is OMA materiel. The IMA materiel is also eliminated from class VIIA square. It should be noted that MAGTF data includes IMA materiel with squadrons having the aircraft, thus

justifying this material for the H&M squadron. In actual practice, the H&M squadron would hold this IMA material, and therefore the removal of this material to the AFOE would be from H&M squadron material.

After all the adjustments to factored cargo are completed, the total bulk and square to be loaded for the unit is summed, and the loading operation is conducted. A table is written to output, listing each unit's input and adjusted cargo values used in the loading operation. This table is input via a manual operation to the Constrained T/E Embarkation Analysis Model. The subroutine then returns control to the main program.

Appendix F

CONSTRAINED T/E EMBARKATION MODEL

Part 1: Narrative Description

## Appendix F

#### CONSTRAINED T/E EMBARKATION MODEL

## Part 1: Narrative Description

## I BACKGROUND

Each standard military unit in the Marine Corps has a prescribed Table of Equipment (T/E) detailing the equipment it is authorized to maintain. The ability of a unit to perform its function(s), is predicated on the availability of the major items of equipment listed in its T/E. Under conditions of commander's judgment, climate, intensive combat, etc., addenda are permitted. The discussion that appears in this appendix is limited to the standard T/Es of basic Marine Corps units.

During the planning stage prior to an amphibious operation, each basic unit brings its complement of equipment up to the authorized strength (if it is not so already) by requisitioning the items in short supply. However, if it is known during the planning phase that shipping space will be insufficient to carry the entire full strength T/E, some of the unit's equipment will have to be left behind in the assault echelon phase of the operation. Listings showing the equipment that can be carried by the assault echelon under space constraints should be prepared during the planning phase.

The standard T/E assumes that there will be no shortage of shipping space in which to load the authorized equipment; but if there is such a shortage, two problems arise: (1) can the operation be successfully mounted; and (2) what part of the full strength T/Es should be carried by each unit in the assault?

Thus, the problem addressed in this appendix is: given that shipping capability is limited by a fixed constraint (cube or square) for an amphibious operation, what is the optimum T/E that should be loaded? It follows that when there is a volume or square constraint on shipping, the objective is to minimize the loss in efficiency caused by the decrease in equipment and supplies.

#### II METHOD OF APPROACH

## A. General Description

When the available shipping space for an entire MAF is inadequate for loading the T/O or T/E for that MAF, the first step in the solution of the problem is to allocate reduced shipping space among the various units that make up the MAF. The method by which the available shipping space is allocated is discussed in Section VI. For the purposes of the Constrained T/E Embarkation Analysis Model (CONTEAM), it is assumed that, for each military unit, a known amount of cube and square storage is given. The problem remaining is the optimal allocation of this scarce space.

For this model, only the class II and the class VII TAM items that appear in the unit's T/E are constrained. If this procedure is unpalatable, the constraint can theoretically be applied to any other class(es) of supply. This procedure produces a concrete, pared down T/E that is smaller than the standard published T/E for a unit. Thus, an operations officer can examine the curtailed T/E, see what would be missing from the assault echelon phase, and determine by how much the efficiency of the assault phase is decreased by the constraint.

To summarize, this appendix describes in detail the method of computing a pared down or constrained T/E for a given unit under square and cube constraints.

The output from the CONTEAM model shows for each unit's T/E the class II and class VII TAM items to be omitted from the assault echelon and to be carried by the follow-on echelon or later replenishment phase.

# B. Rationales for Computing Constrained T/Es

Two different rationales were examined for computing constrained T/Es. The first rationale fills the available space with T/E items (TAMs) according to their importance to the unit--in other words, every unit of every TAM competes with every other unit of the same and other TAMs.

In the second rationale, the constrained space is further constrained by first filling part of its space with a "skeleton T/E" that consists of those items that will be absolutely essential during the interval between the landing of the assault echelon and the arrival of the follow-on echelon. The balance of the space is then filled according to the previous logic.

## C. The Minimum Strength T/E that Can Support a Unit

Philosophically, it is interesting to debate the viability of a unit equipped below authorized strength. Actually this problem is one that is debated in real time by military planners—not by a research organization or a debating society. The output from the CONTEAM model simply shows the equipment to be taken, as well as the equipment to be left behind, for a unit with constrained loading space and leaves to the operational staff planning the operation the decision of whether or not the equipment allocated to this space is sufficient.

## D. The Assignment Priority List

For the exercise of constructing a constrained T/E, one of the key devices is the assignment priority list. This list shows the value of each unit of each item (TAM) to operational readiness. If cube is the limiting factor, then clearly two items of the same volume, the same consumption rate, and the same criticality rank equally. As between two items

with identical criticalities and usage probabilities, but with different volumes, the item having the smaller volume is the more valuable since it puts a smaller strain on the constrained storage. It can even be shown if their volumes are sufficiently disparate, it may be advantageous to load several units of one item and no units of another, even though the items are identical in criticality and are equally likely to be utilized.

The logic upon which this seemingly paradoxical conclusion is based is the following. Usage rates are not determinative, but are stochastic. In other words, there is a finite probability that no units of either item will be utilized; and also a probability that more units of the plentiful item will be utilized than are loaded. Since a penalty will have to be paid if either item is short, we have the choice of chancing a shortage in one or both. This finite chance always exists. By deliberately increasing the odds of a shortage in one item, we are then able to stock enough units of the second item to reduce its odds of being short to a very low figure. Since we cannot avoid the finite probability of being short in both items, it can be advantageous to load no units of one of the items, even though that item has an expected usage rate of one per day.

Thus far the philosophy behind the construction of the priority assignment list has been described, but not the actual method of constructing the list itself.

## E. Construction of the Assignment Priority List

The priority assignment list is a ranking showing the added benefit or advantage that accrues from having on hand each additional unit of each TAM item. Considering the penalties to operational readiness, the first unit of each TAM item is more important than the second unit of

the same TAM item; the latter is more important than the third unit of the same TAM item, etc. The reason for this is that there is a chance the first unit will be needed, while the second unit will either not be needed, or will be used for a less critical mission. Hence, the first unit protects more by itself than does the incremental protection purchased by the addition of the second unit, presuming the first unit is already on hand.

Again considering the penalties to operational readiness, the second, or even the third or fourth unit of one TAM item may be more important than the first unit of another item of the same criticality. The measure of importance or protection is the amount of operational readiness afforded per cubic foot or per square foot of storage space. It is at this point that the constraint of limited storage space makes its influence felt. What is being pursued is the maximum amount of protection or operational readiness per cubic foot or per square foot of storage space.

It must be emphasized that, if there is no limit on the resources to be loaded for the assault echelon, there is no problem to contemplate. Constraints on the T/Es, due to the lack of shipping availability, lie at the heart of the problem.

Previously, the value of a unit was defined as the <u>incremental</u> <u>protection afforded per cubic foot</u> or per square foot for that unit. The meaning of "per cubic foot" or "per square foot" should be clear; now the meaning of "incremental protection afforded" by that unit can be explained.

Attention is fixed on a particular TAM item. The incremental protection afforded by the first unit of that TAM item is simply the probability that that item will be needed for its highest function. For the second unit of the same TAM item the incremental protection afforded by this unit is the probability that exactly two units are needed, less

the probability that exactly one unit is needed. The incremental protection afforded by the third unit is the probability that exactly three units are required, less the probability exactly two units are required. And so on for the fourth, fifth, and subsequent units.

These individual probability terms depend, in turn, on the probability distribution for the TAM item in question. The distribution is determined essentially by historical experience.

For a large class of TAM items, the probability distribution is well represented by a Poisson distribution, the terms of which are easily calculated once an average demand is known.

For an item with mean demand (or expected need) exceeding 4, the demand distribution was assumed to be (truncated) normal, with mean a and variance a.

For each item, then, the incremental probability advantages are computed, multiplied by the item's criticality and divided by the item's cube (square). The sets of numbers so obtained are sorted, and the final priority assignment list might look as follows:

<u>Item</u>	Unit	Number
1		1
1		2
2		1
3		1
1		3
2		2
1		4
3		2
4		1

This table shows, for example, that the first unit of item 3 is more valuable per cubic foot than the third unit of item 1, but less valuable than the second unit of item 1.

# F. Disadvantages of the Above Algorithm

If TAMs are added to or removed from a T/E, the entire assignment priority list must be resorted. Even if a single T/E quantity for a TAM changes, a complete resort is necessary. A more serious difficulty comes from the fact that the incremental values must be computed for a very large number of units of each TAM; thus, the number of entries (TAM no.--Unit no.) to be sorted can be very large even for a T/E of modest size.

# III AN ALTERNATIVE METHOD OF COMPUTING AN ASSIGNMENT PRIORITY LIST FOR A CONSTRAINED T/E

The main logic of the alternate method of constructing an assignment priority list for a constrained T/E is quite similar to the logic used in Volume II of the SRI/NWRC report, "Pre D-Day Fleet Marine Force Materiel Requirements Determination and Distribution System (1975-80)." Detailed flowcharts appear in that reference.

First a spectrum of trial values of the parameter LAM (the Lagrangian parameter  $\lambda$ ) is taken. The trial values of LAM should be in the neighborhood of the reciprocal of the largest T/E quantity. Since it is not at all burdensome to make simultaneous calculations for as many as twenty-five different values of LAM, one can assign several starting values of LAM on either side of the reciprocal of the largest T/E quantity.

Next, for each value of LAM, and for each TAM item, the optimal number of units to be included in the "constrained T/E" is computed according to the procedure described in the "Pre D-Day" study.

As the calculations proceed from one TAM to the next, cumulative totals for cube (square) are kept in a running fashion for each of the values of LAM. At the termination of this phase of the calculations-i.e., when all TAMs have been processed--there will be a set of up to twenty-five tentative constrained T/Es, one for each of the twenty-five starting values of LAM. In general, the number of units shown for each TAM will be a fraction. It is assumed in the preliminary calculations that each TAM is divisible. This device is a convenient fiction to make it possible, in the next step, to enable a more accurate interpolation for a new value of LAM which will allow us to more accurately obtain the target constraint.

It can happen that one of the starting values of LAM gives a constrained T/E that is close to the specified cube (or square). With a minor final adjustment, the computation is then finished.

If (on the other hand) none of the starting values of LAM gives a constrained T/E that is reasonably close to the preassigned square or cube, further computation is required. Ordinarily, this is easy. There will be two values of LAM that result in T/E's that bracket the desired constrained T/E. Several new values of LAM can then be chosen (between the two values last mentioned). The entire process just described can be repeated until a satisfactory constrained T/E is obtained.

#### IV EXPRESSING UNIT OPERATIONAL READINESS

By assigning a weight (or importance) to each item of equipment of a unit, a measure or index of operational readiness can be calculated that is oriented toward the unit's operational function(s).

In this study readiness is estimated by assigning a weighted value to each priority category of equipment. For this procedure designate:

c<sub>h</sub> = criticality of a high-priority item = 8

 $c_m = criticality of a medium-priority item = 4$ 

 $c_1$  = criticality of a low-priority item = 2

c = criticality of a non-priority item = 1

and

 $q_h$  = quantity of a high-priority item

 $q_{m}$  = quantity of a medium-priority item

 $q_1$  = quantity of a low-priority item

q = quantity of a non-priority item

Thus overall readiness, OR, can be expressed by

OR = 
$$\frac{q_h^c_h + q_m^c_m + q_1^c_1 + q_n^c_n}{q_h^c_h + q_m^c_m + q_1^c_1 + q_n^c_n}$$
 (for constrained T/E)

or

OR = 
$$\frac{8q'_h + 4q'_m + 2q'_1 + q'_n}{8q'_h + 4q'_m + 2q'_1 + q'_n}.$$

The weights should be assigned by operational judgment. In this study the weights were assigned as 8,4,2,1 running from the highest - pricrity items according to importance to their unit's mission.

For a given T/E and unit, multiplying the quantity (density) of each item of equipment by its weight (criticality) and summing the products will give a value that indicates full or maximum readiness for that unit. If for some reason the T/E must be constrained by lack of shipping, availability of T/E items, etc, the quantities that can be shipped or that are available can be multiplied by their weighting factor and after summing the products the value of readiness obtained can be compared against that value of readiness obtained from a 100% filled T/E and expressed as a percentage.

For study purposes three readiness indexes were calculated for each unit: (1) An index for square loaded items, (2) an index for cube loaded or bulk items, and (3) an overall index for all items of a unit.

The overall OR index gives the capability for examining important trade-offs. As an example, take an M1038 Infantry Battalion. Suppose only 91% of the required square is available for square-loaded items, and 64% of the required cube is available for bulk loaded items. By using the Constrained T/E Embarkation Analysis Model, a preliminary constrained T/E is computed. The OR index for this constrained T/E turns out to be 85.05.

Now suppose for the same unit the square is further constrained to 85% of the square required to load the entire T/E for M1038 and let this reduction in square be reallocated to increase the loading capacity for the units bulk cargo. By the usage of the CCF model, it is shown that this trade-off (increasing the amount of square stowage that is left unloaded from 9% to 15%) increases available bulk cargo loading space from 64% to 75%.

To determine if this reallocation is beneficial, the Constrained T/E Embarkation Model is again employed and an Operational Readiness Index of 87.73% is computed.

Therefore it can be deduced that by reducing the square loaded from 91% to 85% and reallocating this space to bulk cargo, an increase in Operational Readiness from 85.05 to 87.73 results.

The logic of the Operational Readiness Index is impeccable if one is willing to admit that the shortages can be ranked in importance; e.g., a shortage of paper towels is not equivalent to a shortage of generators, even though both shortages do cause trouble. By assigning a weight or criticality to each item of a T/E, we can assign a measure of how painful a shortage of an item is to a unit. Each shortage of an item decreases the efficiency of a unit and it is precisely this loss of efficiency that the Operational Readiness Index measures.

#### V EXPRESSING CRITICALITY

There is no generally agreed upon measuring rod of criticality. Perhaps this is because criticality is difficult to measure. Criticality of a particular item varies with the combat or support situation. Evaluation of the importance of a given piece of equipment can even vary between two officers trained in the same field in assessing the relative criticality of various pieces of equipment, weapons, or repair parts.

It is necessary to point out the connection between "criticality" in the sense of "combat critical" and the other meanings of the term. These additional meanings include the following:

#### Procurement Lead Time

If a piece of equipment, say a turbine, a generator, or special purpose gasoline-powered motor, can be procured only with difficulty from one source (manufacturer), more attention must be paid to transporting, ordering, supplying, and deploying this item than in the contrary situation.

#### Distribution Time

Items that require a particularly long packing, processing, or distribution time are critical in another sense. Extremely fragile and medical supply items are examples of items that might require special handling.

#### Relative Dependence

There is a certain relativity of criticality between certain pairs of items. Film or blood plasma cannot be stored without a refrigerator. Ammunition is useless without a weapon. Sophisticated weapon systems may be ineffective without aircraft spotters. Thus it can be seen that the criticality of one item can be dependent on the availability or non-availability of a second item.

It is assumed that criticality is greater for the first few units of an item than for the last few units of a given item. Thus, if a T/E requires 58 radios, and all radios are planned to be in use, we still might assume that the military unit will be functional with only 29 radios, even though the next 29 would also serve an important function.

Note that the rationale just explained is only that. It is not intended to be a philosophical discussion of the <u>true</u> criticality of any one of the radios. All that is presented is a method of computation; a method that enables the production of a "constrained T/E." If the "constrained T/E" is not appealing to the planner, he is at liberty to change it according to his independent judgment. The computer program that utilizes this concept is to be thought of as only a first step in the planning process. If it does not produce a final result, at least it produces something of value as an intermediate result.

Lacking reports of a definitive criticality study, one can successfully assign criticalities if he bears the following in mind. First, successful management of many T/Es must be automated, at least in part. Second, automation is even more successful if criticality ratings can be assigned to items in a reasonable manner. Third, accuracy but not perfection in the assignment of criticality is required. Fourth, little success is achievable if every item is rated "highest criticality." Relative ratings must be given. Fifth, a system is more easily managed, and to that extent more efficient, if not too many items are given the highest criticality rating.

It must be remembered that all T/E items are "critical" in the lay sense of the word. An item is placed in a unit's T/E because it is valuable to that unit. The important function is to assign relative criticalities to each item within a T/E.

The Constrained T/E Embarkation Analysis Model is a useful tool in assisting the operational planning officer in assigning criticalities. By varying his criticalities for various items and studying the shortage lists, the planner will be able to adjust his assumptions to obtain results that improve upon his field experience. The user of the model will also learn that sensitivity of the model to variations in criticality ratings is greater for large items than for small ones.

If criticality has any meaning at all, it should be taken into account in the "constrained T/E" logic. To place insufficient emphasis on criticality is to decrease operational readiness.

#### VI ASSIGNING CRITICALITY

#### A. Introduction

The importance of an item of equipment to a unit's mission can be derived by relating its usage to specific functions of the unit and, in turn, determining the relative importance of the specific functions to the unit's combat mission.

For the purpose of this study each T/E item was assigned a priority that related to its importance to the unit's mission. Four categories or ranks of priorities were established:

- · High-Priority
- · Medium-Priority
- · Low-Priority
- · Non-Priority.

The scoring procedure for criticality was 8,4,2,1 from most critical to least critical. As between categories the scoring value is arbitrary, but for study purposes we assumed the items in the highest priority category are twice as badly needed as items in the second priority category and so on down the line. The relative pain of shortages is, therefore, 8,4,2,1. These figures can easily be changed without jeopardizing the rationale of our calculations. For example, certain weapons or super critical items can be given artifically high priorities so that the program always prefers them to other items.

# B. Item Usage Designation (Designation of Application of a Given TAM)

Before a criticality can be assigned a piece of equipment for a unit, it is necessary to relate each principal item (TAM) to a function, and in some cases more than one function, performed by FMF units. The twenty-two discrete functions that a unit may perform are listed below and described later in this appendix.

- 1. Infantry Combat Small Arms Employment
- 2. Fire Support
- 3. Fire Support Control
- 4. Mobility
- 5. Communications
- 6. Intelligence
- 7. Surface Transportation
- 8. Engineer Construction
- 9. Demolition/Obstacle Clearance
- 10. Supply
- 11. Maintenance
- 12. Cargo Handling
- 13. Service Support
- 14. Medical
- 15. Air Support Control
- 16. Power Generation
- 17. Ordnance Delivery
- 18. Air Control
- 19. Air Operations Support
- 20. Air Transport
- 21. Communications/Electronics Maintenance
- 22. Aviation Maintenance

Examples of this functional assignments are:

TAM	DESCRIPTION	FUNCTIONAL GROUP
A0240	CENTRAL OFFICE TELEPHONE	COMMUNICATIONS
A0380	COUNTERME ASURES SET	INTELLIGENCE
в0780	GENERATOR SET	POWER GENERATION
D0900	TRUCK, AMBULANCE	MEDICAL

For a complete catalog breakdown of all TAM items in the table of essential equipment (TEE) the reader may refer to Table F-1.

It should be noted that the criticality of the same TAM can vary depending on the military unit for which it is listed in the various T/Es. For example, if a unit has "communications" as one of its primary functions, and the TAM item is a radio or a telephone switchboard, the TAM is high-priority (8) for that unit. However, should another unit have "communications" as a secondary function, the radio or telephone switchboard would be assigned as a medium-priority (4) item.

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42, AN/TSC-42A
AN/TSO-54
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SET, AN/DRM-1A
SET, AN/DRM-47A
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POWER SUPPLY, PP-38&/U
RADAR SET, AN/TIQ-1
RADAR COURSE DIRECTING, CENTRAL
RADAR RELAY SET, AN/TXQ-3
RADAR SET, AN/TPQ-11
RADAR SET, AN/TPQ-31
RADAR SET, AN/TPS-22
RADAR SET, AN/TPS-23
RADAR SET, AN/TPS-37
RADAR SET, AN/TPS-48
RADAR SET, AN/UPS-10
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RADDAR SET, AN/UPS-10
RADDAR SET, AN/UPS-10
RADDAR SIG NATIONS-10
RADDAR SIG SIMULATOR, AN/UPM-9
RADDAR TEST SET AN/UPM-99
RADDO TEST SET AN/UPM-99
RADDO PACILITY GROUP, AN/RADDO RECEIVER AN/PRR-15
RADDO RECEIVER AN/PRR-15
RADDO RECEIVER AN/RA-16
RADDO SET, AN/GRC-129
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RADIO SET, ANYTRO-97, 24
RADIO SET, ANYTRO-97, 24
RADIO SET, ANYTRO-97
RADIO TERMINAL SET, ANYTRO-129
RECEIVER RADIO, R-39JURR
RECEIVER RADIO, N-39JURR
RECEIVER RADIO ANYGRA-9
RECEIVER RADIO, N-39JURR
RECEIVER RADIO ANYGRA-9
SHOP, ELECTRONIC, ANYGRA-3
SHOP, ELECT
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TACTICAL DATA COMMUNICATIONS CENTRAL AN/T
TELEGRAPH TERMINAL GROUP,
TELEPHONE EXCHANGE TRANS- PORTABLE LN/
TELEPHONE SET, TA-341/TT
TELEPHONE SET, TA-341/TT
TELETYPE EQUIPMENT KEPAIR
TELETYPE EQUIPMENT KEPAIR
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Table F-1 (continued)

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3D RAJAR DATA PROCESSOR GROUP AN/TYA-18
DATA COMMUNICATION GROUP AN/TYA-19
COMPATIBILITY COMPUTER GROUP AN/TYA-20
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DATA PROCESSOR GROUP AN/TYA-6
GEGRAPHIC DISPLAY GEN GROUP AN/TYA-7
OPERATOR GROUP AN/TYA-9
COMMUNICATIONS GROUP AN/TYA-12
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AIR CONDITIONER, MCS, HORIZON-
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KIT, MK-993/PRC-25

SET, ANGMH-56

SET, AN/UPH-64

SET, COMMUNICATIONS

SET, COUPLE CONTROL,

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BACKHJE, GRANE-SHOVEL, BAY

BACKHJE, MOD F-C-88-61

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TION AND SERVICING CONCRETE, SHIP LOAJE, TRLR 4TJ, 4 WH RELOCATABLE BULLOING ENERATOR, PU-499/U, 2.5 KH, EL TO ENERATOR, PU-359/U, 4 KH, EL TO TESTING KIT  WITE PRETATION SET, UNIT APHIC PRINTING AND PROCESSING SEC RSCTION TO COMPUTING SET TING ASSORTMENT, TING ASSORTMENT, TING ASSORTMENT, TO COMPUTING SET TO TOOL OUTFIT, AIR COMPACESSUE TING UNIT, PIESEL, FYSAMILL, TRLR 4TD SEMBLY, EXPECIENT REFUELER, FUGL CIPROCATING, MARLDH, 445 MUD-HCG CIRR GOUIPHENT SET, TOPOGRAPHIC, 7 ATTACHHENT, HHREE SHANKEAR MOUNTING, ATTACHHENT, HHREE CATON GOUIPHENT, HREE CATON GOUIPHENT, HREE CATON GOUIPHENT, HREE CATON GOUIPHENT,		IGH	8	2	0		101	1				,		•	
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ENERATOR, PU-365/U, L. KM, K. 10 %.  ENERATOR, PU-329A/U, 7.5 KM, 61 TO  UN TESTING KIT  NTERRETATION SET, TEAM  NTERRETATION SET, UNIT  APHIC PRINTING AND  PROCESSING SEC  APHIC SYSTEM COMBAT  ER SECTION  COMPLING AND  TING ASSORTMENT,  G AND COMPUTING SET  COMPCESSING SEC  TIOCOLOUTEIT, AIR  NIT, DIESEL, F/SAMMILL,TRUR MTO  SEMBLY, EXPECIENT  OTROCATING, MARLOM, 445 MUD-HCG  CIPROCATING, PRECH, 445 MUD-HCG  CIPROCATING, PRECH, F/SAMMILL,TRUR, MTO  NOT, SECON, 56 FT HEAD  ING UNIT, GARBON  RATOR UNIT, MARLOM, 445 MUD-HCG  CIPROCATING, MARLOM, 445 MUD-HCG  CIPROCATING, PRECH, MARLOM, AND  RATOR, DOINT, MARLOM, MARLOM, FI  RATOR, PREFAR, 1UC CU FT  ATTACHMENT, MHITE  CTION EQUIPMENT, MHITE  CTION EQUIPMENT, MHITE  CTION EQUIPMENT, MHITE  ATTACHMENT, HHRE  ATTACHMENT, HHRE  ATTACHMENT, HHRE  ATTACHMENT, HHRE  ATTACHMENT, MHITE  ATTACHMENT  ATTACHMEN	6	Z	A	œ	ā		66	)				1	ú	-	
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CABLE ASSEMBLY SET, ELECTRICAL-HAMK- AN/GSA-1
CARLE ASSEMBLY SET, ELECTRICAL-HAMK- AN/GSA-1
CARRESSOR, RECIPROCATING, POWER DRIVEN, F
COMPRESSOR, RECIPROCATING, POWER DRIVEN, F
COMPRIES, GUN DIRECTION, M18
CONSOLE, ASSULT, FC, GM, AN/TSM-4 SERIES
CONTROL BOX, GM LAUNCHING SECTION, AN/GSA
CONTROL BOX, GM LAUNCHING SECTION, AN/GSA
CONTROL BOX, GM LAUNCHING SECTION, AN/GSA
CONTROL BOX, GM LAUNCHING
FIXTURE, CROSS LEVEL AND
FIXTURE, PETISCOPE, COLLIMAT- ING, M/E F/M15
FLAMETHROWER, PORTABLE, M9-7
GUIDEJ MISSILE BASE, MAINT
GUIDEJ MISSILE, AN/TSM-96H-HAMK
GUIDEJ MISSILE, AN/TSM-96H-HAMK
GUIDEJ MISSILE BATTERY CONTROLCENTRAL, AN/TSM
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HOWITZER, LT TOWED, 105MH MIG1A1 W/E
HOWITZER, MEDIUM, SELF-
HOWITZER, MEDIUM, SELF-
HOWITZER, MED TOWED, 155MH, MI4A1 W/E
HOWITZER, MIN, SELF-PROPELLED, MI10, W/RADIO S
HOWITZER, MIN, MEANY, SELF-
IMPROVED PLATION COMMUN IPCP
INFORMATION CONQUINATION CEN- TRAL AN/HSQ-95
INSTALLATION KIT, 8009 CRANE, -HAWK-
KIT, NIGHT DRIVING, INFRA-RED, LVI MI
LANDING VEHICLE, TRACKED COM-
LANDING VEHICLE, TRACKED COM-
ENGINEER, LVIE1
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                       TANK, WATER, 100 GAL, 2-1/27, 6x6, MS
TRACTOR, 5T, 6x6, M52A2M/O WINCH, W/PT
TRACTOR, 10T, 6x6, M123A1C
TRACTOR, 10 TON 6x6, M123A2 - L 280 M
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VAN, 2-1/21, 6X6, H109A3, H/OH, H
MRECKER, 51, 6X6,M543A2-L 31G H 97 H H
PLOTIING, M5P2
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MAINTENANCE SET, GENERAL

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MORRAY, INF. 30744, 403, 412,42

MORRAY SET, ANAMPO-44 SERIES HAMK-

RADAR SET, ANAMPO-47 SERIES HAMK-

RADAR SET, ANAMPO-47 SORTES HAMK-

RECOVERY VEHICLE FULL TRACK SOTTES HAMF-

RECOVERY SET, ANAMPO-47 SORTES HAMF-

SORTE SOTTES HAMF-

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U3280 TRACTOR, MALKING, POWER ORIVENHOD 22-4E
U3290 TRAMMAY, SET, ACRIAL
U3292 TRAMMAY SET -F/USE WITH
U3292 WINTERIZATION KIT, CRANE, BAY CITY, MOD 3
U3300 WINTERIZATION KIT, CRANE, ADAMS 550 *
U3350 WINTERIZATION KIT, GRADER, ADAMS 550 *
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#### VII EVALUATION OF ITEM IMPORTANCE TO UNITS

To determine how each item of equipment relates to a unit's primary and secondary operational functions, it was first necessary to specify 22 discrete functions that units may perform. These functions are listed below. The nature of each function is self-evident in the listing, but in some cases it was necessary to add qualifying constraints to discriminate equipment use in the functions. An obvious example of this discrimination is in the mobility and transportation functions. Both of these functions are in the general function of movement of personnel and materiel. However, more specific equipment use is defined by dividing this general function into mobility, which includes unit movement/displacement, and internal movement of personnel and transportation, which includes all other forms of surface movement of personnel and materiel. The functions, together with their respective qualifying constraints, are as follows:

#### Infantry Combat Small Arms Employment

Employment of individual and crew served weapons up to and including 81mm mortar and the 106 recoilless rifledoes not include 4.2" mortar.

#### Fire Support

Employment of equipment used directly for delivery of fire support, including 4.2" mortar, 105mm howitzer and larger.

#### • Fire Support Control

Fire direction and supporting arms coordination.

#### • Mobility

Unit movement/displacement; internal movement of personnel.

#### • Communications

Operational communications only.

# • Intelligence

Collecting and processing of intelligence. Functional importance rating does not necessarily reflect the unit's need for intelligence--e.g., a unit may have a great need to receive the finished product, but have no equipment for collecting and processing intelligence.

#### Surface Transportation

Transportation of personnel and material <u>external</u> to the unit, and transportation of supplies for <u>internal</u> unit distribution; supply point distribution for unit, and/or logistic support.

# • Engineer Construction

- Demolition/Obstacle Clearance
- Supply

#### • Maintenance

Equipment maintenance other than communications/ electronics and aviation.

#### Cargo Handling

# • Service Support

Combat service support functions other than engineer construction, supply, maintenance, cargo handling, medical, transportation, and power generation.

#### • Medical

- Air Support Control
- Power Generation

#### • Ordnance Delivery

Equipment in this category limited to LAAM, FAAD, and MASS. Includes actual delivery and control of delivery. If aircraft were in the LM2 cards, they would be in this category. GSE for activities such as rearming are in A/C maintenance category.

# • Air Control

Air control functions other than Air Support Control and Air Traffic Control.

# • Air Operations Support

Air Traffic Control and ground support operations, other than maintenance, that are unique to aircraft operation.

# Air Transport

Equipment in this category includes items used in delivery of material by air transport--e.g., aerial delivery containers.

#### Communications/Electronics Maintenance

# • Aviation Maintenance

The assigned mission of each organization was then examined, and each of the 22 functions was classed as follows:

- A: Primary
- B: Secondary--directly affects primary
- C: Tertiary--affects general performance of unit.

Functions that did not fall into these categories were designated as non-applicable. The functions for two units (M1038 and M1758) are classified in Tables F-2 and F-3.

# Table F-2

# M1038 INFANTRY BATTALION FUNCTIONS, BY RELATIVE IMPORTANCE

# Primary Functions (A)

Infantry Combat/SA Employment

Mobility

Communications

# Secondary Functions (B)

Intelligence

Demolition/Obstacle Clearance

Medical

Air Support Control

Power Generation

Comm/Elect Maintenance

# Tertiary Functions (C)

Supply

Maintenance (except Comm/Elect)

Service Support

# Table F-3

# M1758 SERVICE BATTALION FUNCTIONS, BY RELATIVE IMPORTANCE

# Primary Functions (A)

Surface transportation

Supply

Maintenance (except Comm/Elect)

Service Support

Comm/Elect Maintenance

# Secondary Functions (B)

Engineer construction

Cargo handling

Power Generation

# Tertiary Functions (C)

1

SA Employment

Mobility

Communications

Intelligence

Medical

Table F-4 is a full listing of the functions in each of the three categories for each unit. Each principal item was classified as either equipment that performs a primary, a secondary, or no role in fulfilling each of the 22 functions. Secondary classification was assigned only in a few cases where it was clearly indicated. For example, D1160 1/4-ton truck (M151A1) is classified as making a primary contribution to mobility, and no contribution to any of the other functions. Table F-1 lists the functional uses of each of the equipment items, by TAM number.

To determine an item's importance to a unit, one scans all uses for which that item has primary application. If primary application is found in any function that is a primary function of the unit, the item is determined to be a high priority item to that unit. If an item is not a high priority item, but it has secondary application in a primary function or primary application in a secondary function it is called a medium priority item. If the item has application in tertiary function or secondary application in a secondary function it is called a low priority item. A process of refinement of unit function and item use designations caused all TAM items in the EAF to be found in one of these three priority levels-high, medium, or low. (Maintenance float items were tabulated separately without consideration of priority.)

The EAF was then searched for equipment to be found in each unit; each item was classified to be of high, medium, low, or nonpriority. Full listings of individual items for each unit were also obtained, but they are too extensive to appear in this appendix.

LIST OF UNIT FUNCTIONS, BY RELATIVE IMPORTANCE

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(4) Mobility	444	*****	*****	irs A B B B B B B A A A A A A A A A A A A A	momom
(3) Fire Support Control		444444	111114	Civil Affairs	
(2) Fire Support	1.1.1	*****	A A	Command &	育
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	Infantry I M1038 M1428 M4623	Artillery M1128 M1138 M1148 M4112 M4192 M4193 M4201	Combat T M4238 M4239 M4655 M4659 M4682	Ground C M1096 M1196 M1988 M4226 M4918/1 M1996	Engineer, M1378 M1868 M4343 M4358 M4358

Note: Column numbers are keys to equipment use designations in Appendix C.

A = Primary importance.
B = Secondary importance.
C = Tertiary importance.

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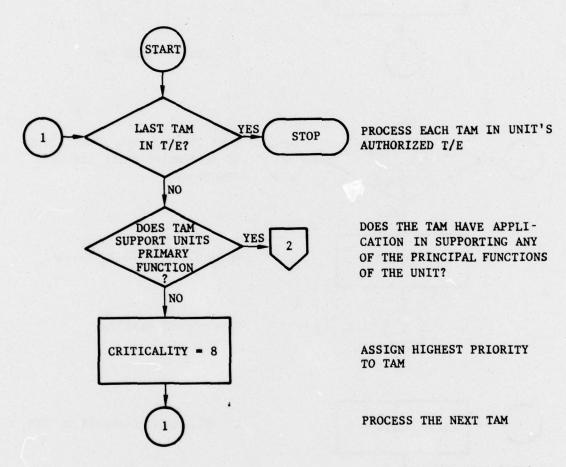
		Air Com M8610	M86112 M8612 M8615 M8615	M8631 M8640	Air Com M8710 M8715 M8813 M8913	Air Ope M8820 M8821 M8920 M8712	Fighter/ M8835 M8844 M8847 M8855 M8859 M8968 M8968 M8969 M8969	M8762 M8762 M8780 M8932 M8937 M8944
â	S. A. Employ- ment	Air Command Control	200	mm one	Air Command/Maint,  M8710 C C  M8715 C C  M8813 C E  M8913 C E	Air Ope rations Support  M8820 C  M8821 C  M8920 C  M8920 C  C  M8712 C	Fighter/Attack M8835 C M8844 C M8848 C M8855 C M8855 C M8859 C M8859 C M8969 C M8969 C	Air Transport
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(20)	Air Transport	ı			< . mm			****
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(22)	Avn. Maint.				<b>4444</b>	< 1 < 1	~~~~~~	<b>4444</b>

Table F-4 (concluded)

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		(7)	Ground		Ç	o	C	0	0	m,
		(8)	Engr.		O	o	0	0	0	0 1
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	rions, B	(12)	Cargo		C	c	C	0	0	01
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		(11)	Ord. Delivery				1			<b>4 4</b>
		(18)	Air							1.1
		(19)	Air Opne. Support		В	В	В	В	В	1.1
		(20)	Air Transport							1 1
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# VIII FLOW DIAGRAM OF CRITICALITY COMPUTATION

The criticality computation for TAMs within a T/E is logically summarized in Figure F-1.



(CONTINUED NEXT PAGE)

FIGURE F- 1. FLOW DIAGRAM ILLUSTRATING THE ASSIGNMENT OF PRIORITIES TO TAMS ACCORDING TO THE IMPORTANCE OF THE FUNCTION THE TAMS SUPPORT WITHIN THE UNIT

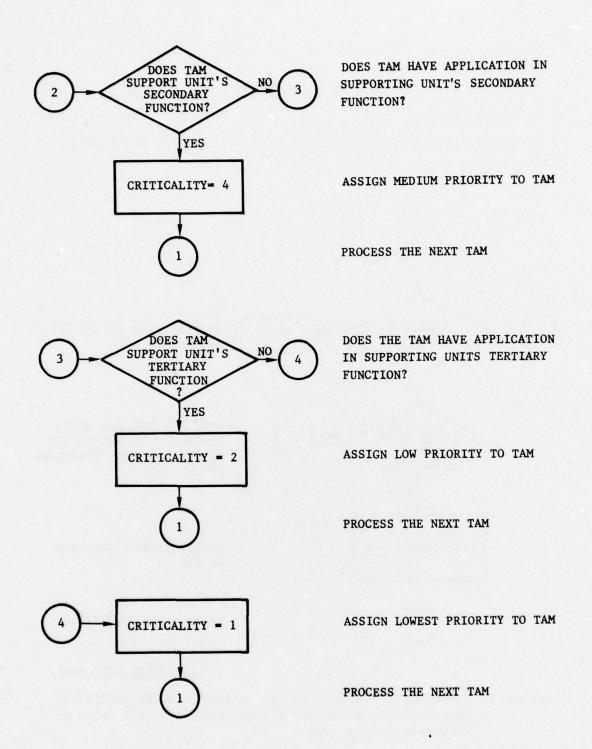


FIGURE F- 1 . (CONCLUDED)

#### IX THE CONTEAM MODEL

#### A. Introduction

The CONTEAM model is a computerized planning aid to assist the operational planner-officer in deciding which items of materiel he must leave behind when preparing a load list under cube and/or square loading constraints due to reduced shipping availability.

A brief, nontechnical description of the model follows.

#### B. Input Parameters Required for the CONTEAM Model

For the algorithm it is necessary to have the following input parameters for each unit being constrained:

- (1) Quantities of each class II and class VII TAM items that appear in the unit's T/E
- (2) Cube of each item (if the item is cube loaded)
- (3) Square of each item (if the item is square loaded)
- (4) Item square stowage indicator (for each item)
- (5) Square constraint
- (6) Cube constraint.

In addition, item criticality to the unit is utilized; however, this factor is computed within the model.

The T/E quantities, square, cube, and square stowage indicator for a given Marine Corps unit can be retrieved from the MAGTF data base. Output from the Constrained Cargo Factoring Model (CCF) provides the cube and square constraints.

# C. Computation of the Constrained T/E

The logic of the algorithm is given in the flowchart of the CONTEAM model. A description of the model follows.

#### 1. First Step

Read the square and cube constraints for the unit being constrained. Input the T/E quantity, square, cube, and square stowage indicator for each item in the unit. Compute the total cube and square requirement of the unconstrained T/E for the unit.

## 2. Second Step

Compute a "skeleton" T/E by taking one-half the highest criticality TAM items. Check whether the loading of this "skeleton" T/E will overflow the cube or square constraint placed upon the unit. For some Marine Corps units, it is indeed the case that a relatively modest constraint will make it impossible not only to load the entire T/E, but even to load that part of the T/E consisting of one-half the TAMs of the highest criticality (frequently for the square loaded items). This situation will be flagged. It does indicate the necessity of either: (1) scrubbing the mission, or (2) loading fewer than one-half the authorized T/E quantity of TAM items in the category of highest criticality.

# 3. Third Step

After the two preliminary steps have been taken, computation of up to 25 tentative loading lists proceeds. The main logic of the CONTEAM model is quite similar to the logic used in Volume II of the SRI/NWRC report "Pre D-Day Fleet Marine Force Materiel and Distribution System (1975-1980)."

Remembering that in the second step a "skeleton" T/E was developed of half the T/E quantity of those TAM items that have the highest criticality, this phase takes the remaining items in the T/E (including the other half of

the highest criticality items) and uses probability tables to compute the quantity of each of the remaining TAMs that are to be loaded to fill, but not to overflow, the constraint. This gives a tentative T/E.

The last phase of the computation is an interpolation and checking of the final results in order to bring the tentative T/E even closer to the constraint.

The output of the program is a constrained T/E, plus a list of quantities of each T/E item that must be left behind under the constraint assumed during the execution of the CONTEAM model.

#### 4. Fourth Step

As emphasized earlier, the computer program produces nothing but a tentative T/E that may need to be adjusted by the operational planning officer. (This is the fourth step.)

The program can be modified mathematically. For example, the factor "half" in the second step can be altered to another factor, such as "five-eighths." However, initial trials show that "half" is a reasonable mathematical assumption for the program. The priority for an item may be changed to either force this item "in" or "out" of the constrained T/E. For instance, if the planner wishes the program to select weapons ahead of every other TAM item, he would assign each weapon a very high priority.

After the planner has made all of the adjustments he deems necessary, he can then rerun the CONTEAM model to obtain a more desirable T/E.

### D. Flow Charts of CONTEAM Model

A flow chart illustrating the steps necessary in assigning priorities to items of materiel according to their importance in supporting a unit's

functions was presented in Figure F-2. The CONTEAM model commences with the identical logic. Flow charts picking up the logic of the model where Figure F-2 leaves off follow.

## E. General Characteristics of the CONTEAM Model

For TAM items that occur in a unit's T/E with authorized quantities of 1 to 20, the program will include TAMs with the highest criticality and exclude TAMs with the next-to-highest criticality when the constraint amounts to 60-75 percent of the space required to load the unit's full authorized T/E. Of the TAMs with low criticality, the bulky ones will be selectively excluded, but usually in part. That is, the quantity admitted to the constrained T/E will be some fraction of the authorized quantity. Nonpriority TAM items will probably be completely excluded from the constrained T/E.

For items that appear in the unit's T/E with authorized quantities of 40-1200, the program will exclude some portion of the full T/E quantity in almost every case--even for the highest priority items. This is purely a function of the algorithm as it begins to favor the first units of low priority items over, say, the 100th unit of a higher priority item. Experience shows these results to be useful, although they can be modified if the planner feels this is necessary.

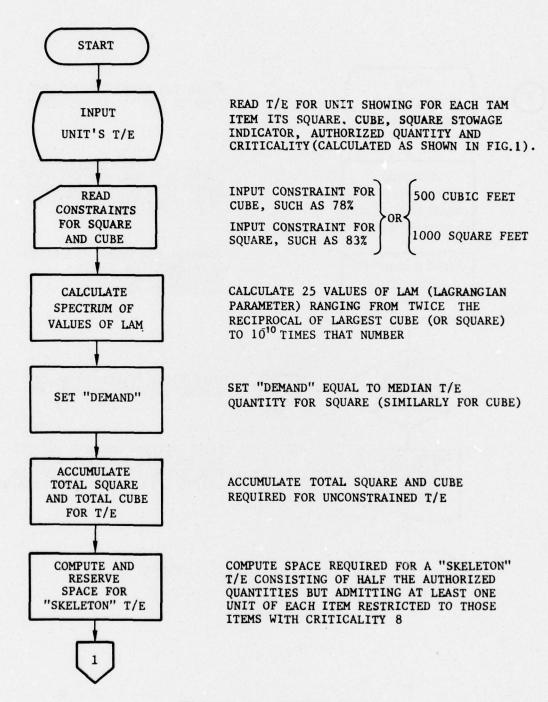
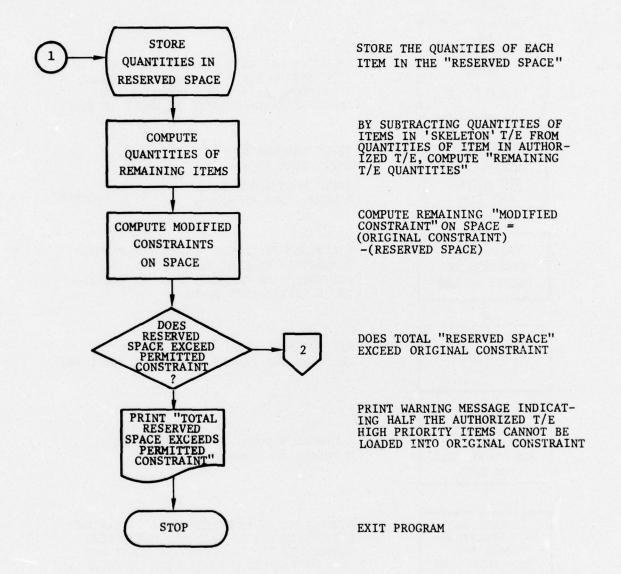
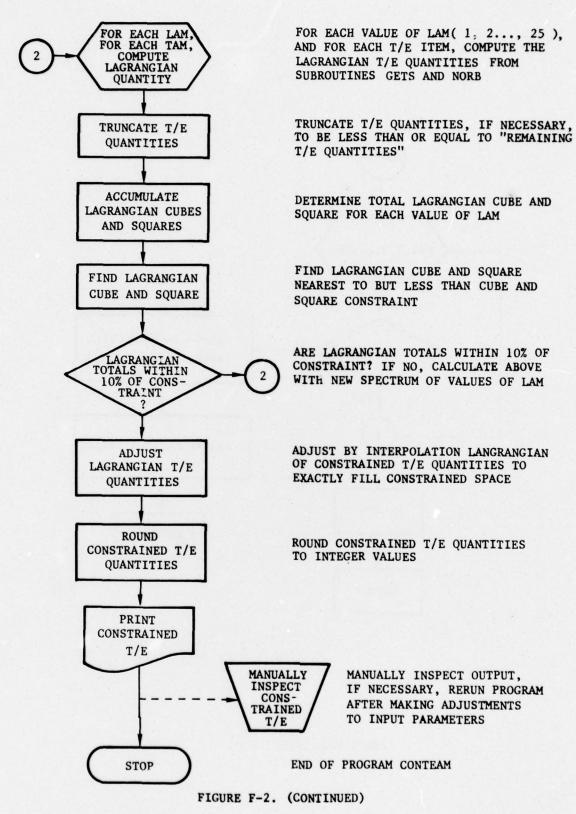


FIGURE F- 2. PROGRAM CONTEAM





F-55

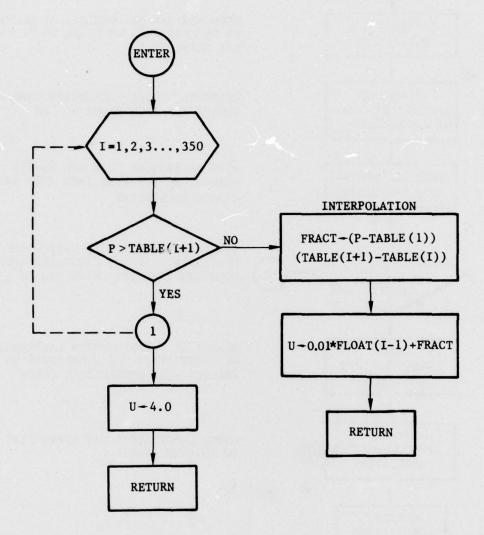


FIGURE F-2. (CONTINUED)

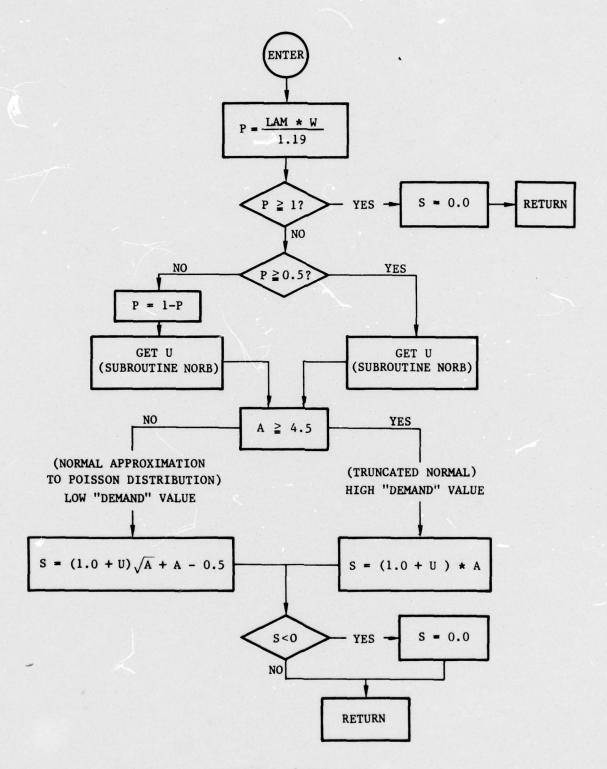


FIGURE F-2. (CONCLUDED)

Appendix F

CONSTRAINED T/E EMBARKATION MODEL

Part 2: Technical Description

#### Appendix F

#### CONSTRAINED T/E EMBARKATION MODEL

## Part 2: Technical Description

#### I INTRODUCTION

In the first part of this appendix, an algorithm is described for the construction of a constrained T/E that will maximize protection against shortages. This algorithm was used as a means of obtaining improvement over the conventional method of constructing a T/E (which would simply reduce all authorized quantities in a fixed ratio). In this use, the algorithm is oriented to the construction of T/Es under cube or square constraint.

The general format of the first part of this appendix comprises discussions of the objective of the algorithm, its derivation and mathematical logic, the practical considerations in its application, and finally, a flow description of its operation.

#### A. Constraints

There are a number of overall constraints that may be used in the algorithm. For the purpose of determining a constrained T/E for distribution of materiel, the respective constraints are square, cube, and (sometimes) total weight. If two constraints operate simultaneously, the algorithm is applied separately to square loaded and bulk cargo. If necessary, bulk space is reassigned, and operational readiness is recomputed with the redistribution of bulk and square space.

## B. Objective Function

The objective of the calculation is to determine a T/E, i.e., to show the number of units of each TAM that will minimize the expected pain of shortages and maximize operational readiness.

### C. Preliminary Filling

The list of TAMs of highest criticality is assumed to be especially important. To doubly emphasize this importance, a preliminary computation partially fills the constrained space with half the authorized quantities of these high criticality TAMs. If the constraint is so restrictive as to forbid even this part of the T/E, the mission is assumed to be impossible to execute because of lack of shipping space.

#### II DISTRIBUTION FUNCTIONS OF "DEMAND"

In this algorithm, "demand" is an artificial parameter used to enter (or construct) certain probability tables. Although many records of use have been processed, a useful procedure (for constructing a T/E) based on true demand has not been found. Hence, "demand" is simply a parameter only partly related to T/E quantity. In most cases, the parameter "demand" does not change through an entire T/E. Specifically for square loaded TAMs, "demand" is usually 2; for bulk loaded TAMs, "demand" is usually 5. The algorithm applies to class II and class VII TAMs only; the numbers 2, 5 are chosen since these are medians of the respective authorized T/E quantities.

### A. The Assumed Distribution Functions of Demand

For TAMs with a "demand" of less than 4.5, the demand distribution is assumed to be Poisson. For TAMs with a "demand" of 4.5 or more, the demand distribution is assumed to be a truncated normal distribution, with parameter  $a = 0.78 \times 10^{-5} \times$ 

$$p(t) dt = \frac{1.19}{a\sqrt{2\pi}} \exp \left[ -\frac{1}{2} \left( \frac{t - a}{a} \right)^2 \right] dt . \qquad (1)$$

Therefore

$$\int_{0}^{\infty} p(t)dt = 1 .$$
 (2)

Note that, for this choice of parameters in the truncated normal distribution, the standard deviation is a large fraction of the mean. Thus, a very considerable variation about the mean is to be expected.

# B. Mathematical Derivation

Calculation of optimum stocking procedure is as follows. Suppose the constraint is:

$$\Sigma w_{i} s_{i} = W.$$
 (3)

Then the quantity to optimize is:

$$F(s_1, s_2, \ldots) = \sum_{i} c_i \int_{s_i}^{\infty} (t - s_i) p_i(t) dt + \lambda (\sum_{i} w_i s_i - W) . \qquad (4)$$

(All summations are over the values of i.)

The quantities to determine are  $s_i$ , the amount of the ith TAM to be supplied. The notation is as follows:

F = Function to be optimized

c = Criticality

t = Demand, which is the variable of integration

 $\lambda$  = Lagrangian parameter needed to take account of the constraint

 $w_i$  = Unit square, or cube, of the ith TAM

W = Constraint = total square or cube permitted

 $p_{i}(t)$  = Distribution function of demand for the ith TAM.

Differentiating the function with respect to each independent decision variable, the relation

$$\lambda = \frac{c_i}{w_i} \int_{s_i}^{\infty} p_i(t) dt$$
 (5)

is obtained.

Thus, if the quantity  $w_i^{\lambda/c}$  is equal to or greater than 1,  $s_i^{\lambda/c}$  must be taken to be 0: the ith TAM is not included. If the quantity  $w_i^{\lambda/c}$  is less than 1,  $s_i^{\lambda/c}$  is determined by the equation:

$$\lambda_{w_{i}}/c_{i} = \int_{s_{i}}^{\infty} p_{i}(t) dt . \qquad (6)$$

It is seen that the greater the criticality  $c_i$ , the larger will be the stock  $s_i$ . Also, the smaller the unit (square or cube)  $w_i$ , the larger will be the stock  $s_i$ . On the other hand, when the unit (square or cube) is quite large, the strategy will be to accept shortages in the items that have a large size to gain the extra benefit of avoiding shortages in other items.

The T/E quantity  $\mathbf{s}_{\mathbf{i}}$  is always truncated so as not to exceed the authorized T/E quantity.

#### C. Practical Implementation

In all this calculation, the quantity  $\lambda$  is not yet determined. The way to determine  $\lambda$  is by trial. A fixed value is chosen for  $\lambda$ , and the entire supply table, including the value of  $s_i$  for each TAM, is computed. Then the total square or cube is cumulated to see whether the trial value of  $\lambda$  is too small or too large. If the trial total is too large, the trial value of  $\lambda$  was too small, and vice versa.

## D. Starting the Algorithm

To avoid too many trials, it is desirable to have a reasonable starting value for  $\lambda$ . If the largest unit (square or cube) is 500, a reasonable starting value for  $\lambda$  is 0.002. For a T/E that contains many items with unit square exceeding 500, but very few with unit squares exceeding 5,000, a reasonable starting value for  $\lambda$  is 0.0002. In general, the choice is the reciprocal of the truncating unit square.

In experimental calculations, instead of using a single starting value for  $\lambda$ , and then adjusting, 25 values for  $\lambda$  were used that were expected to bracket the correct budget. The relation between the constraint and the corresponding value of  $\lambda$  is approximately of the form:

$$\lambda^n$$
 . B = constant, (7)

where B is the constraint, and the constant depends on the spectrum of TAMs for which the T/E is being computed. Once a T/E has been computed for each of the 25 values of Y bracketing the constraint, a table showing constraint versus Y can be entered, and the correct number of units of each can be determined by making a final adjustment to the particular T/E that is closest to, but below the constraint. This adjustment is ignored for any TAM already taken in authorized quantity. Any method of adjustment will do; an increase in constant ratio is to be recommended. The ratio is determined by simply summing the square of the short fall TAMs, and comparing this short fall with the constrained space not yet filled. But no TAM must be taken in more than the authorized T/E quantity.

At this point, the quantities for many TAMs will be fractions. For practical implementation, these quantities can be rounded to the nearest whole number.

## E. Solution of Equation (6)

It remains to explain how to solve equation (6) for  $s_i$ , when all the other letters and the distribution function are known. The method used when the distribution was assumed to be normal (demand, per period, 4.5 units or more) was simply to enter a machine stored table of the normal cumulative probability, and take out  $s_i$ . This cannot accurately be done for values of  $s_i$  exceeding three times the mean demand, unless the table is considerably more detailed than it is convenient to store in a computer with limited memory space. In this case  $s_i = 4.0$  was taken whenever the cumulative probability calculated from (6) exceeded 0.9998 (residual probability less than 0.0002). This means that a T/E quantity exceeding 4 cannot be attained. That is, quantities of a TAM in excess of 4 times the "demand" will always be short.

But some TAMs have very large authorized quantities, and quantity should not be restricted to 20. Therefore, for a TAM with an authorized quantity of 40 or greater, the parameter "demand" is set to 1/8 of the authorized quantity. This device will make it possible to take the entire authorized quantity of a high criticality TAM.

#### III APPROXIMATION TO EXACT ALGORITHM

## A. Assignment Priority List

In this section, a mathematically exact algorithm is described. Later a computer oriented approximation is given, and it is shown that that approximation is equivalent to the exact algorithm. The mathematically exact algorithm begins with the construction of an assignment priority list.

## 1. Rationale

For each (ordinal) unit of each TAM, the value of that extra unit providing additional protection against shortage must be computed. If p(t) is the probability density of demand for t units, the incremental value of the k-th unit can be shown (see below) to be approximately equal to:

$$(c/w) \int_{k-\frac{1}{2}}^{\infty} p(t) dt .$$

Note that the integral runs from  $k - \frac{1}{2}$  to  $\infty$ .

Notation:

c = Criticality of the TAM

w = Unit square (for square loaded TAMs) or unit cube (for bulk loaded TAMs)

p(t) = Probability density of demand.

For large values of "demands", x, it is usual to take:

$$p(t) = \frac{1.19}{a\sqrt{2\pi}} \exp \left[-\frac{1}{2}(t-a)^2/a^2\right],$$
 (8)

where

a = 0.78x  $\bar{x} = "Demand".$ 

Formula (8) is the density of a truncated normal distribution, truncated at t = 0; the mean of the original (nontruncated) normal distribution is equal to its standard deviation a. (See Fig. F-3.)

For low values of "demand," the (discrete) Poisson distribution is appropriate:  $p(t) = e^{-a} t/t!$ , where now a = "demand."

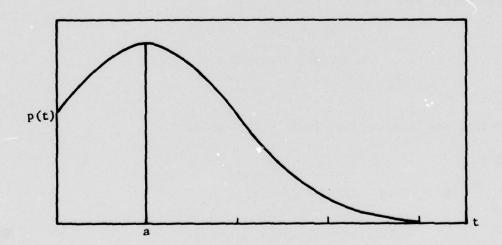


FIGURE F-3. THE TRUNCATED NORMAL DISTRIBUTION, TRUNCATED AT t = 0, a =  $0.78\bar{x}$ ,  $\sigma$  =  $0.47\bar{x}$ 

### 2. Mathematical Derivation

The extra protection afforded by the next unit of a TAM can be found from tables that are readily available. The precise meaning of the term "extra protection" has first to be specified. In the analysis of this appendix, stress on a military unit, is measured by "number of units needed but not available." Thus, a shortage of 8 is more stressful than a shortage of 2. An authorized T/E for quantity 100 that is 99 percent filled (with 1 short) is less burdensome, in terms of expediting, lost time, and reduced efficiency of operation than is an order for the same quantity (100) that is only 50 percent filled.

If the probability density of "demand" is p(t), and the quantity shipped is k, then the criticality weighted <u>expected</u> shortage penalty is given by the formula:

$$(c/w) \int_{k}^{\infty} (t - k) p(t) dt .$$

If the probability density corresponds to a discrete probability, the integral sign must be replaced by a summation sign. Assume for the moment that the probability density is continuous; this assumption is valid when the "demand" is large (more than 4.5). As an example, compute the added protection (diminished penalty) provided when 1 unit (instead of 0 units) of a TAM is shipped. The criticality weighted expected shortage penalty will be reduced from:

$$(c/w)$$
  $\int_{0}^{\infty} t p(t)dt$  to  $(c/w)$   $\int_{1}^{\infty} (t-1) p(t)dt$ ,

as the above discussion shows. The first integral  $\int\limits_{0}^{\infty}$  can be written

as 
$$\int_{0}^{1} + \int_{0}^{\infty}$$
, so the difference in question amounts to:

$$(c/w) \int_{0}^{1} t p(t)dt + (c/w) \int_{1}^{\infty} p(t)dt .$$

The "theorem of the mean" in integral calculus shows that the first integral can be approximated by the expression:

$$\xi_1 \int_0^1 p(t)dt$$

where  $\xi_1$  is some number between 0 and 1. A better approximation, valid for any slowly changing probability density function p(t), is:

$$\int_{0}^{1} t p(t) dt \approx \int_{\frac{1}{2}}^{1} p(t) dt .$$

The validity of this approximation is obvious in case p(t) is constant in the interval (0,1). In summary then, the diminution of penalty provided by the first unit of a TAM is given approximately by the formula:

$$(c/w)$$
  $\int_{0.5}^{\infty} p(t)dt$ .

This number can be found by reference to tables of cumulative probability that correspond to the probability density p(t).

Similarly, the further diminution of penalty provided by a second piece of the same TAM is given by the formula:

$$(c/w)$$
  $\int_{0}^{\infty} p(t) dt$  ,

which is an approximation to the difference

$$(c/w) \int_{1}^{\infty} (t-1) p(t)dt - (c/w) \int_{2}^{\infty} (t-2) p(t)dt$$
.

In general, the additional diminution of penalty brought about by the k-th unit of a TAM is given approximately by the formula:

$$(c/w) \int_{k}^{\infty} p(t)dt .$$

This formula is valid if p(t) changes only slowly in the interval  $\lfloor k-1,k \rfloor$ . The above formulas are certainly valid for the truncated normal distribution, provided the "demand" is large.

#### 3. TAMs With Low Demand (Square Loaded T/E List)

For the square loaded portion of the T/E list, "demand" is typically 2. For this case, a useful probability distribution is the Poisson distribution. This is a discrete distribution so integrals cannot be used to represent the expected number of units short. For a discrete distribution, the correct formula involves a sum, not an integral. The criticality weighted expected penalty for shortage is:

$$(c/w)$$
  $\sum_{t=k}^{\infty} (t - k) p(t)$ ,

provided the current quantity is k units.

The analysis in this case parallels the analysis above for a continuous probability density. The work with sums is simpler than the work with integrals. The result is that the quantum diminution in penalty provided by the k-th increase of the TAM quantity is:

$$(c/w)$$
  $\sum_{t=k}^{\infty} p(t)$ .

For the Poisson distribution corresponding to "demand" a, this is clearly equal to:

$$(c/w)$$
  $\sum_{t=k}^{\infty} \frac{a^t e^{-a}}{t!}$ .

Tables of this partial sum are available for a large range of values of a "demand." Also, the partial sum can be approximated by use of other tables, only tables of the normal probability integral are needed (see the discussion following equation (9)).

## 4. Construction of the Working List

After completing the "incremental protection" computations, the next step is to list all (ordinal) units of all TAMs in sequence. The sorting is arranged so that the unit providing the greatest quantum of benefit comes first, followed by the unit that provides the second greatest benefit. A section of such a list looks as shown in Table F-5. The most advantageous T/E for any total is the one obtained by simply

chopping Table F-5 off at the row indicated by the figure in the last column of the table. This result is exact; however, there is a disadvantage in using this method.

## B. Disadvantages of the Above Algorithm

If TAMs are added to or removed from a T/E, the entire list (Table F-5) must be resorted. Another difficulty comes from the fact that the incremental values must be computed for a very large number of units of each TAM; thus, the number of entries (TAM No.--Unit No.) to be sorted can be 2,500 or more, even for a modest T/E of only 50 TAMs.

SEQUENCE OF TAMS SORTED ACCORDING
TO THE BENEFIT PROVIDED BY EACH UNIT--CONSTRAINT = 45

Table F-5

TAM	Ordinal Number of Unit	Unit Square	Cumulative Square
A0	lst	3	3
A0	2nd	3	6
C2	1st	2	8
A0	3rd	3	11
C3	1st	5	16
C2	2nd	2	18
A0	4th	3	21
D4	1st	20	41
E	1st	1	42
A0	5th	3	45

NOTE: Constraint filled (if T/E quantity of AO... is 5 or more)

Table F-6

VALUES OF THE NORMAL PROBABILITY INTEGRAL, P(u), FOR VALUES OF u BETWEEN 0.0 AND 3.49

$$P(u) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{u} \exp \left[ -\frac{1}{2} t^2 \right] dt = 1 - Q(u)$$

$$Q(u) = \frac{1}{\sqrt{2\pi}} \int_{u}^{\infty} \exp \left[ -\frac{1}{2} t^{2} \right] dt$$

u	+ .00	.01	.02	.03	.04	.05	.06	.07	.08	.09
0.0	.5000	.5040	.5080	.5120	.5160	.5199	,5239	.5279	.5319	.5359
0.1	.5398	.5438	.5478	.5517	.5557	.5596	.5636	.5675	. 5714	.5753
0.2	.5793	.5832	.5871	.5910	.5948	.5987	.6026	.6064	.6103	.6141
0,3	.6179	.6217	.6255	.6293	.6331	. 0368	,6406	.6443	.6480	.6517
0.4	.6554	.6591	.6628	.6664	.6700	.6736	.6772	.6808	.6844	.6879
0.5	.6915	.6950	.6985	.7019	.7054	.7088	.7123	.7157	.7190	.7224
0.6	.7257	.7291	.7324	.7357	.7389	.7422	.7454	.7486	.7517	.7549
0.7	.7580	.7611	.7642	.7673	.7704	.7734	.7764	.7794	.7823	.7852
0.8	.7881	.7910	.7939	.7967	.7995	.8023	.8051	.8078	.8106	.8133
0,9	.8159	.8186	.8212	.8238	.8264	.8289	.8315	.8340	.8365	.8389
1.0	.8413	.8438	.8461	.8485	.8508	.8531	.8554	.8577	.8599	.8621
1.1	.8643	.8665	.8686	.8708	.8729	.8749	.8770	.8790	.8810	.8830
1.2	.8849	.8869	.8888	.8907	.8925	.8944	.8962	.8980	.8997	.9015
1.3	.9032	.9049	.9066	.9082	7.9099	.9115	.9131	.9147	.9162	.9177
1.4	.9192	.9207	.9222	.9236	.9251	.9265	.9279	.9292	.9306	.9319
1.5	.9332	.9345	.9357	.9370	9382	.9394	.9406	.9418	.9429	.9441
1.6	.9452	.9463	.9474	.9484	.9495	.9505	.9515	.9525	.9535	.9545
1.7	.9554	.9564	.9573	.9582	.9591	.9599	.9608	.9616	.9625	.9633
1.8	.9641	.9649	9656	.9664	.9671	.9678	.9686	.9693	.9699	.9706
1.9	.9713	.9719	.9726	.9732	.9738	.9744	.9750	.9756	.9761	.9767
2.0	.9772	.9778	.9783	.9788	.9793	.9798	.9803	.9808	.9812	.9817
2.1	.9821	.9826	.9830	.9834	.9838	.9842	.9846	.9850	.9854	.9857
2.2	.9861	.9864	.9868	.9871	.9875	.9878	.9881	.9884	.9887	.9890
2.3	.9893	.9896	.9898	.9901	.9904	.9906	.9909	.9911	.9913	.9916
2.4	.9918	.9920	.9922	.9925	.9927	.9929	.9931	.9932	.9934	.9936
2.5	.9938	.9940	.9941	.9943	.9945	.9946	.9948	.9949	.9951	.9952
2.6	.9953	.9955	.9956	.9957	.9959	.9960	.9961	.9962	.9963	.9964
2.7	.9965	.9966	.9967	.9968	.9969	.9970	.9971	.9972	.9973	.9974
2.8	.9974	.9975	.9976	.9977	.9977	.9978	.9979	.9979	.9980	.9981
2.9	.9981	.9982	.9982	.9983	.9984	.9984	.9985	.9985	.9986	.9986
3.0	.9987	.9987	.9987	.9988	.9988	.9989	.9989	.9989	.9990	.9990
3.1	.9990	.9991	.9991	.9991	.9992	,9992	.9992	.9992	.9993	.9993
3.2	.8993	.9993	.9994	.9994	.9994	.9994	.9994	.9995	.9995	.9995
3.3	.9995	.9995	.9995	.9996	.9996	,9996	.9996	.9996	.9996	.9997
3.4	.9997	.9997	.9997	.9997	.9997	,9997	.9997	.9997	.9997	.9998

Source: Handbook of Mathematical Functions, U. S. National Bureau of Standards, AMS#55, Table 26.1, 1968.

### C. An Alternative Computation

The alternative computation is explained in the flow description following.

## 1. Computation

For each value of LAM, and for each TAM, the T/E quantity (for constrained square or cube) is computed according to the formula:

$$(w)(LAM)/c = \int_{s}^{\infty} p(t)dt , \qquad (9)$$

where

w = Unit square or cube (if total is the constraint)

c = Criticality factor

LAM = Value taken unchanged during this step of the algorithm

s = Number of units: this is the unknown in the equation.

If (w)(LAM)/c exceeds 1, or is equal to 1, s is taken as 0.

The formula ( $\ell = 1.19$ )

$$p(t) = \frac{\ell}{a\sqrt{2\pi}} \exp \left[-\frac{1}{2}(t - a)^2/a^2\right]$$
 (10)

has been previously stated. Therefore, (9) can be solved for s by solving the equation

$$\frac{(w) (LAM)}{(c) (l)} = \frac{1}{\sqrt{2\pi}} \int_{u}^{\infty} \exp\left(-\frac{1}{2} v^{2}\right) dv$$
 (11)

for u, and then setting s = ua + a. The integral on the right-hand side of (11) will be recognized as the standard probability integral; moreover, the integral is independent of the TAM, and so may be entered into a computer in tabular form. This makes it possible to obtain the value of u by table look-up. In the program the table was to have only finite length, so the arbitrary decision was made that whenever the quantity  $1 - \frac{(w)(LAM)}{(c)(\ell)}$  exceeded 0.9998, u would be entered as 4. The values to be entered are given in Table F-6, which is adapted from standard publications.

For square loaded TAMs, "demand" was taken = a = 2; then the use of equation (4) is not an accurate method. The formula for p(t) should be replaced, for such TAMs, by the Poisson distribution. An approximation to the Poisson distribution frequency function, given by the following lemma, was used:

If t is Poisson distributed, with mean a, then

$$\frac{t-a+0.5}{\sqrt{a}}$$
 is approximately normally distributed.

For values of a near 0, and for values of t equal to 0 or 1, the word "approximately" should be read as "very approximately"; nevertheless, for the present purpose, the approximation is adequate. The only features of the distribution required to be approximated are the cumulative values, i.e., the frequency function integral or distribution function. For these values, the approximation is acceptable. The fact that the normal distribution function is again involved makes the table look-up convenient; the value of u is computed as before, and s is taken to be:

It is understood that s must never be negative; when (12) brings out a negative result, it must be adjusted upward to 0. (The result could be very slightly negative in certain cases.)

All quantities s must be truncated to the authorized T/E quantity if they exceed it.

As the calculation proceeds from one TAM to the next, cumulative totals are kept in a running fashion for each of the values of LAM. At the end of this phase of the calculation--that is, when all TAMs have been scanned--there will be a set of 25 total constraints, one for each of the 25 values of LAM. The item record of each TAM will show the number of units of that TAM needed to bring out the total constraint shown. In general, the number of units shown will be a fraction. In other words, it is assumed in this preliminary calculation that each TAM is divisible. This device is a conventient fiction to make it possible, in the next step, to interpolate more accurately from one constraint to the next. If by chance the correct constraint is not bracketed in the 25 calculations, further choices of LAM are to be made. A quick procedure for homing in on the best choices for LAM is given next.

#### 2. Interpolation to Obtain the Correct Value of LAM

The fourth step describes the inverse interpolation needed to home in on the correct value of LAM, and also the final interpolation used to obtain the T/E. In the preceding pages it was shown how to compute a constrained square or cube for any given value of LAM.

A graph of the relationship between LAM and constrained cube has approximately the shape indicated in Figure F-4.

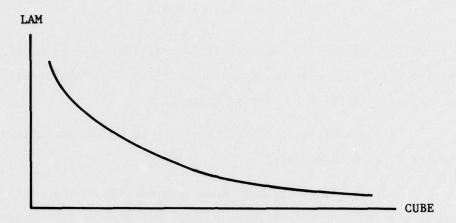


FIGURE F-4. APPROXIMATE FORM OF RELATION BETWEEN LAM AND CUBE

- When LAM is decreased, the corresponding cube will increase
- If LAM is taken small enough, the cube can equal the authorized T/E cube
- For large values of LAM, the cube approaches zero.
   (Ultimately, it can be zero.) In other words, above a threshold value, there is no computation to be done.

If the 25 trial values of LAM run from the reciprocal of the smallest item cube to  $10^{-10}$  times this quantity, the constraint will be well approximated by one of the 25 trial grand total cubes. (If by chance (or error) this does not occur, interpolation or extrapolation should be used; a graphical procedure, or logarithmic interpolation, is quite accurate. To make a final adjustment from an approximate constrained cube to the exact constraint the method explained in the computation flow description was used. Briefly, this is a proportional increase in the trial T/E quantities of all TAMs at below authorized quantities in the tentative T/E.

## APPENDIX F REFERENCES

- J. L. Brenner, W. S. Duff, and R. B. Ringo; "Pre-D-Day Fleet Marine Force Materiel Requirements Determination and Distribution System (1975-1980--Volumn II: Algorithms for the Construction of a Table of Supply Under Size Constraints and for the Simulation of Item Processing at a Marine Corps Supply Center"; Final Report, Stanford Research Institute Project EGU-1003-50-53, Contract N00014-71-C-0205; October 1971.
- 2. M. A. Geisler and H. W. Karr; "The Design of Military Supply Tables for Spare Parts"; Operations Research Society of America Journal, Vol. 4; (pp. 431-442) 1956.
- 3. E. C. Molina; "Poisson's Exponential Limit"; Van Nostrand, New York.

Appendix G

MAGTF IMPROVEMENT EFFORT

### Appendix G

### MAGTF IMPROVEMENT EFFORT

#### I BACKGROUND OF MAGTF IMPROVEMENT EFFORT

Because the "Materiel Weight and Cube Control" study required many long computer runs of the program MAGTF, and because of the excessive processing time on the computer each of these runs would require, the first task of this project was to streamline the coding of MAGTF for more efficient processing. An associated task in this effort was to correct all known programming errors. Also, an up-to-date and accurate data base was to be provided the project. These reprogramming, debugging, and data base updating efforts had to be provided within the limitations of a restricted time frame and budget.

## A. Determination of Where to Concentrate the Program MAGTF Improvement Effort

Before the process of speeding up the execution time of program MAGTF could commence, it was necessary to determine exactly where in the MAGTF coding the majority of the total execution time of cun was being spent. To accomplish this task, temporary FORTRAN statements were inserted into each of MAGTF's original 192 subroutines to measure the amount of CPU time required by each of the individual subroutines. Then, by running a small, test MAGTF, it was possible to determine precisely the percentage of the total execution time of the program that was being consumed by each of the subroutines.

Additional coding was also inserted into each subroutine to count the total number of times each of the subroutines in MAGTF was called or accessed during the execution of the test case.

This preliminary analysis enabled the project team to concentrate its efforts on reducing the execution time of only those subroutines that would give the maximum payoff (reduced CPU time) for the minimum man-hours expended by the team.

## B. Program MAGTF Core Reduction

Equally important as the reduction of the running time of MAGTF subroutines was the reduction of the overall core requirement of the program. The reduction of the program size was important since the original size of the program was so large that it could not be loaded in its entirety into a 200K partition on the HQMC's 360/65 computer. Because of the program MAGTF's length it was, therefore, necessary to break the program up into several overlays. By overlaying, the amount of coding that was required to reside in core at any one time was greatly reduced; however, the execution time of the program was greatly increased since each time a new overlay was needed by MAGTF, the overlay currently residing in core had to be written to disk storage, and the new overlay then read from disk storage. This additional reading and writing (I/O) placed an additional burden on top of the already lengthy running time of the program. By reducing the total core requirement of program MAGTF, fewer overlays would be required, thereby reducing the I/O requirements of the program, which in turn decreased the overall execution time of the program.

## C. Elimination of Debug Statements

During the programming of MAGTF, it was found to be useful to place several debug PRINT statements in each of program MAGTF's subroutines. These debug PRINT statements could be activated by either the programmer or the user of MAGTF by including a DEBUG card in his data stream. However, as MAGTF became more frequently utilized and reliable, the need for the debug coding became less and less useful. Therefore, all of the debug statements were removed from the production version of program MAGTF. This accomplished a significant reduction in core storage requirements, as well as a noticeable reduction in CPU time required to execute the program.

#### D. Reduction of I/O Buffers

The next step in improving the execution time of MAGTF was to reduce the size of the I/O buffers for the card reader, the card punch, and the printer. By reducing the size of the I/O buffers, a considerable amount of core storage was saved at the expense of a very slight increase in CPU and I/O time.

## E. Program MAGTF Coding Improvements

The biggest saving in CPU time resulted from the recoding of three subroutines and by the addition of a new subroutine. Subroutines SYSTEM, BINARY, and CHTONO were almost completely recoded in a vastly more efficient manner. A completely new subroutine, GETCHR, was written to handle more expeditiously special character transfers previously handled by subroutine CHAR.

### F. Streamlining of PRINT Routines

In programming the original version of the program MAGTF, a separate subroutine was written to perform the printing of each unique page of output. Since it was frequently the case that the output from a regular listing differed from that of a compendium by only the heading or by the inclusion or omission of a column of figures, it was decided to combine

these similar PRINT routines into a single subroutine whenever possible, and to set a switch in the new routine that would allow the subroutine to decide which heading or which column of figures to print. This effort resulted in a very substantial core reduction.

#### II ADVANTAGES OF CORE REDUCTION

The results of the core reduction effort were utilized in two ways.

#### A. Elimination of Overlays

The first utilization of the additional core now available from the reduction effort was to completely eliminate all overlays i.e., allow the complete program to reside in central memory during the execution of the program as opposed to the original time-consuming calling of the overlays to and from disk storage. Running with the unoverlayed version of MAGTF allowed a large savings in I/O time.

### B. Increasing Accumulation Blocks

The second way in which the freed core was utilized was to retain the most frequently needed accumulation blocks in central memory permanently, as well as to increase the number of accumulation blocks temporarily residing in core from 4 to 32. This improvement by itself reduced program MAGTF's total I/O requirement approximately 60 percent.

#### III MAGTF MAINTENANCE

Several program MAGTF errors were identified and corrected during the improvement effort. The majority of the corrections were for overflowed fields, misspelled headings, column and total alignment, etc. All of these can be grouped under the general description of formating problems. These problems were as a rule quickly and easily corrected.

The most troublesome error to correct was in the restart procedure of MAGTF. As it turned out, the problem was not so much a programming deficiency as it was an interface problem with the operating system. Whenever in the execution of MAGTF an abnormal ending, such as an "operator drop" or a "time limit" halt was experienced, the disposal of the output buffers was inconsistent. In MAGTF's case, the printed output listing would indicate that the input data had been processed to a given point, while the output tape (restart tape) would indicate the processing terminated at an entirely different point. Therefore, when an attempt was made to restart a run that had terminated abnormally by telling the program to proceed from where the output listing left off, the program became confused since this was not the same place the restart tape left off. This problem was corrected by reprogramming the restart procedure with a more complicated logic.

The second troublesome bug to correct was in the "mobile loading" procedure. In this case, correction of the programming errors was not the problem so much as the correction of each error seemed to uncover a new error. Such a sequence continued through several iterations until the mobile loading procedure finally performed as desired.

#### IV RESULTS OF THE MAGTF IMPROVEMENT EFFORT

The results of the MAGTF improvement effort were startling. All known program and data base errors were cleaned up, and the program's improved execution time exceeded all expectations.

Personnel from the Assistant Chief of Staff (Installations and Logistics, LPS) and the MAGTF systems coordinators processed a Marine Amphibious Force (MAF) computer run during January 1975. The computer processing time for this run was approximately 63 wall clock hours, or 29.11 minutes per unit on the HQMC computer. In early November 1975, a Marine Amphibious Brigade (MAB) was processed using the improved version of program MAGTF averaging 4.12 minutes per unit--an 86 percent improvement over the original 29.11 minutes per unit.

As can be seen from Table G-1, I/O time has been decreased from 22.99 minutes per unit to 1.76 minutes per unit, or a 92 percent reduction. CPU time has been reduced from 6.12 minutes per unit to 2.36 minutes per unit, a 61 percent reduction.

Table G-1

COMPARISON BETWEEN ORIGINAL VERSION OF MAGTF AND IMPROVED VERSION OF MAGTF EXECUTION TIMES FOR PROCESSING MARINE CORPS T/O UNITS

	Original MAGTF	Improved MAGTF	Improvement	Percentage Improvement
I/O minutes per unit	22.99	1.76	21.23	92%
CPU minutes per unit	6.12	2.36	3.76	<u>61</u>
Total minutes per unit	29.11	4.12	24.99	86%

#### V FUTURE PROGRAM MAGTF IMPROVEMENT

During the process of improving the execution time of program MAGTF, several areas were observed where the program could be even further improved. These areas for possible improvement include ease of user usage, increased readability of printouts, and programming improvements to decrease execution time. It is felt that the computer running time of program MAGTF can be further reduced by a minimum of 50 percent with additional reprogramming.

In light of the above, the following recommendations are made:

- (1) Reprogram the method by which MAGTF accesses the data base. By making a second pass through the UNIT and SYSTEM files during a program CREATE run, it is possible to attach disk addresses to each trailer record, and thus enable MAGTF to directly address any data record. This effort will eliminate two binary searches (decreasing CPU time) and eliminate one disk access for every retrieval (decreasing I/O time).
- (2) Modify the data base structure so that as many data elements as possible lie on computer word boundaries. This will save additional computation time since these elements can be read into core without the need of repositioning these elements before calculations can be made.
- (3) Store data in the data base in a computational (Integer or Floating Point) format. This will eliminate the necessity of decoding an element when it is retrieved before it can be used for computations.
- (4) Each subroutine in program MAGTF should be examined individually for further code condensing and execution time improvements.
- (5) The restart procedure should be reprogrammed to eliminate the need for user intervention.

- (6) The MAGTF Program should be modified to permit all intermediate maintenance ground support equipment, computed from supported aircraft, to be displayed in the Headquarters and Maintenance Squadron listing.
- (7) The program should be modified to search through the entire user input stream for errors before processing a MAGTF run.
- (8) Output formats should be reformatted where necessary to eliminate ambiguities and to facilitate reading and comprehension.

Appendix H

HQ FMFPAC DATA ANALYSIS

#### Appendix H

#### HQ FMFPAC DATA ANALYSIS

#### I GENERAL

This appendix contains a more detailed description of the analysis undertaken on the records of requisitions referred to in the HQ FMFPAC report. A summary description of the analysis, with some tabulations, is in the main body of this report.

The data to be processed consisted of several tape files that recorded some 900,000 requisitions originating in Vietnam during 1968-1970. Accompanying written material was used in decoding and interpreting these files. The files were originally prepared to obtain dollar funding requirements for the Vietnam operation. Records showed not only unit prices, but also quantities, dates, requisitioning organization, and combat status (active/na). This voluminous file warranted the expenditure of some modest analysis.

It was too much to expect that most TAMs in every current T/E would appear in the HQ FMFPAC file itself. Many descriptive TAM (end item) numbers have changed in the last few years; T/Es have changed; some equipment has become obsolete: some new equipment has been added. Even so, the file could be useful if a correlation existed between monthly consumption rate (demand) and a definitely determinable parameter, such as unit price or unit weight. If such a correlation could be validated, then future consumption, averaged over all TAMs in a T/E, could be estimated because both the weight and the T/E quantity of every TAM are entered in the MAGTF data base.

Even though there may be occasional deviations in consumption or demand from the consumption calculated from a correlation formula, the formula is still useful. If the deviations are small on the whole, and if large deviations are rare, the correlation formula can be used to compute a tentative T/E for an amphibious operation that must proceed under shipping constraint.

Experience with other supply systems suggests that a correlation between demand and unit weight exists of the form:

$$D = a W^b$$
,

where

D = Demand (quantity, units) per month

a = Constant of proportionality

W = Unit weight

b = Dimensions exponent, between -1/3 and -1.

If this correlation is indeed a valid one, ordinary regression analysis can be used with any sufficiently extensive data file to determine the unknown constants a and b. Indeed, the principal unknown is the exponent b. The constant of proportionality a, if one exists, can probably be determined in other ways. Furthermore, for some stocking purposes, the value of a is not needed.

#### II REDUCTION OF THE DATA

## A. Record Extraction

The file contained a record of all (or perhaps of some) requisitions that were made in ordinary fashion. It is known that no emergency requisitions were included in the file. The items requisitioned were identified by FSN (Federal Stock Number). The first step was to extract only those records that pertained to an end item (called a TAM). The extract routine required a specially prepared input file.

This file (file A) showed, for each TAM from A0001 to E9999, the FSN corresponding to the TAM. The flow chart for the extract routine is shown in Figure H-1.

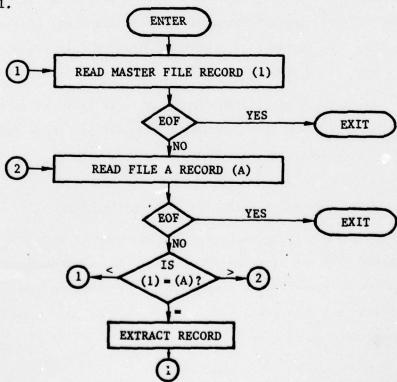


FIGURE H-1 ROUTINE FOR EXTRACTING TAM RECORDS FROM MASTER FILE

AD-A041 598

STANFORD RESEARCH INST MENLO PARK CALIF NAVAL WARFAR--ETC F/G 15/5
MATERIEL WEIGHT AND CUBE CONTROL (1975-1980).(U)
MAR 76 T H ALLEN, R B RINGO
N00014-75-C-0708
NL

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7 of 7 ADA041598





END
DATE FILMED
8 - 77

The primary sort in the master file was actually RUC (Reporting Unit's Code), so that the exit point in the preceding flow chart was, in fact, a subroutine that rewound file A, and progressed to the next RUC in the master file. After all RUC subfiles were processed, the extract routine was ended.

Certain organizationally identical units occurred several times in the master file--for example, HQ company in the 1st, 2nd, 3rd,... battalions. Each requisition record had a date (month 1-24). Combat status for each RUC was available. Thus, it seemed likely that some measure of variation between organizationally identical units in combat status in the same theater of operations might be obtainable.

## B. Extraction of Weight, Cube, and Square

Several extracted files were made, chiefly for military units M1038, M1988. The primary sort in these files was RUC; secondary sort was FSN. The record also showed requisition date, requisition quantity, unit price, and TAM.

For further processing, the files were resorted so that the secondary sort was TAM. The weight, cube, and square were then added to each record that corresponded to a class VII (end item) TAM.

#### C. Determination of Normalized Consumption Rate

In the preceding step, the T/E quantity of each TAM was also entered. The specific consumption rate (consumption rate per unit quantity in the T/E) was next obtained by simple division. This is the datum (D) that was expected to correlate logarithmically with unit weight (or with unit price).

Parenthetically, note that the T/E quantity used to bring out specific demand was the current (1975) authorized T/E quantity. It is common knowledge that most T/E quantities in the Vietnam Theater were expanded. If the expansion was more or less uniform over all TAMs in the T/E the specific demand (D) would be merely magnified uniformly. A correlation of the form  $D = a W^b$  would still be expected to exist, but with an altered value of a.

## C. Search for Correlation

Reasonable attempts to find a correlation ended in failure. Either the records available were incomplete, or else the postulated correlation does not in fact exist.

Many supply systems do show a correlation of the postulated type. That is, very large or expensive items of equipment are so well made, or are so well protected and so carefully serviced in use, that they tend to last longer than do smaller items of equipment. There does not seem to be a logical, operational explanation for the failure of this postulate. Perhaps the records were incomplete.